2024 ORE RESERVE ESTIMATE FOR THE BARRUECOPARDO W MINE

Prepared by:

MiningSense Global, SL

And reviewed by:

Mr. Hugh Thompson

For:

Saloro SLU

October 2024

Reference: SLO_ORE_2410

Version Control

Rev	DATE	DESCRIPTION	BY	CHK	APP
00	21/06/2024	Draft for the client	MiningSense	Hugh Thompson	
01	30/06/2024	Includes first comments from client on ver 0	MiningSense	Hugh Thompson	
04	03/07/2024	Review of v01 with changes in process costs	Hugh Thompson	Hugh Thompson	
05	18/07/2024	Review comments on ver04	MiningSense	Hugh Thompson	
06	23/07/2024	Review comments on ver05	MiningSense	Hugh Thompson	
07	24/10/2024	Ore production plan increased up to 1.8Mt of ore per year requested by customer	MiningSense	Hugh Thompson	

Purpose of the report

This report has been prepared by MiningSense Global SL (MiningSense) for the sole use of Saloro SLU (Saloro) and its parent company EQ Resources Limited (EQR), as the ore reserves estimate report as of September 2024, and may not be utilised or relied upon for any purpose other than that. The report is issued to Saloro SLU through the agreed recipients. Unless otherwise agreed by MiningSense, this does not grant rights to any third party.

The report is done following the requirements of the 2012 JORC edition.

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EXECUTIVE SUMMARY

Introduction

Saloro S.L.U. (a subsidiary of EQ Resources) is currently mining the Barruecopardo Tungsten deposit located in the municipality of Barruecopardo in the Castilla y León region of Western Spain. The mining operation began in 2019, and the annual production is 260.000mtu of high quality WO_3 scheelite concentrate. Operations consisting of an open pit mine and a processing plant.

MiningSense has been requested by Saloro SLU to complete a Ore Reserve Estimates report (ORE) compliant with JORC (2012) code for reporting reserve estimates. Where JORC is the Joint Ore Reserves Committee (https://jorc.org/). To do so, MiningSense, based in Salamanca Spain, has worked with Mr. Hugh Thompson, from Teneriffe Services Ltd. Based in Brisbane, Australia, who has acted as the Competent Person.

The Table 1 Summarises the Competent Person and other experts who assisted in completing this Ore Reserve Estimation report.

Table 1 Competent Person and Other Experts

List of Competent Persons				
Competent Person	**Position / company**	**Responsibility**	**Independent of Saloro**	**Professional Designation**
Hugh Thompson	Teneriffe Services	Overall Reserves CP	Yes	F. AusIMM, CP (mining)
Other Experts assisted the competent person				
Expert	**Position / company**	**Responsibility Chapters**	**Independent of Saloro**	**Professional Designation**
Jesús Montero	MiningSense	2.1, 3.1, 3.2, 6, 10, 11 12, 13, 14, 16, 17 Appendix 1, 2, 4, 5	Yes	M. AusIMM, IMEB Member, Mining Eng. Col. 526-Sur
María de los Ángeles Ramos	MiningSense	3.5, 3.6, 7.4, 9	Yes	Mining Eng. Col. 713-Sur
Carlos Mezquita	MiningSense	4, 5	Yes	Geologist
Mercedes Mallo	MiningSense	1, 2.2, 2.3, 3.3, 3.4, 3.5, 3.7.1, 7.2, 7.3, 7.4, 7.5, 8, 10, 15, 18, Appendix 3, 6	Yes	Mining Eng. Col. 4980
Pedro Jiménez	Saloro SLU	Metallurgic, Ch.11	No	
Evren Ören	Saloro SLU	Mineral Processing, Ch.11.3.1 & 11.3.2	Yes	

This report is more extensive than is usual for a typical JORC 2012 ORE report. This is primarily due to the time that has passed since the previously released Ore Reserves Estimate for this property, there have been numerous updates and changes in many areas fundamental to the estimate of the ore reserve. Therefore, the documentation contained herein is correspondingly more comprehensive.

Background

The Barruecopardo Tungsten deposit was sporadically mined from the early 1900's until the 1980's. The mining activity was re-started in 2019 and, up to December 2023, a total of 35.5Mt of total rock has been mined. Of this, 6.5Mt was mined as ore to produce a scheelite saleable concentrate, and the rest, 29Mt, was considered waste and sent to the waste dump.

The most important documents in the recent history of the project are:

- The current Mining License was requested via submission to the Mining Authority as the request for Exploitation Project (EP), C.E. Barruecopardo, Nº6.432-11 ("Proyecto de Explotación". Sadim, 2011). Sadim is a Spanish consulting firm. The submission for the EP included the required components of the Rehabilitation Plan and the Environmental Impact Assessment. The latest has not been provided for its review to develop this ORE report. The EP request was granted in 2014, as noted below.
- Mineral Resource Estimation Barruecopardo Tungsten Deposit. CSA Global Resources, 2012.
- Feasibility Study Saloro SLU Barruecopardo Tungsten Project. CSA Global Resources, 2012.
- Mineral Resource Estimation Barruecopardo deposit. JORC Code Edition 2012 technical report. Jörg Pohl, 2024.

The base technical information date is December 2023, and the effective date of the Ore Reserve Estimate is the 1st of September 2024.

Reliance on other experts

Hugh Thompson as Competent Persons accomplished mining professional with 40 years of experience in the feasibility, design, and operations of mining projects in Australia, Asia-Pacific, Africa and South America. He led numerous multi-discipline projects, working with professionals from backgrounds such as Environmental, Community, Geology, Mining, Processing, Infrastructure and Corporate aspects of projects. He has a B. Eng (mining), and a Grad. Dip (Finance). He is both a Fellow of the AusIMM and a CP mining. He holds First Class Mine Managers Certificates for; Western Australia, Queensland and Papua New Guinea.

The competent person, Hugh Thompson, has not visited the site. He has relied on MiningSense for their site visit verifications, noting the long relationship MiningSense has had with Saloro since they began operations in 2019. Hugh Thompson has known MiningSense professionally for 10+ years. Hugh Thompson held regular meetings with MiningSense during the delivery of this service; mostly via video conferences and one in-person meeting.

Mineral asset

Barruecopardo mine licence and operating permit were submitted for approval on 11 January 2011. These permits were granted, as follows:

- On the 16th of January 2014 the Environmental License, ("Declaración de Impacto Ambiental") (DIA), was granted, and published on the 6th of February 2014 in the public bulletin "Boletín Oficial de Castilla y León" ORDEN FYM/2014.
- The Mining License was granted on the 19th of December 2014 as "Concesión de Explotación Barruecopardo" (C.E. BARRUECOPARDO Nº6.432-10). This allows the extraction of Tugnsten, according to the Spanish mining regulation. The validity of the Mining License is for 30 years, being renewable two more times for the same period. The project site, and mining concession is 100% owned by Saloro SLU.

On August 2023 EQ Resources Limited (EQR) acquired a 100% interest in Saloro from Oaktree. Oaktree remains a substantial shareholder in EQR, because of the transaction.

The Barruecopardo project, covers 6.052km^2 is in the municipality of Barruecopardo, Figure 1, in the Salamanca province of Castilla y León, in Western Spain. This is 260km WNW of Spain's capital Madrid and close to the Portuguese border. The mine is 4 Kms south of Barruecopardo village and is accessed by the public roads DSA-573 and DSA-570 public roads as shown in Figure 3-3. These roads connect through with the town of Vitigudino (population2,700), and through to the regional capital of Salamanca (population 150,000) 95 Kms from the mine.

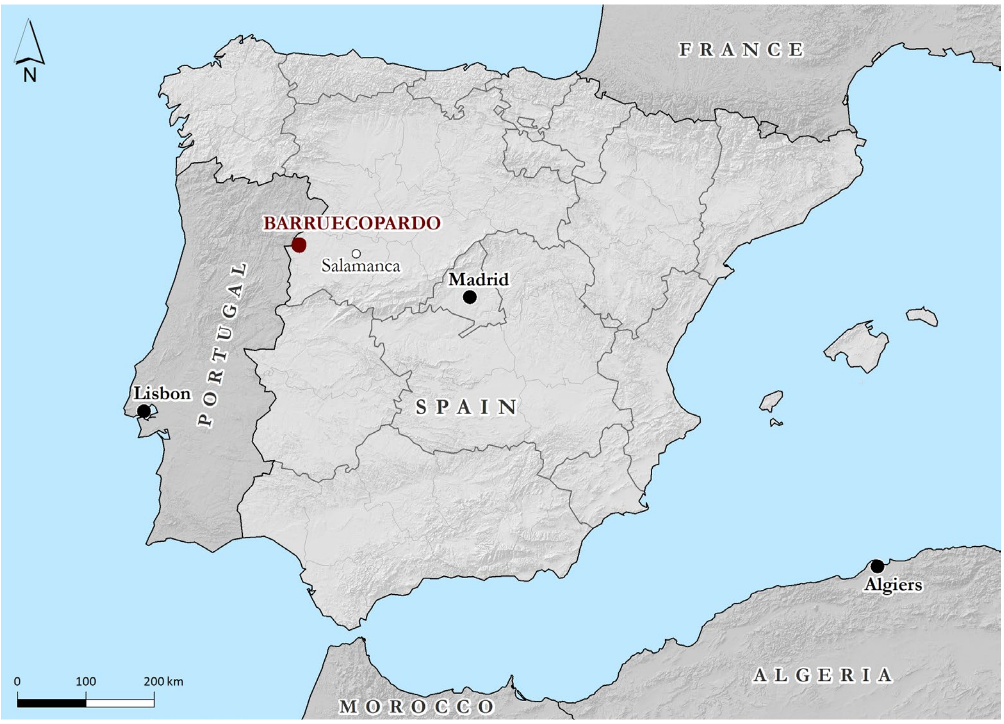


Figure 1 Barruecopardo Regional Location

Mineral Resource Estimate

This section is based on the document "JORC TECHNICAL REPORT Mineral Resource Estimation of Barruecopardo Tungsten deposit", prepared by Jörg Pohl (EurGeol. #1728) for SALORO SLU. in November 2023.

The first JORC resource reported by CSA in 2012 was based on 83 diamond drill holes (DD) drilled between 2006 and 2011. Seven more DD holes were added in 2012 and 2015 to test the deposit's eastern extension. In 2019, 27 DD holes were drilled to investigate structural control. Between 2021 and 2023, 26 more DD holes explored depth continuity, totalling 143 DD holes. After each campaign, the block model was updated, and 378 reverse circulation holes (RC) drilled between 2018 and 2020 were used for grade control. Holes drilled between 2021 and April 2022 aimed to explore deeper levels, referred to as "Phase 6", with May 2022 resource estimates using only DD holes.

Regarding regional geology, the deposit area is part of the Central Iberian Zone (CIZ) of the Iberian massif. The basement rocks are metasedimentary units and a large volume of granitic Variscan rocks. The Palaeozoic metasediments are part of the Shist-Grauwacke Complex (CEG). Predominant rocks in the area are massive intrusive granites and a metamorphic sediment sequence. The granite intrusions took place during the Variscan age (326-311 Ma) and have been deformed during the Variscan orogeny.

The deposit area is comprised of the following geological units:

- 13: Granite "Ala de Mosca", of medium to large grain size
- 14: Zone of occurrence of quartz dikes, and 14a pegmatites
- 18: Granite of Barruecopardo
- 19: Metasediments (pellitic-psamitic) with quarzitic intercalations

Two main orientations of structures exist in the area being NW-SE (mainly dextral) with a general dip of 40-60 degrees towards S-SW.

Mineralisation occurs within the pegmatitic veinlets cutting through the granite complex. Two main Tungsten minerals are present: scheelite (CaWO4) and wolframite ((Fe, Mn) WO4). Other abundant minerals are quartz, muscovite, pyrite, chalcopyrite and arsenopyrite. The mineralised veins, which correspond to the main stress orientation during the Variscan and later the Alpine orogeny, are oriented along a strike with a main orientation of NNE 10-15º, and they usually range between 1mm and 10 cm of thickness.

The Barruecopardo deposit is interpreted as a sheeted vein system deposit, with its veins being filled after hydraulic fracturing during the orogenic phases.

Regarding the resource estimation method, based on the drillholes (both DD and RC) and the grade control and geological mapping, wireframes representing packages of veins used as resource estimation domains were modelled and a rotated block model representing the orebody was developed. Parent block size is 6x6x5m (x-y-z), allowing two times sub blocking in the x and y direction, for a maximum resolution of 1.5x1.5x5m subblocks. Tungsten was interpolated using ordinary kriging. The estimation method consists of a separate validation of deleterious elements, application of top cut to avoid a nugget effect, definition of ordinary kriging parameters, and explanation of the estimation process.

Reporting of the MRE for the Barruecopardo deposit is based on the guidelines defined in the JORC code (2012 edition). The MRE has been classified as a Measured, Indicated and Inferred Mineral Resource of 24.4 Mt at an average grade of 0.195 % WO_3. The following table shows the MRE at a 0.05% WO_3 cut-off grade, the values in the table are rounded to reflect confidence levels in the estimate.

Table 2 Barruecopardo Mineral Resource Estimate as of 9th November 2023

Category	Tonnes (Mt)	Grade (WO_3 %)	Contained Metal (t of WO_3)
Measured	10.05	0.191	19,204
Indicated	10.46	0.174	18,200
Inferred	3.86	0.259	9,993
Grand Total	24.37	0.195	47,527

Geotechnical

The geotechnical performance and parameters of the Barruecopardo open pit have been comprehensively reviewed in 2023 and 2024. The geotechnical review was conducted by Mr

Leandro Alejano, Professor of Rock Mechanics, School of Mining and Energy Engineering, University of Vigo. During the study the historical information has been analysed and site visits undertaken to map exposed faces, measure the in-situ conditions of the rockmass and take samples for laboratory analysis of physical properties.

The rock mass was characterized using discontinuity samples from the mine, data from Golder's 2020 report and bi-monthly updates by Saloro and MiningSense. This update categorized the rock mass as a medium to good quality with a GSI of 62, identifying four main joint sets: three sub-vertical and one sub-horizontal.

The final slope design proposed confirms the previous Golder's report: double-benching of 10m resulting in 20m benches, at 75º inclination and 7m berms to a maximum depth of 290m.

Potential instabilities such as toppling, planar, and wedge failures were reviewed and recommendations to control their effects are included in the geotechnical report.

General pit slope stability was assessed using four representative sections of a similar pit design to the final pit obtained as per the current ORE, with 20m slopes and 59º overall slope angle. This resulted in safety factors above acceptable levels (FoS > 1.6, SRF > 1.4), ensuring stability if structural homogeneity and fault absence assumptions hold.

Mining operations

Mining is carried out by a contractor responsible for: Drill and blast, load and haul, maintenance of roads and sumps, and refeeding from the ROM stockpiles into the ROM Ore bin. All ore goes through the stockpiles, with no direct truck dumping into the ROM hopper. All waste goes to the ex-pit waste storage facility immediately to the west of the pit. All waste has been characterised as Non-Potential Acid Forming. Dried tailings from the concentrator are co-disposed inside the waste storage facility, along with the run-of-mine waste.

Saloro, as the owner, provides overall supervision, and mine technical services such as resource estimation, grade control in—pit, and pit design. As well Saloro directly conducts the progressive rehabilitation of the waste storage facility. Saloro operates the processing plant and uses a separate contractor for the offsite truck transport of concentrate as final product.

The water used in the operation comes from the mine drainage system, stored in various ponds on surface depending on the intended use.

The mining operation uses two 120 Tonne excavators with loading 100-tonne trucks on both ore and waste. Mining benches are nominally 5m high, with double-benched 10m heights used in bulk waste.

The mine works two 12-hour shifts Monday to Friday, with a 12-hour shift on weekends. Generally, day shift operates 1 excavator plus two drills, and the night shift operates two excavators and one drill.

Grade control

Grade control is based on the collection and analysis of data from blast holes after initial review with a UV lamp. The visual positive blasthole samples are analysed in the on-site laboratory, typically providing results within 1-2 days. These results are used to define polygons representing different grade zones within the blasting area. The definition of the polygons after blasting, that is their translation in space, is supported with on-site specialised software.

The material is classified into five categories:

- A+: Ore with a grade higher than 0.15% WO_3 and high sulphide content.
- A-: Ore with a grade higher than 0.15% WO_3 and low sulphide content.
- B+: Ore with a grade between the 0.07% and 0.15% WO_3, and high sulphide content.
- B-: Ore with a grade between 0.07% and 0.15% WO_3, and low sulphide content.
- OP: Ore assigned outside the geological model according to grade control.

Mine optimization and design

The resource block model used for grade estimation, has been re-blocked up to the SMU (Selective Mining Unit) of 6x6x5m for optimisation and design. This includes the addition of 12% planned dilution and 2% losses. Further to these planned losses and dilution, an additional operational loss and dilution of 6% and 15%, respectively, are applied in the mine plan.

To identify measured and indicated category resources for the optimization process a cut-off of 0.05% WO_3 has been applied using the domains defined as class 1 and 2.

The MRE resource block model has been checked for alignment along the main orientation of the mineralised veins' strike which is 15º NNE. The rotation is applied to minimise any dilution which might occur through misalignment between mineralisation and blocks. The extents of the block model are 1800m in the NNE-SSW direction, 800m across strike in a WNW-ESE direction with vertical extension between 755m and 300m RL. Good lateral definition along strike, and reasonable vertical continuity mean that mining to minimise loss and dilution should be successful.

The ORE block model has been depleted with the end of period surface as of 31 December 2023, to account for mining operations continuing from 1 January 2024, the date of record of the model, until 31 August 2024, date of record for the ORE estimate.

In the economic scenarios different mining limits have been set for total material moved from 6.2Mt to 9Mt of total material moved. A fixed plant throughput of 1.3Mt of ore is targeted per year and a minimum production of 9,000mtu/month.

The 8% discount rate has been applied to this optimization. All the cost and revenues have been denominated in US$ in the optimization software with the exchange rate of 1.10 €/US$ applied when the base data was provided in Euros.

The long-term scenario, used for selecting the ultimate pit-shell, considers a 54º slope angle, 71% metallurgical recovery and 330US$/mtu price scenario. This was done whilst including the material selected as ore for the short-term scenario. The pit-shell selected delivers 11.1Mt of ore at an average grade of 0.153% WO_3 and 48.6Mt of waste at a Cut-off grade of 0.059% WO_3.

Two pit-shells, maximum cash flow (pit-shell 36), pit-shell selected (pit-shell 45) and current phase in operation design boundary have been displayed in plan view, Figure 2, and section view, Figure 3.

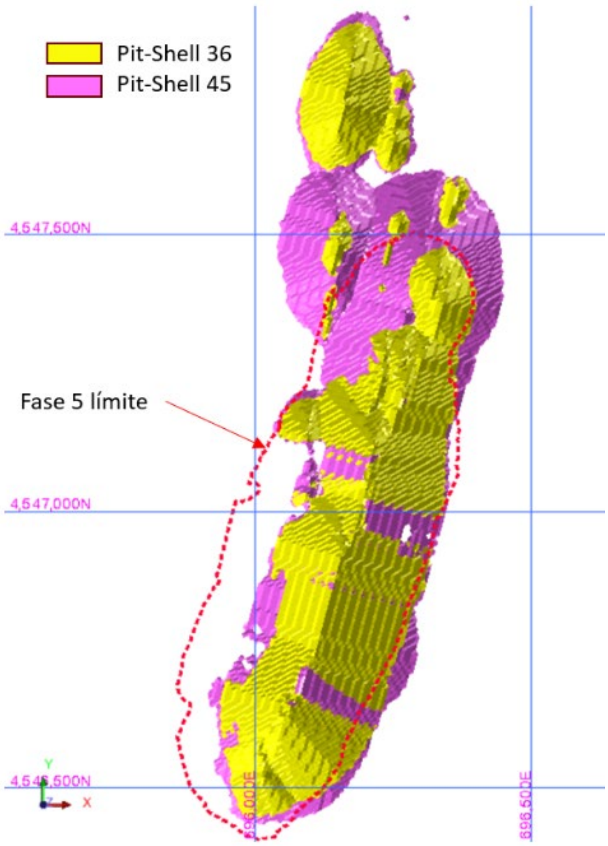


Figure 2 Pit-shell 36 versus Pit-shell 45 selected plan view

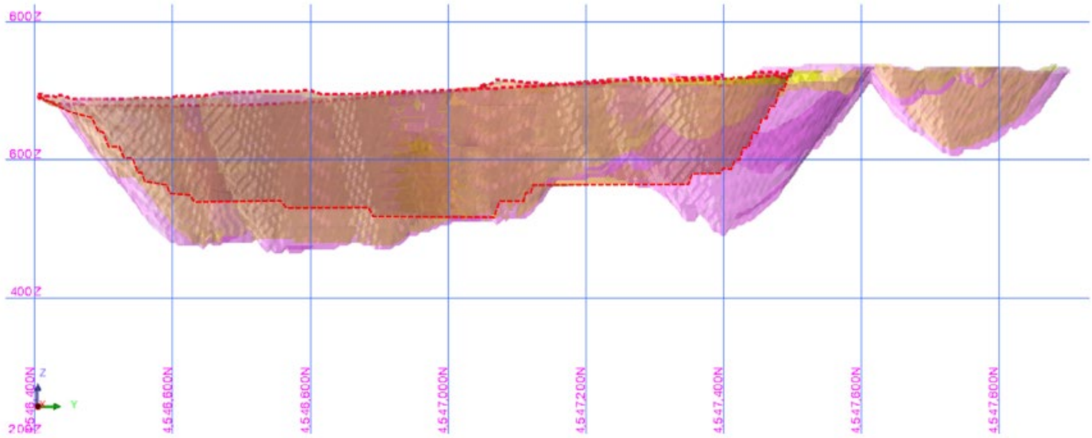


Figure 3 Pit-shell 36 versus Pit-shell 45 selected, section view

Final pit design has been performed after several iterations to optimize material ore/waste balance, and allowing for haul ramps etc. After that, practical phases have been designed for schedule and operational purposes with a minimum of 25 meters working width.

The phased design was then assessed in Whittle, with the assumption that the pit must be mined in a feasible sequence which delays, as much as possible the North area. This resulted in a Whittle DCF NPV reduction of 1.6M€ - if the northern phase is included. Furthermore, mining of the northern phase would require the removal of currently existing surface infrastructure, thus incurs a capital cost (not included in this analysis). As a result, the northern phase is not included in the production plan. The final design considered for planning is shown in Figure 4 in plain view, and Figure 6 in section view.

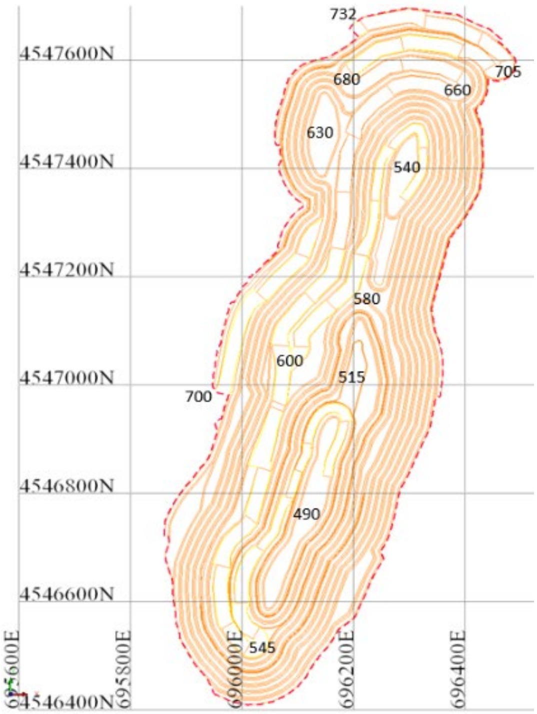


Figure 4 Final Pit Design

Figure 5 shows the final, selected pit design and the excluded “Northern Phase” As the North area is not considered in the final design due to the proximity of the current infrastructure and the high strip ratio in this area, it may be studied further for inclusion in a future reserve estimate.

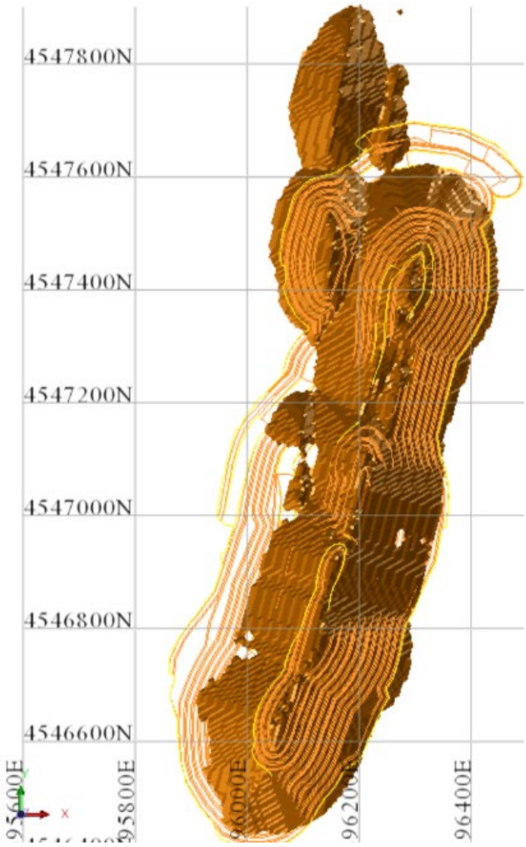


Figure 5 Final Pit Design vs Pishell plan view

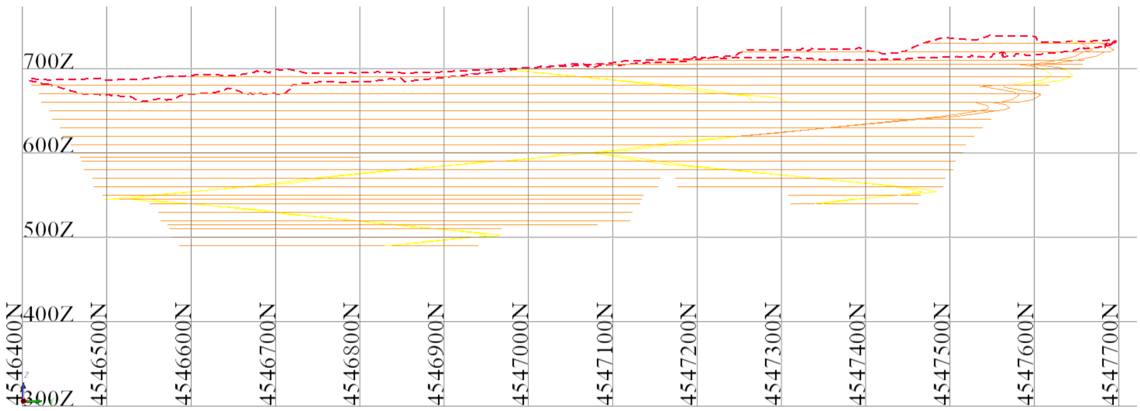


Figure 6 Final pit design long section view

Mine schedule

The pit has been scheduled out to the end of its' Life of Mine (LoM) so that it exhausts the reserves. Scheduling has been at monthly for the first two years, quarterly the following two and yearly for the remaining LoM. Reports are shown here only at an annual level. The existing stockpiles form part of the ore reserves, Table 3, shows the status as of 31 Dec 2023. These have been depleted to their levels as of 31 August 2024, for the mining conducted in the interim. These have been included in the mine plan.

Table 3 Stockpile status included in the Production Plan

Stockpile status	Tonnage Dec 2023	WO_3 %	After sorting t	% WO_3 after sorting
A	92,373	0.182		
B	125,695	0.101		
OP	54,684	0.095		
MAR (not included)	574,763	0.064		
Scalping (concentrate included)	332,458	0.058	29,921	0.55
To plan/reserves				
HG (A stockpile + scalping)	122,294	0.272		
LG (B stockpile + OP stockpile)	180,379	0.099		
MAR (updated 09/24 to plan)	335,375	0.061		

The production plan targets the ramp-up from 1.45Mt of ore in the first year to the stable target of 1.8Mt per year of ore feed to the process plant. Ore feed could come from either existing stockpiles, or ore direct mined from the pit The increase in plant capacity is based on the sucessful conclusion of the current de-bottlenecking campaign.; as described in 11.3.1below.

Table 4 shows the LOM mine plan by phases in each year, with Table 5 showing the plant feed and concentrate production for the same periods. The mine plan table shows the potentially deleterious elements of arsenic, sulphur and phosphorus.

In this production plan, material coming from the pit has been prioritised for feeding the crusher. Higher grades are available in the first years..

The stockpiles secure consistent plant feed if any disruption occurs in the pit during the first five years. The last two quarters in year 5 includes some marginal material blended with the low grade reaching a 0.12-0.10% WO_3 head grade after blending. The 6th year is processing the remaining marginal material for feeding the crusher reaching 1.2Mt of ore at head grade of 0.13%WO_3. During this year the phase 4 of in-pit mining exhausts the last of its' ore and phase 3 reaches a vertical development face of 60 meters.

Table 4 Mine Plan

Time	Item	Unit	1	2	3	4	5	6	7	Total
Phase1	Waste	Tonnes	4,045,997	1,237,962	124,403	-	-	-	-	5,408,363
	Ore	Tonnes	1,626,733	1,636,222	555,182	-	-	-	-	3,818,136
	Total	Tonnes	5,672,730	2,874,184	679,585	-	-	-	-	9,226,499
	EoP Bottom	RL	570	540	525-520-515					
	Ore-S	%	0.13	0.13	0.13	-	-	-	-	0.13
	Ore-AS	%	0.05	0.06	0.08	-	-	-	-	0.06
	Ore-P	%	0.08	0.09	0.09	-	-	-	-	0.08
Phase2	Waste	Tonnes	1,610,887	7,471,718	2,468,343	753,295	-	-	-	12,304,243
	Ore	Tonnes	71,925	614,076	628,677	417,376	-	-	-	1,732,054
	Total	Tonnes	1,682,812	8,085,793	3,097,021	1,170,671	-	-	-	14,036,297
	EoP Bottom	RL	715-710-705-700	665-660						
	Ore-S	%	0.05	0.07	0.10	0.12	-	-	-	0.09
	Ore-AS	%	0.03	0.05	0.05	0.04	-	-	-	0.05
	Ore-P	%	0.19	0.11	0.07	0.07	-	-	-	0.09
Phase3	Waste	Tonnes	63,104	-	-	3,443,866	6,166,642	7,254,143	2,458,352	19,386,107
	Ore	Tonnes	2,040	-	-	319	192,363	689,723	1,776,173	2,660,618
	Total	Tonnes	65,144	-	-	3,444,185	6,359,005	7,943,866	4,234,525	22,046,725
	EoP Bottom	RL				650	605	545	485	
	Ore-S	%	-	-	-	0.09	0.11	0.11	0.11	0.11
	Ore-AS	%	-	-	-	0.48	0.04	0.03	0.07	0.06
	Ore-P	%	-	-	-	0.02	0.08	0.04	0.07	0.06
Phase4	Waste	Tonnes	46,837	-	6,798,682	5,786,337	3,562,559	115,030	-	16,309,445
	Ore	Tonnes	-	-	277,128	803,621	1,628,832	145,306	-	2,854,887
	Total	Tonnes	46,837	-	7,075,810	6,589,958	5,191,391	260,336	-	19,164,332
	EoP Bottom	RL			690-685-680-675	625-620-615	555	540		
	Ore-S	%	-	-	0.09	0.09	0.12	0.10	-	0.11
	Ore-AS	%	-	-	-	0.48	0.04	0.03	0.07	0.16
	Ore-P	%	-	-	-	0.02	0.08	0.04	0.07	0.05
Total	Waste	Tonnes	5,766,825	8,709,680	9,391,429	9,983,498	9,729,201	7,369,173	2,458,352	53,408,158
	Ore	Tonnes	1,700,698	2,250,297	1,460,987	1,221,316	1,821,195	835,029	1,776,173	11,065,695
	Total	Tonnes	7,467,523	10,959,977	10,852,415	11,204,814	11,550,396	8,204,202	4,234,525	64,473,853
	StripRatio		3.39	3.87	6.43	8.17	5.34	8.83	1.38	4.83
	Ore-S	%	0.12	0.11	0.11	0.10	0.12	0.11	0.11	0.11
	Ore-AS	%	0.05	0.06	0.05	0.33	0.04	0.03	0.07	0.08
	Ore-P	%	0.08	0.09	0.06	0.04	0.08	0.04	0.07	0.07

Table 5 Plant Feed

Ore Feed by Source	Units	1	2	3	4	5	6	7	Total
From Pit HG	Tonnes	946,205	1,074,091	677,646	509,877	603,627	308,408	962,532	5,082,386
From Pit LG	Tonnes	409,612	744,930	783,341	711,439	1,215,377	526,621	813,641	5,204,960
From Stockpile HG	Tonnes	99,976	-	157,433	-	-	-	-	257,409
From Stockpile LG	Tonnes	-	-	200,666	597,930	-	354,374	-	1,152,970
Plant Feed - Total	**Tonnes**	**1,455,793**	**1,819,021**	**1,819,086**	**1,819,246**	**1,819,004**	**1,189,403**	**1,776,173**	**11,697,725**
Plant Feed WO_3 Grade	%	0.22	0.18	0.16	0.12	0.13	0.12	0.16	0.16
mtu Contained		317,808	347,726	292,046	215,249	232,395	137,624	292,643	1,835,490
Metallurgical Recovery	%	58	71	71	71	71	71	71	69.2
mtu Produced		184,329	246,885	207,352	152,826	165,000	97,713	207,777	1,261,883

The Figure 7 shows the ore and waste mine production by phase each year. First year has been limited to 7.5 MT total movement and 1.45MT of ore to align with the current year production on site. The tonnage declines in absolute terms from year 6 onwards will be offset by deeper pit hauls, therefore total equipment fleets are expected to be constant until the later years of the mine life.

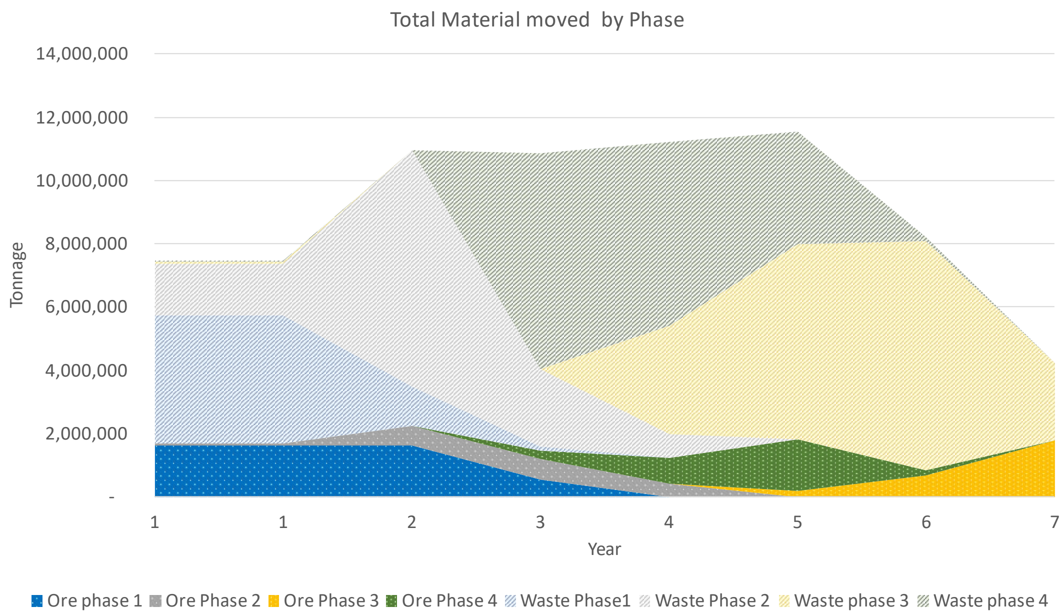


Figure 7 Mine Ore and Waste Production Plan per Phase

The Figure 8 shows the different source contributors to plant feed, the average head grade and the expected mtu contained.

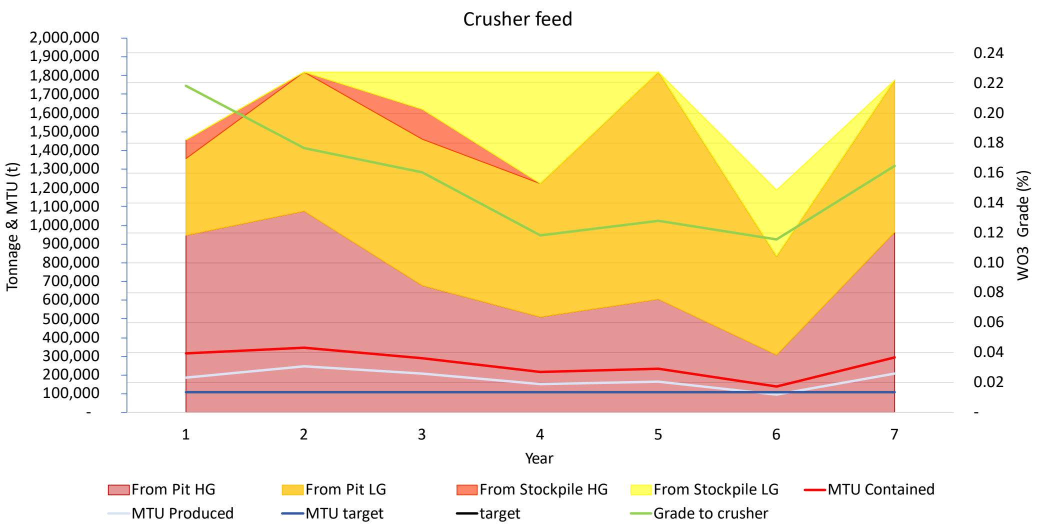


Figure 8 Plant Feed Production Plan

As the mine is in operation, phase position and stockpiles, Table 6, have been updated with the end-of-month surface in Aug 2024. During this eight month of operations a total of 4.4Mt of material has been excavated according to the reserves block model to produce 502kt of high-grade ore and 414kt of low-grade ore. A total of 0.9Mt of ore at an average grade of 0.20% that contains 175,564 mtu.

Table 6 Stockpile update EOM Aug 24

Stockpile status	Tonnage EOM Aug 2024	Grade	Concentrate t (after sorting)	Concentrate WO_3% (after sorting)	mtu
A	144,883	0.194			28,058
B	157,290	0.102			16,009
OP					
MAR (not included)	337,399	0.064			21,593.54
scalping (concentrate included)	139,450		12,550	0.058	20,076
To plan/reserves					
HG (A stockpile + scalping)	157,433	0.183			48,134
LG (B stockpile + OP stockpile)	157,290	0.102			16,009
MAR (updated 09/24 to plan)	335,375	0.061			20,572
Total	**650,098**	**0.10**			**84,715**

Mineral processing

The processing route is gravimetric concentration. The ore is stockpiled and blended before feed to the crushing circuit. This has the objective of reducing the size of the ore from 800mm to 5mm.

Once the material is reduced a preliminary concentration is affected by removing some of the coarse particles that contain mainly gangue from which the potential mineralized particles are recovered in the following ore sorting stage. This ore sorting stage can remove 25% of the waste included in the crusher feed material with a minimum loss of metal.

The process continues with the gravimetric plant where the heavy minerals are separated from the lighter ones by a combination of screens, cyclones, spirals and shaking tables. The gravimetric product includes sulphides. These deleterious elements are then removed by two stages of flotation followed by a further gravimetric concentration using shaking tables.

The underflow material from the flotation circuit is dried and passes through a cascade of magnetic separators to remove deleterious elements, increasing also the concentrate grade and producing the final scheelite concentrate.

The scheelite concentrates range from 60% to 70% WO_3, it has been used 64% for the ORE. The mine plan supporting the ORE report includes the production of 1,257,064 WO_3 mtu in a scheelite concentrate weighting 19,642 t of concentrate.

The processing plant was built in 2019 and has operated for five years and is in good condition. Nevertheless, the metallurgical recoveries achieved have been low in comparison with both other similar projects, and with the plant design criteria.

Recently Saloro management has put in place a program to upgrade the plant, and thereby improve recovery. This program identifies the recoveries per area and equipment, prioritising the improvements with the highest impact on the recovery. The plan to implement these changes was initiated in January 2024. The complete plan will take some 18 months to implement, and thus be complete circa December 2025. These initial results, which are 'tracking to plan' so far and the detailed future works defined by Saloro are encouraging. This provides credibility to that recovery will lift from the existing (dec 2023) of ~ 50% to the 71% assumed in this report.

The 7-stage improvement plan covers:

- Homogenization of the feed material passing through different stages.
- Increased Recovery of fines.
- Pre-concentration by removing part of the waste by adding new circuits of ore sorting and scalping. These are already in place by May 2024.
- Replacement of certain equipment for others with easier maintenance and improved control.
- Reduction in source rock fines production.

This plan is costed into the economic analysis conducted in this ORE, as is the monthly variable recovery scheduled in 2024 to 2025 whilst the improvement plan is being enacted.

Waste Storage

Over the life of the current Barruecopardo mine Project, there have been several waste storage facility designs. The various changes and extensions have been required and implemented. Essentially growing the same footprint. As and when relevant these have been presented with their corresponding documentation to the relevant mining authorities as re-permitting has been required. The last of these was in 2021, whereby a total volume of 25.2 Mm^3 has been approved for waste storage on this project.

Noting that the plant tailings are co-disposed with the run-of-mine waste into the same waste storage facility. Therefore, the facility needs to be of sufficient volume to allow for both the tailings storage as well as the mine waste.

The total waste volume required to be stored, in order to support this 2024 reserve estimation is 6.50Mm^3 of tailings, including ore mined and stocked material, and 23.44Mm^3 of waste rock, as shown in Table 7.

Table 7 Waste volume LOM Storage

* Calculated by Topo_Origen	Volume (m^3)
Taillings	6,498,736
Waste	23,443,589
Total volume with swell and compaction	29,941,325

The currently approved dump currently has a capacity of 25.2Mm^3, of which 19.3Mm^3 have already been filled. This leaves some 5.9Mm^3 of remaining volume approved. Figure 9 shows the waste storage facility as of May 2024. Therefore, some 24 Mm3 (30 – 6) of extra approved waste storage is required to support this 2024 ore reserve estimate.

During the second half of 2024 a new waste dump project will be presented to the mining and environmental regulators for permitting. This will have a total volume of almost 69Mm^3, an increase of 43 Mm^3 in total storage capacity, and more than sufficient to satisfy the LOM waste storage requirements. The extended waste storage facility is entirely within the currently approved Barrauecopardo project site and is required to be in place by late 2026. This is considered feasible timing, given the prior history of re-permitting waste storage, the technical aspects involved, and discussions with regulators.

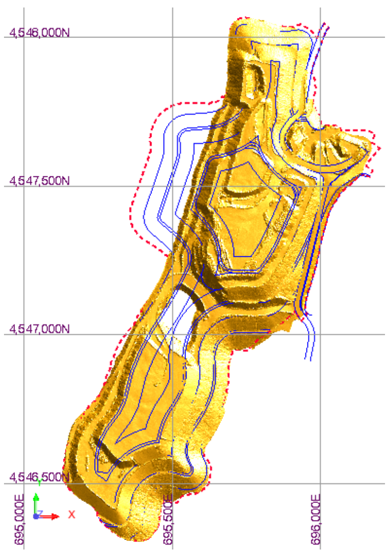


Figure 9 Waste storage - May 2024

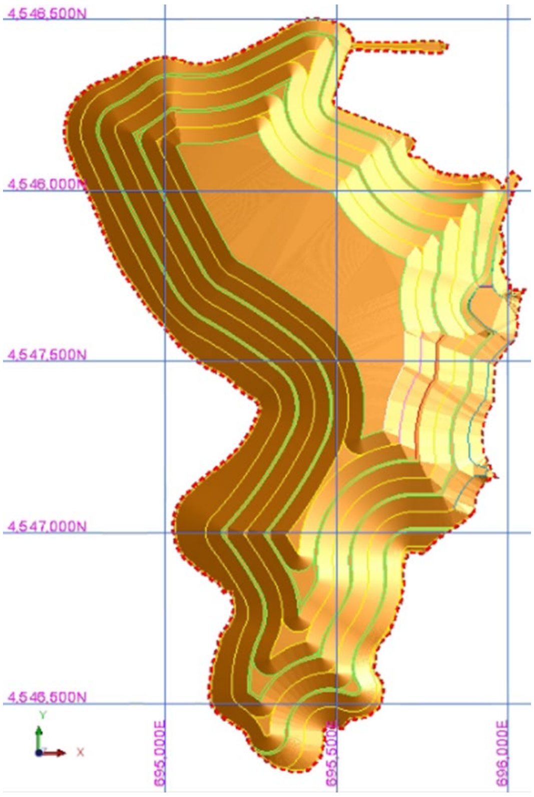


Figure 10 Final waste storage, to be submitted 2024

Table 8 Waste Storage Facility design criteria

Waste Storage Facility design criteria	
Slope angle	33 degrees
Berm width	8m
Bench height	10-30m
Final slope angle after reclamation	18/20 degrees
Swelled density	2.3t/m3
Swell factor	25%
Ramp width	25m
Ramp gradient between	7/10%
Overall slope angle	16 degrees
Heigh above ground	90m
Total volume capacity	69.4Mm^3

Water Management

The water management system is based on controlling water flows to separate clean water from the process water. Aiming to minimise the discharge of used water into the natural environment and optimize the use of water in all process during the LoM.

Surface drainage system to collect run-off water outside the pit and all facilities are maintained to optimize the water balance and to minimize the environmental impact.

The drainage network consists of 4 water ponds lined with high-density geosynthetic plastic (PEAD) equipped with their own pumping systems. Several local sumps and an external drainage system collects pit bottom water and rainfall and delivers that water to the ponds. After settlement this is then sent to the water treatment plant, from where it goes to either the process plant or discharged off-site.

The water table level is monitored through a series of perimeter observation holes. An underground and surface monitoring plan is in place to detect any early-stage change in the performance of the aquifers.

Environmental Social and Permitting

The project currently has valid and appropriate Environmental License(s) and Mining License to operate until 2044. The project also has the appropriate construction authorisation that enabled the 2018 construction of the plant and the project associated facilities.

The water usage and water discharge permits are in place with a water consumption permit of 884,774m^3/year and a water discharge permit of 12,000m^3/year. Most of the water consumed is retained in the tailings and used for rehabilitation and dust control. With this permit, the mine has been able to work continuously since 2019 without any interruption due to water permit restrictions. Saloro in any case is currently requesting an increase in their discharge permit to improve the operation flexibility.

The current open pit is authorised for a limited footprint, that supports operations until the end of the year 2 of the mine plan reported in this ORE. To support the full LOM considered for this ORE, it will be necessary to seek approval to increase the waste dump footprint, as described above, and to increase the permitted open pit footprint. Both items are planned to be requested in 2024.

These will, likely, be considered a 'material change' to the existing operating licence for the project, therefore it is likely that a new, or revised Environmental Impact Assessment will also be required. This process usually takes 1 to 2 years to be assessed by regulators.

As the mine is in operation and the changes triggering an environmental impact assessment are not new or substantial, it is likely that time between submission and approval may be shorter. Furthermore, although the project is in an environmentally sensitive area, it is expected that the new authorizations are likely to be granted based on the exceptional performance of the project to date on the environmental aspects, as well as the positive social perception of the operation.

Capital and Operating Cost

The cost base used for the model have provided by Saloro in Euro as per 2024Q1.

The capital costs are limited to the investment needed in the plant to improve recovery, as described above, plus a reasonable allowance for overall sustaining capital Table 9 summarises this CAPEX.

Table 9 CAPEX summary

Item	Unit	Total LoM
Plant improvements	k€	630
Sustaining capital	k€	700
Total CAPEX	k€	1,330

The operating cost is composed of:

- Mining costs – contractor operation.
- Processing cost – own operation.
- General and administrative costs.
- Selling costs.

The Table 10 summarises the operating costs used, that are aligned to the current Saloro costs.

Table 10 OPEX summary

Item	Yearly Cost (k€/year)	Total LoM Cost (k€)	Per total Mined Tonne €/t (o+w)	Per Ore tonne €/t ore	Per metal con tonne produced €/mtuWO3
Mine	13,582	122,235	1.90	11.05	97.24
Process	9,294	83,644	1.30	7.56	66.54
G&A	1,842	16,578	0.26	1.50	13.19
Selling	399	3,587	0.06	0.32	2.85
Total OPEX	**25,116**	**226,044**	**3.51**	**20.43**	**179.82**

The rehabilitation costs considered includes the waste storage facility slope restoration, progressively undertaken during the operating life of the mine, and the final site decommissioning including stockpiles, built facilities, ponds and haul roads. The pit will be maintained partially backfilled. The pit slopes will be rehabilitated to be used for future nests for the birds. Table 11 shows the rehabilitation costs.

Table 11 Rehabilitation costs

Item	Unit	Total LoM
Waste dump recovery	k€	1,224
Decommissioning	k€	3,928
Total Rehabilitation	k€	5,152

Technical Economic Model

A life of mine economic model has been developed, to satisfy the Reasonable Prospects for Economic Extraction criteria of JORC. This has been developed only for the purposes of testing that the mine reserves show a likelihood of supporting an economically viable proposition. This economic work is general in nature and limited to assessing probable economic exploitation. It is not meant to be a fully detailed financial model and should not be understood in terms of assessing the project value or used for that purpose.

Financial assessment was completed to check reasonable prospects of positive economic outcome using these factors and assumptions.

This resulted in the Competent Person being of the opinion that there indeed are reasonable prospects of economic extraction.

Ore Reserve Statement

After technical and economic analysis done considering the modifying factors, described in previous sections, the Ore Reserve Statement can be declared with sufficient confidence.

The Table 12 shows the Resource conversion into Reserves.

Table 12 Resource to reserve and design conversion

	Mineral Resource Estimation Cut-Off 0.05% WO_3			Ore Reserve Cut-Off 0.06% WO_3*			Pit Design Cut-off 0.06% WO_3*			
Category	Tonnes (Mt)	Grade (WO_3 %)	Contained Metal (t of WO_3)	Tonnes (Mt)	Grade (WO_3 %)	Contained Metal (t of WO_3)	Tonnes (Mt)	Grade (WO_3 %)	Contained Metal (t of WO_3)	Category
Measured	10.05	0.191	19,196	7.13	0.155	11,021	7.68	0.164	12,581	**Proven**
Indicated	10.46	0.174	18,200	3. 33	0.141	4,704	3.40	0.141	4,770	**Probable**
Inferred	3.86	0.259	9,997							
Grand Total	**24.37**	**0.195**	**47,522**	**10.46**	**0.156**	**16,367**	**11.07**	**0.157**	**17,351**	

*Includes loss and dilution

The Ore Reserve Estimation updated in August 2024, in accordance with the JORC Code (2012 Edition) guidelines are reported in the Table 13.

"An Ore Reserve is the economically mineable part of a Measured and/or Indicated Mineral Resource. It includes diluting materials and allowances for losses, which may occur when the material is mined or extracted and is defined by studies at Pre-Feasibility or Feasibility level as appropriate that include the application of Modifying Factors. Such studies demonstrate that, at the time of reporting, extraction could reasonably be justified." JORC Code (2012 Edition)

After technical and economic analysis done considering the modifying factors, described in previous sections, the Ore Reserve Statement, included in Table 13, can be declared with sufficient confidence extending the Life of Mine.

Table 13 Ore Reserves Statement September 2024

Classification Category	Mining Type	Tonnes (t)	Grade (WO_3%)	Metal contained (mtu)
Proven	Open-Pit	6,816,530	0.16	1,102,148
	Stockpile	314,723	0.14	
Total Proven		7,131,253	0.155	1,102,148
Probable	Open-Pit	3,332,177	0.14	470,387
	Stockpile			
Total Probable		3,332,177	0.141	470,387
Total	Open-Pit	10,148,707	0.16	1,572,535
	Stockpile	314,723	0.14	64,143
Total Ore Reserve		**10,463,430**	**0.156**	**1,636,678**

Notes:

- Reported from the reserves block model "saloro_202310_res_rot_6x6x5.mdl" regularized block model from the resources block model saloro_202310_res_rot.mdl.
- Cut-off grade 0.06 % WO_3 for the long-term use for all the stages of the project.
- Modifying factors operational loss 6% and 15% operational dilution over a regularised model that includes 2% loss and 12% dilution against the resource model.
- Metallurgical recovery of 58% during the first year of production and the rest of LoM metallurgical recovery of 71%.
- Stockpiles A, B, OP and scalping have been considered. No marginal stockpile is included in this Ore Reserve Statement. Although it has been included in the LOM mine plan developed to test reasonable economic extraction. This is minor in quantity, and described in section 8.
- The reporting standard adopted for the reporting of the ORE uses the terminology, definitions and guidelines given in the Joint Ore Reserves Committee (JORC) Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (2012).
- It is considered that last report completed in 2012 scheduled 9 years of production starting in 2019 and this ORE reports additional 7 years of production plan which means the LoMP has been extended a total of 3 years of production since last ore reserves declaration. Below, in Table 14, 2012 MRE and reserves included in the production plan in the exploitation project for reference.

Table 14 2012 MRE and Reserves

	MRE 2012			Reserves 2012 (not under standard code reported)			
Category	**Tonnes (Mt)**	**Grade (WO_3 %)**	**Contained Metal (t of WO_3)**	**Tonnes (Mt)**	**Grade (WO_3 %)**	**Contained Metal (t of WO_3)**	**Category**
Measured	5.47	0.34	18,000	5.20	0.37	19,209	**Proven**
Indicated	12.33	0.26	32,000	2.87	0.32	9,169	**Probable**
Inferred	9.59	0.23	22,000	0.81	0.24	1,975	
Grand Total	**27.39**	**0.27**	**72,000**	**8.07**	**0.35**	**28,378**	**Proven + Probable**

Risks overview

The main risk in the estimate of these reserves is in not achieving the planned metallurgical recovery. Lower than planned recovery will compromise the economics of the project. To mitigate this risk, it is recommended that clear KPIs' are defined to measure the incremental and long-term performance of the recovery improvement plan currently underway.

The other risks of note are;

- The risks inherent in mining veined deposits such as Barruecopardo whereby loss and dilution control require tight operational supervision, and vigilance.
- Delays in obtaining the required variations to operating permits and authorisations, as necessitated by the extension of the Life of Mine.

Forward work plan

It is recommended to perform a detailed study to reduce planned and operational loss and dilution. Although economic viability is proven, profitability could be increased by optimizing these parameters and delivering increased value to the project. Work is suggested in both how loss and dilution are operationally controlled through all stages of mining, as well as how it is modelled and assessed for planning.

The reserves are highly influenced by the expected recovery, a considered program on how these improvements in the plant produce the expected recovery, on a near to real-time basis is critical and must be aligned with an accurate reporting system to track the changes and improve future planning.

1 Introduction

Saloro SLU. (a subsidiary of EQ Resources) is currently mining the Barruecopardo Tungsten deposit located in the municipality of Barruecopardo in the Castilla y León region of Western Spain. Current operations began in 2019, with annual production of 260,000mtu of high quality WO_3 scheelite concentrate. Operations consist of an open pit mine and a processing plant.

Mining is by traditional drill & blast, Load & Haul methods. Ore reports to stockpiles near the ROM feed point, and waste goes to the waste storage facility, adjacent to the open pit. The primary crusher takes the ROM feed, and the ore goes through various stages of crushing and milling before being concentrated in the gravimetric plant. This produces concentrate of saleable specification. The tailings produced as waste from the process plant are co-disposed in the waste storage facility.

MiningSense has been requested by Saloro SLU to complete an Ore Reserve Estimates report (ORE) compliant with the JORC (2012) code for reporting reserve estimates. Where JORC is the Joint Ore Reserves Committee (https://jorc.org/). To do so, MiningSense, based in Salamanca Spain, has worked with Mr. Hugh Thompson, from Teneriffe Services Ltd., based in Brisbane, Australia, who has acted as the Competent Person.

The Table 1 Summarise the Competent Person and other experts who assisted in completing this Ore Reserve Estimation report.

Table 1-1 Competent Person and Other Experts

List of Competent Persons				
Competent Person	Position / company	Responsibility	Independent of Saloro	Professional Designation
Hugh Thompson	Teneriffe Services	Overall Reserves CP	Yes	F. AusIMM, CP (mining)
Other Experts assisted the competent person				
Expert	Position / company	Responsibility Chapters	Independent of Saloro	Professional Designation
Jesús Montero	MiningSense	2.1, 3.1, 3.2, 6, 10, 11 12, 13, 14, 16, 17 Appendix 1, 2, 4, 5	Yes	M. AusIMM, IMEB Member, Mining Eng. Col. 526-Sur
María de los Ángeles Ramos	MiningSense	3.5, 3.6, 7.4, 9	Yes	Mining Eng. Col. 713-Sur
Carlos Álvarez Mezquita	MiningSense	4, 5	Yes	Geologist
Mercedes Mallo	MiningSense	1, 2.2, 2.3, 3.3, 3.4, 3.5, 3.7.1, 7.2, 7.3, 7.4, 7.5, 8, 10, 15, 18, Appendix 3, 6	Yes	Mining Eng. Col. 4980
Pedro Jiménez	Saloro SLU	Metallurgic, Ch.11	No	
Evren Ören	Saloro SLU	Mineral Processing, Ch.11.3.1 & 11.3.2	Yes	

1.1 Background

The Barruecopardo Tungsten deposit was sporadically mined from the early 1900’s until the 1980’s. The mining activity was re-started in 2019 and, up to December 2023, a total of 35.5Mt of total rock has been mined. Of this, 6.5Mt was mined as ore to produce a scheelite saleable concentrate, and the rest, 29Mt, was considered waste and sent to the waste dump.

The most important documents in the recent history of the project are:

- The current Mining License was requested via submission to the Mining Authority as the request for Exploitation Project (EP), C.E. Barruecopardo, Nº6.432-11 (“Proyecto de Explotación”. Sadim, 2011). Sadim is a spanish consulting firm. The submission for the EP included the required components of the Rehabilitation Plan and the Environmental Impact Assessment. The latest has not been provided for its review to develop this ORE report. The EP request was granted in 2014, as noted below.
- Mineral Resource Estimation Barruecopardo Tungsten Deposit. CSA Global Resources, 2012.
- Feasibility Study Saloro SLU Barruecopardo Tungsten Project. CSA Global Resources, 2012.
- Mineral Resource Estimation Barruecopardo deposit. JORC Code Edition 2012 technical report. Jörg Pohl, 2024.

A full bibliography of source material used can be found in the section 18. Section 2.3 outlines the other key documents relied on for this reserve estimate. The data sourced from Saloro by MiningSense to undertake this service has been verified and validated to consider it fit for purpose to undertake this service. Where and as appropriate MiningSense has performed further reasonableness checks to establish the credibility of the data provided. This implies reliance on the data originators, as to underlying quality

MiningSense has been providing an external service for completing monthly and annual mine plans and designs, for several years. The monthly mine plans are used onsite, and the annual mining plan is part of the submission by Saloro to the regulator of the annual Works Plan (“Plan de Labores”) that contains the summary of what has been done in the last year and the plan for the coming year. Therefore, MinignSense’s knowledge and understanding of the Barruecopardo mine is significant.

The economic model presented in this report has been formed to satisfy that the mining reserve and mine plan has a Reasonable Prospect of Economic Extraction, the RPEE criteria for JORC 2012.

1.2 Reporting compliance

MiningSense has relied on the accuracy and transparency of the information listed in the section 2.3, as provided by Saloro SLU. as supporting documentation to underpin this Ore Reserve Estimate.

Saloro SLU has confirmed that to its knowledge, the information provided is complete and not incorrect or misleading in any respect. MiningSense has no reason to believe that any material facts have been withheld. The economic model used to confirm the reasonable expectation of economic extraction of the mine plan was and built by MiningSense based on the information provided by Saloro.

MiningSense declares, to the best of its knowledge, that it has taken all reasonable actions to ensure that all information contained in and reported on in this Ore Reserve Estimation (ORE) is in accordance with these facts and contains no material omission that might affect its significance. This has been checked by the Competent Person acting as a reviewer.

This report is more detailed than the typical JORC 2012 ORE report. This is because of the time that has passed since the last time a JORC ORE was presented, which was by CSA in their DFS report of 2011. Therefore, this comprehensive report was required to update all the changes since then to accurately reflect the current situation of the mining project.

1.3 Base technical information date and effective date

The base technical information date is December 2023, and the effective date of the Ore Reserve Estimate is the 1st of September 2024.

1.4 Verification and validation

MiningSense has reviewed and assessed all technical material and documentation provided by Saloro SLU. MiningSense relies on Saloro SLU. as the owner for verifying this material. If any additional information was needed it has been submitted upon request and reviewed during the elaboration process of this technical report.

The verification of technical information, included as part of this report, has been aided by multiple site visits to inspect of the facilities, production performance, and historical data. Discussions with key stakeholders have been held in respect of all the matters that are considered as inputs for this Ore Reserve Estimation. These have also helped to identify the potential risks and opportunities that result from this service.

The assumptions for the commodity (WO_3) price have been reasonably assessed and are based on the forecasts from the Wood Mackenzie 2021 report for the Ammonium Paratungstate (APT) covering the period 2021 to 2030. This is a consulting report commissioned directly for EQ Resources from Wood Mackenzie.

The Ore Reserves Estimate assumes that the forecast metallurgical improvements, as described in the section 6.2 will be achieved. This relies on the action plan that started early 2024 being successfully completed.

1.5 Limitations, reliance on information and Statement

The information used for this Ore Reserve Estimation has been based on both historical information and short and medium-term forecasts including factors such as operating performance, cost forecasts, market forecasts and foreign exchange rates. As a result, this report should not be taken as a guarantee of the economic performance of the deposit as any and all of these factors or assumptions may change. The prediction of these factors involves assessment of real risks that could change the outcome of this report. The key risks and are listed in section 16. Similarly the achievement of the production plan included here for the LoM is not guaranteed although MiningSense holds reasonable prospects for its' completion as described Cashflows derived from the Economic Model forecast contained herein are inherently uncertain and actual results may differ. The cost model is based on the updated expenditure and contracts in place as of December 2023.

Part of the information provided by Saloro SLU. has been elaborated by external consultants, as indicated in section 2.3. All the specialists responsible have wide and proven experience in their disciplines covered in the reports. MiningSense fully trusts in the veracity of these documents although has not fundamentally verified such information and disclaims any responsibility or liability in connection with such information.

MiningSense disclaims any liability or responsibility arising from any modification or misuse of this document by Saloro SLU., or others.

MiningSense will receive a fee for providing this service and this report as per normal professional consulting practices and will not depend on the findings of this report. MiningSense declares that it will not receive any other benefit as result of its services that might affect the veracity of the information contained in this report and will not use the information and findings for its own benefit.

2 Reliance on other experts

2.1 Qualifications of consultants and competent persons

Hugh Thompson, acting as the Competent Person as defined in JORC (2012) is an accomplished mining professional with 40 years of experience in the feasibility, design and operations of mining projects in Australia, Asia-Pacific, Africa and South America. He led numerous multi-discipline projects, working with professionals from backgrounds such as; Environmental, Community, Geology, Mining, Processing, Infrastructure and Corporate aspects of projects. He has a B. Eng (mining), and a Grad. Dip (Finance). He is both a Fellow of the AusIMM and a CP mining. He holds First Class Mine Managers Certificates for; Western Australia, Queensland and Papua New Guinea.

MiningSense S.L. has a long relation with Saloro and has been collaborating giving technical support as described in detail in section 3.3.

2.2 Site visit

The competent person, Hugh Thompson, has not visited the site. He has relied on MiningSense for their site visit verifications, noting the long relationship MiningSense has had with Saloro since they began operations in 2019. Hugh Thompson has known MiningSense professionally for 10+ years. Hugh Thompson held regular meetings with MiningSense during the delivery of this service; mostly via video conferences and one in-person meeting.

Since kick-off meeting on the 7th of November 2023, regular site visits were scheduled by MiningSense in accordance with Saloro SLU. for data reception and verification purposes.

2.3 Resources of information

Apart from the data shared by Saloro with MiningSense for the specific task of developing this ORE report, MiningSense has been periodically engaged at Barruecopardo mine by Saloro since 2019. This historical knowledge and information has also been used in this service.

Table 2-1summarises the key source documents and data inputs used to provide this ORE.

Table 2-1 Key documents and data used in the 2024 ORE

Document	Description
Título de Concesión de Explotación	(, Junta de Castilla y León, 2014) Exploitation Concession Permit
202405_Limites administrativos	(Saloro, 2014) Mining Lease
202405_Titularidad terrenos	(Saloro, 2014) Land Ownership
202405_Zonas protegidas	(Saloro, 2014)Environmental protection areas
140206 Declaración de Impacto Ambiental (BOCyL)	(BOCYL, 2014) Environmental permit granted
image002	Image of the project
AIG.200046-PROYECTO-ESCOMBRERA-BARRUECOPARDO-SALORO	(Sadim, 2021) Waste Storage extension application
C.E. BARRUECOPARDO, Nº 6.432-11 PROYECTO DE EXPLOTACIÓN	Application for permit for Exploitation of the project (Sadim, 2012)
ANEXO 11 - ESTUDIO HIDROGEOLÓGICO	(Otero Molero, 2012) Hydrogeological Study
Memoria-pag-Saloro-SALORO-2021-FINAL-ENVIADO	(Alejano, 2021) Pit design criteria analysis by UCyL
20136767_Saloro_Open Pit Slope Update Salamanca_23_abril_2020_final version	(Golder, 2020) Geotechnical report
20231109_JORC_Technical_Report_MRE_Barruecopardo_2023_EN_FINAL	(Pohl, 2023) Mineral Resource Estimation
9.Mineral Resource Estimation	(CSA Global, 2012) Mineral Resource Estimation
R166.2012 BAR.BFS.01_Barruecopardo Feasibility Study	(CSA Global, 2012) Feasibility Study
2022 09 01 Tungsten market report price data	Wood Mackenzie, (2022) Tungsten market report
2023_Optimization_EQR Review	Optimization inputs by EQR
2023_Optimization_EQR Review_V0	Optimization inputs by EQR revision
20211108_EQ Resources Tungsten market report_v1	(Wood Mackenzie, 2021) Tungsten market report by Wood Mackenzie
PEAL HISPANIA - ANEXO 8 - Precios	Pit contractor cost by Saloro
PEAL HISPANIA - ANEXO 9 - Revision de precios	Pit contractor cost revision by Saloro
Histórico recuperación	Recovery historical data by Saloro
2023_ Control diario planta	Process Plant Control Workbook by Saloro
2023_ Kevin Datos de espirales Rev. 10a	Spiral Tails performance analyst by Saloro

Document	Description
ENSAYO 1 AMP ESPIRALES MT	Spirals testwork by Saloro
Ensayos control de molienda	Mill testwork by Saloro
Incremento de recuperación	Recovery ramp-up evaluation by Saloro
Rgh Tables 2023_ Seguimientos mesas grueso y fino Rev.3	Particle size workbook by Saloro
Informe equipos de ciclonado Final	Cyclones testworks performance and analysis report by AMP & Saloro
CERTIFICATE OF ANALYSIS (SALORO ASSAYS) _(112_230101_20_W)	(Saloro, 2023) Ore concentrate analysis results 112
CERTIFICATE OF ANALYSIS (SALORO ASSAYS) _(114_230103_20_S)	(Saloro, 2023) Ore concentrate analysis results 114
CERTIFICATE OF ANALYSIS (SALORO ASSAYS) _(124_230303_20_X)	(Saloro, 2023) Ore concentrate analysis results 124
saloro_202310_res_rot.mdl	Resource block model file
topo_jun23_v2pt.dtm	Topography used in Resources Block Model
EXC_Diciembre2023_TOTAL_3D.dxf	December 2023 Topography, used to deplete the block model for optimization
EXC_Agosto2024_TOTAL_3D.dtm	31 August 2024 Topography update for depletion prior to final optimization runs
ROM_30092024	Ore stockpile inventory map

3 Mineral asset

This section summarizes the historical mining activities performed at the deposit since the early 20th Century, the current ownership and operations and permitting.

3.1 Historical mining activity

Tungsten mining in the area dates to the beginning of the 20th Century, reaching a peak during the years 1914 -1919 and then stopping before the Second World War. Thereafter, production fluctuated with the main producer being Coto Minero Merladet, with open pit mining active until 1982.

Previous mining at Barruecopardo has historically focused on two main zones: the Filon Maestro Zone, developed in the northwest of the project area; and the Filon Principal Zone which is the focus of the most recent open pit operation. The terms Filon Maestro and Filon Principal are historical terms which no longer directly apply and do not correlate with the current resource estimate.

The Barruecopardo Mine was one of Europe's largest tungsten producers and produced a high quality scheelite concentrate. When operational, Barruecopardo produced around 500,000 to 600,000 tonnes per year of process plant feed, with a maximum production rate in the 1970s of 800,000 tonnes per year, at an average grade of 0.08% WO_3. The low grade resulted from all mined material – both ore and waste - being fed to the process plant due to an inflexible materials handling system in use at the time. The gravity processing plant of the time had a capacity of 150t/h. There are no accurate production records available from the time of this open pit operation, which was run by a private company.

The last open pit mining was in 1982, with and production continuing during 1983 and 1984 by feeding from stockpiles. The open pit was then allowed to flood and the old mine buildings mostly removed. Old waste dumps and tailings occupy the area immediately to the south of the pit.

3.2 Ownership structure and acquisition history

In the mid to late 1990s A pre-feasibility study was commissioned by Coto Minero Merladet to establish the viability of restarting the operation by extending the open pit to the north, mining known mineralised material located below the crusher station in the old operation, and underground mining. There are no known exploration data from previous work at Barruecopardo. An exploration programme was carried out by Minera del Duero S.A. over the Valdegallegos prospect, to the west of Barruecopardo, but no details of this programme are available.

The Investigation Permit (IP) “Saldeana” which covers the Barruecopardo Project location, was granted to the Sociedad de Investigación y Explotación Minera de Castilla y León (SIEMCALSA) in 2001, for the investigation of gold mainly.

SIEMCALSA retained the tenement for years by applying for extensions of the IP. In 2011 SIEMCALSA and Saloro agreed to the transfer of the IP such that Saloro became the titleholder of the IP. With this agreement Saloro gained 90% interest in the project and SIEMCALSA the remaining 10%. A later agreement between Saloro and SIEMCALSA for the remaining 10% resulted in SIEMCALSA completely exiting the Barruecopardo project.

Ormonde Mining PLC (an Irish mining company listed on the London and Dublin stock exchanges) acquired Saloro SLU. in 2008. Detailed feasibility studies, and applications for various operating permits followed in the 2009 through 2014 period.

In 2015 Oaktree Capital (Oaktree) acquired 70% of Saloro from Ormonde, with Ormonde retained as the project managers. This enabled the project construction to be initiated in 2018, with open pit operations beginning in 2019. In 2020 Oaktree acquired the remaining 30% to complete their 100% ownership of the Barruecopardo Project.

In August 2023 EQ Resources Limited (EQR) acquired a 100% interest in Saloro from Oaktree, Oaktree remains a substantial shareholder in EQR, as a result of the transaction.

3.3 Previous work by MiningSense at Barruecopardo mine

MiningSense began the relationship with Saloro in 2018 by reviewing the pit designs to reduce the initial strip ratio during the first years of the pit development.

Since then, MiningSense has been involved in the project by producing monthly and annual mine plans, with regular visits to the Barruecopardo mine.

In 2022-2023 MiningSense also developed the geotechnical monitoring program for the Barruecopardo open pit slopes. Following that MiningSense collaborated with Dr. Leandro Alejano to assess the optimum slope angles for the Barruecopardo pit.

3.4 Mineral tenure, permits and permissions

3.4.1 Exploitation Concession

Barruecopardo permit was submitted for approval on the 11th of January 2011 and was granted on the 19th of December 2014 via the “Concesión de Explotación Barruecopardo” (C.E. BARRUECOPARDO Nº6.432-10). This allows extraction of section C minerals for 30 years, being renewable two times for the same period. It is owned 100% by Saloro SLU. with no restrictions within the Permit. Scheelite being a section C mineral.

The area of concession covers 6.052km^2 and is shown in Figure 3-3. This is as outlined in the Mining License Application (Proyecto de Explotación), submitted in 2012 by Saloro, and authored by Sadim (Spanish consulting firm).

3.4.2 Environmental permit

On the 16th of January 2014 the Environmental Permit was granted for the Barruecopardo Exploitation Concession in the "Declaración de Impacto Ambiental" (DIA) and published on the 6th of February 2014 in the "Boletín Oficial de Castilla y León" ORDEN FYM/2014.

The deposit is located within the Nature 2000 area and restrictions exist in terms of bird life protection, such that Saloro works closely with the Environmental authority's department as to the application of their regulations in the ongoing operations. Since mining began 2018, and processing in 2019 there has not been any negative findings, complaints or non-compliances with respect to the existing environmental permits.

Saloro SLU applied for authorisation to modify the tailings storage footprint on the 6th of March 2021, this being granted on the 15th of November 2021. This is shown in Figure 3-1.

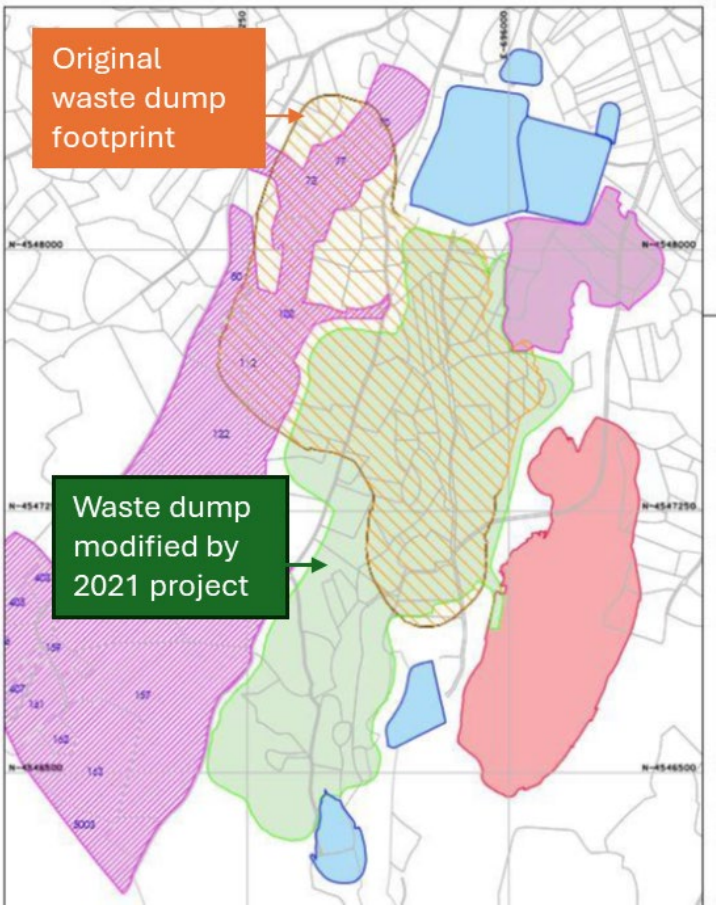


Figure 3-1 Waste dump modified by 2021 modification

As described in chapter 9 on waste storage, a new application is required in 2024 to further alter the waste storage footprint and permit. This application will require an Environmental Impact

Assessment review. However as explained elsewhere in this report, there is no reason to believe this will not be granted.

3.5 Location, accesses and surface layout

The Barruecopardo project is in the municipality of Barruecopardo, Figure 3-3, in the Salamanca Province of the Castilla y León region in Western Spain. This is 260km WNW of Spain's capital Madrid and close to the Portuguese border. The mine is 4 Kms south of Barruecopardo village and is accessed by the public roads DSA-573 and DSA-570 public roads as shown in Figure 3-3. These roads connect through with the town of Vitigudino (population2,700), and through to the regional capital of Salamanca (population 150,000) 95 Kms from the mine.

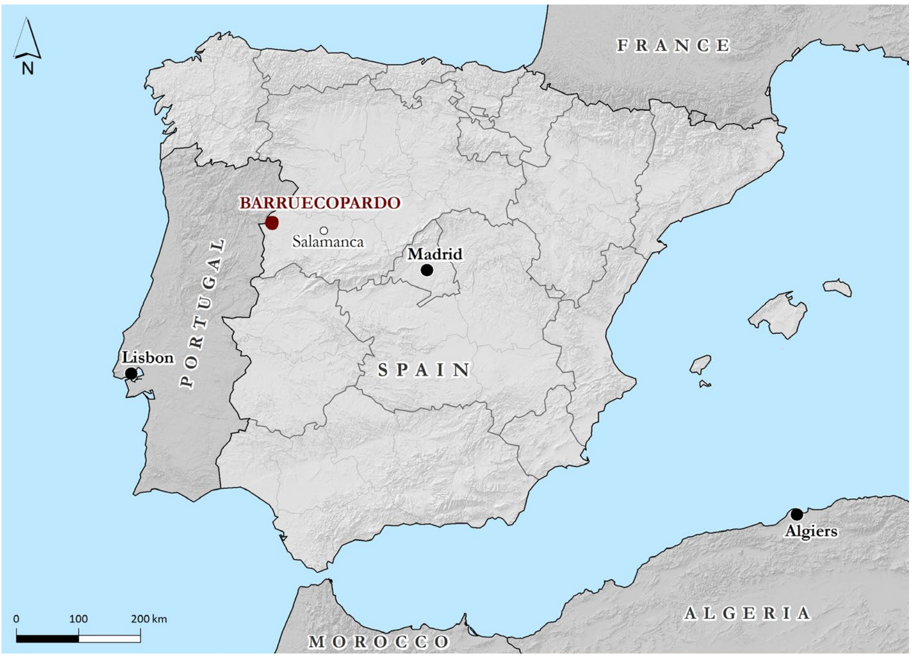


Figure 3-2 Barruecopardo Regional Location

The site map including the physical lay-out is shown in Figure 7-19, later in this report.

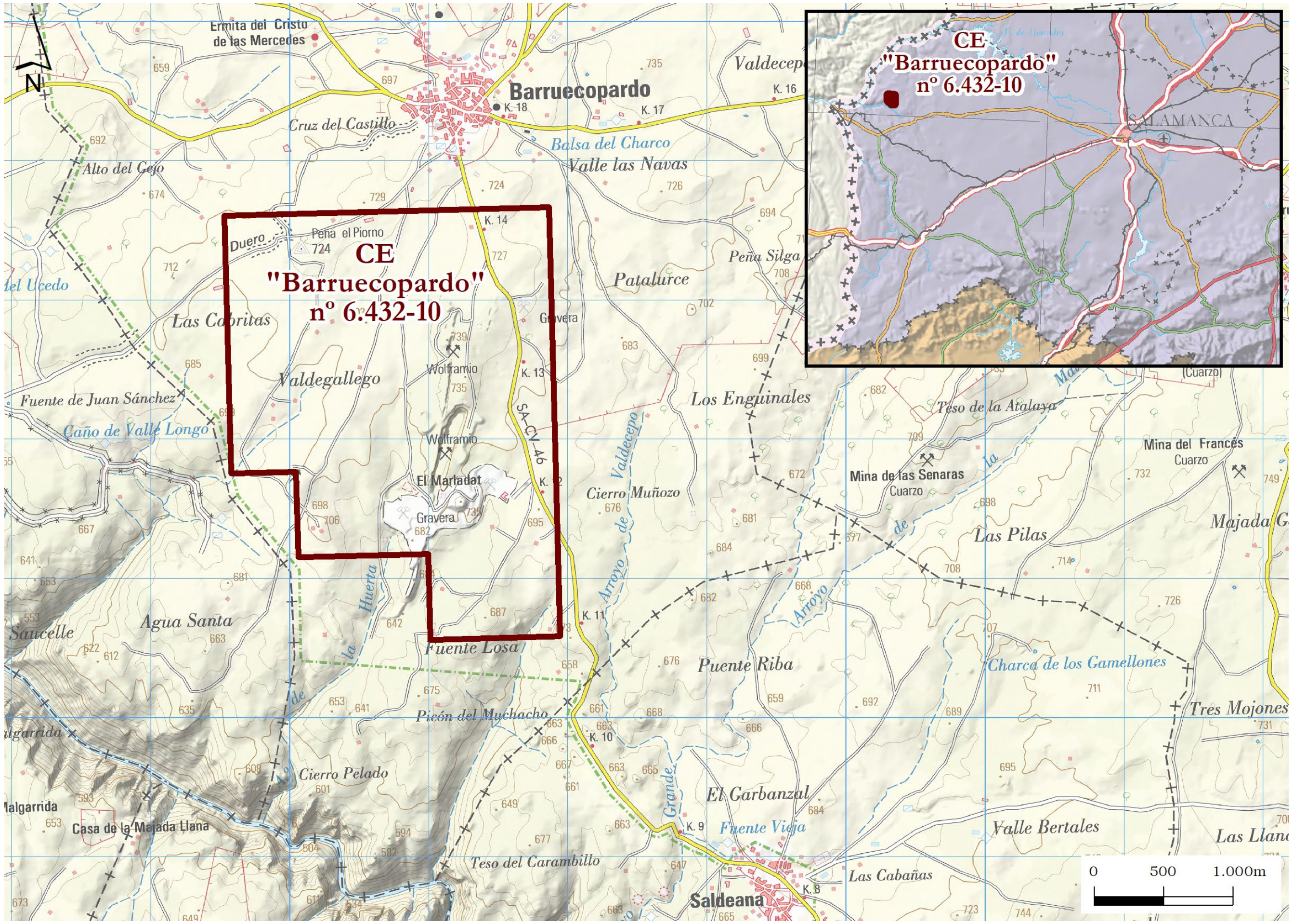


Figure 3-3 Barruecopardo Location

3.6 Mining methodology

3.6.1 Operation description

Mining is carried out by a contractor responsible for: Drill and blast, load and haul, maintenance of roads and sumps, and refeeding from the ROM stockpiles into the ROM Ore bin to feed the primary crusher. All ore goes through the stockpiles, with no direct truck dumping into the ROM hopper. All waste goes to the ex-pit waste storage facility immediately to the west of the pit. All mine waste has been characterised as Non-Potential Acid Forming. Dried tailings from the concentrator is co-disposed inside the waste storage facility, along with the run-of-mine waste.

Saloro, as the owner, provides overall supervision, and mine technical services such as resource estimation, grade control in—pit, and pit design. As well Saloro directly conducts the progressive rehabilitation of the waste storage facility. Saloro operates the processing plant and uses a separate contractor for the offsite truck transport of concentrate as final product.

The mining equipment fleet used for the project is detailed in Table 3-1.

Table 3-1 Mining Equipment

Type	Model	Capacity	Type	Model
Excavators (backhoe loader)	KOMATSU PC1250-7	120 T	Bulldozer	CAT D8T
	KOMATSU PC1250-11	120 T		CAT D8T
	CAT 6015BH	150 T		CAT D8T
Auxiliar excavators	KOMATSU PC 450-7K			KOMATSU D155A-3
	HITACHI ZX350		Loader	CAT 988F
Auxiliar trucks	CAT 740	40 T		CAT 972G
	CAT 740	40 T		CAT 980K
Trucks	KOMATSU HD785-7	100 T		CAT 988K
	KOMATSU HD785-7	100 T	Drilling	TAMROCK PANTERA 1500
	KOMATSU HD785-7	100 T		SANDVIK DP1500
	KOMATSU HD785-7	100 T		EPIROC SMARTROC T45
	CAT 777G	100 T		SANDVIK DP1500 IS5
	CAT 777G	100 T		SANDVIK DP1500 IS5
	KOMATSU HD785-7	100 T	Grader	CAT 16G
	KOMATSU HD785-7	100 T	Auxiliary equipment	IVECO MP380E44W
	KOMATSU HD785-7	100 T		MAN 18285LC
	KOMATSU HD785-7	100 T		CAT 775D
				CAT 777C

*The water is supplied with a small deposit

The water used in the operation comes from the mine drainage system, stored in various ponds depending on the intended use. Water for plant operations is pre-treated, while untreated water pumped from the bottom of the pit is used for dust suppression and rehabilitation.

Electricity for the project is supplied through an external power line (45 kV) connected to an internal substation that distributes electricity throughout the site at 13.4kV. There is no power generation onsite at the project.

The main electricity needs are in the plant area where the principal infrastructure is located. The electrical needs for the pit, such as pumping of the mine water, are supplied by mobile diesel generator sets.

Blast patterns are designed based on the geological model and planning to separately identify the ore from the waste. Ore blasts are at 5-metre intervals to avoid dilution, while waste blasts are at 10-metre intervals to improve efficiency. Once the blast polygons are defined, they are marked on the bench, and the blasts initiation sequence is controlled to separate the different material categories.

The mine works two 12-hour shifts Monday to Friday, with a 12-hour shift on weekends. Generally, day shift operates 1 excavator plus two drills, and the night shift operates two excavators and one drill. The shifts and the equipment per shift may vary depending on the operational needs

3.6.2 Grade control methodology

The LG and HG definition by Saloro uses the cut-off for HG as 0.15%WO_3.Grade control operates to provide quality control for the crusher feed. The process is summarized below.

Phase 1: Geological Resource Model

The geological resource model is used as a basis for grade control, with modifications made based on the results obtained from operational sampling and the reconciled mineral estimation of the benches immediately above.

Phase 2: Grade Control Model

A visual analysis of the blast holes in all potential ore areas is carried out, using UV lamps to identify mineralization. Positively identified drill holes are then analysed in the on-site laboratory to determine the grade of each blasthole. A turnaround time of 1 to 2 days is typical to get the results from the laboratory. This time lag does not impact on production as grade control drilling is conducted far enough in advance. After the blast hole results have been received, the final blast design polygons can be defined, along with the initiation sequence. Then the blast is loaded and detonated. The drill hole laboratory results are loaded into a short-term version of the resource model, called the grade control model.

The assay results are grouped graphically, dividing the blasting area in separate polygons that correspond to the stockpile destination definitions. Post-blast reviews of polygon movement are conducted, using the UV lamps and visual control of scheelite, to assess shape movement from blasting. The polygon shapes are then adjusted accordingly prior to excavation. The blast polygons are evaluated separately to assign its' grades and select the destination of each polygon.

Phase 3: –Blasting Control - OrePro

The OrePro software is used to predict the movements of the blast and define the polygon boundaries, as well as to estimate the grades that should result after dilution and losses associated with the blasting. After reviewing the drill holes and adjusting the mineral polygons in terms of contour and grade, blasting is carried out.

Once the blast is fired, the surveyed topography showing the blasted material heave pile is loaded into OrePro to reevaluate the translation of the polygons. This system helps to reconcile the material selected for stockpiling with the initial material as defined by the blastholes assays.

Phase 4: In Situ Review – Loading

The polygons generated by the post-blast review in OrePro are marked out in the field, and inspection with UV lamps. If necessary, the boundaries of the polygons are modified. If required, the revised contours are reassessed with Datamine to determine the grades based on the dimensions of the updated polygons. Excavation and loading of the polygons are organized by ore category, taking into account the number of trucks and their corresponding tonnage.

No sampling is done of the production faces on regular basis, due to safety issues and rock hardness, although lately the veins are being mapped.

The historical reconciliation between grade control and resource model has been improved over the years, according to Saloro. The comparison over the different years/benches/months is directly done by the Saloro Geology team.

Phase 5: Stockpiles

The material is classified into five categories:

- **A+:** Ore with a grade higher than 0.15% WO_3 and high sulphide content.
- **A-:** Ore with a grade higher than 0.15% WO_3 and low sulphide content.
- **B+:** Ore with a grade between 0.07% and 0.15% WO_3, and high sulphide content.
- **B-:** Ore with a grade between 0.07% and 0.15% WO_3, and low sulphide content.
- **OP**: Ore assigned outside the geological model according to grade control.
- **MAR**: Ore with a grade between 0.07 and 0.05%

  The material is stockpiled according to its previously defined category for separate reclaim and further processing in the primary crushing. The nominal grade for each stockpile is an average grade of the stockpile, being the result of the material that has entered.

The volume of the stockpile is calculated by topography, and the density of the stockpile is assumed at 2.26t/m3, based on a previous test. The test was done few years ago and checked against truck counts at nominal payload measured against the volume of the cone produced after dumping. The trucks do not have weightometers.

It is the opinion of MiningSense that density testing of the stockpiles should be done on regular basis.

In terms of grade, no sampling is done on the stockpiles: the grade is calculated based on the number of trucks coming from each blast polygon to which an average grade has been assigned in the grade control. The mine does not use destination controls in a electronic Fleet Management System, so truck counts by destination are taken from operators records.

Phase 6: Feed to Primary Crushing

The material used for feeding the primary crushing is selected based on the plant's needs, balancing the WO_3 grades and sulphide content to avoid operational issues. The crusher is fed with the material previously stockpiled and all the material feeding the crusher passes through one of the stockpiles. There is no direct tipping of mine trucks into the primary crusher bin.

3.7 Historical Ore Reserves Estimates

CSA Global made several Mineral Resource Estimations and technical reports during 2007, 2008 and 2010.

The Definitive Feasibility Study by CSA Global Resources in 2012 is based on the Mineral Resource Estimation Statement done by them the same year. This reports 5.5Mt Measured ore with average grade of 0.34% WO_3, 12.3Mt Indicated ore with average grade of 0.26% WO_3, and 9.6Mt of Inferred ore with average grade of 0.23% WO_3.

The Exploitation Project application signed in 2012 to the Spanish authorities for project permitting with a total of 5.20Mt of measured resource category in the production plan at an average grade of 0.37% of WO_3, 2.87Mt of indicated resource category in the production plan at an average grade of 0.32% of WO_3. And includes 0.81 inferred resource category at an average grade of 0.24% of WO_3. It means a total of 8.07Mt of ore reserve corresponding 5.20Mt proven reserves at an average grade of 0.37% of WO_3 and 2.87Mt probable reserves at an average grade of 0.32% of WO_3. This Exploitation Project doesn't specify ore reserve estimation under any standardize code of ore reserves reporting.

This is the last publicly released ore reserve estimate, prior to this 2024 ORE estimate by MiningSense.

4 Mineral Resource Estimate

This section is based on the document “JORC TECHNICAL REPORT Mineral Resource Estimation of Barruecopardo Tungsten deposit”, prepared by Jörg Pohl (EurGeol. #1728) for SALORO SLU. in November 2023.

4.1 Introduction

4.1.1 Background

The first JORC report on this deposit, presented by CSA in 2012 was based on the results of 83 diamond holes (DD), drilled between 2006 and 2011 in close distance to the historic pit wall. In 2012 and 2015, 7 more DD holes were added, testing the eastern extension of the deposit. In 2019 a short-hole drill campaign took place with 27 diamond holes in phase 1 area, to investigate structural control, using an acoustic televiewer. In 2021 and 2022, 13 DD hole have been drilled and between 2022 and 2023 another 13 DD holes have been added, to investigate continuity at depth. This sums up to a total number of 143 DD holes. After every drill campaign, the initial block model has been re-estimated in the new areas, to create updated estimates, for an internal purpose. In parallel, grade control models have been prepared using exclusively the 378 reverse circulation holes (RC) that have been drilled for this purpose between 2018 and 2020, targeting the areas to be mined immediately.

The holes drilled between 2021 and April 2022, had the objective to investigate several deeper levels of the deposit and to explore previously undrilled areas. This phase of the mine is referred to as “Phase 6”. For that MRE (May 2022), as well as all previous resource estimations only the diamond drill holes have been used.

4.1.2 Scope of work of MRE

After finalising 13 more diamond holes in May 2023, drilled in areas 6 and 7 of the deposit, and the reception of all chemical assays, Saloro SLU. requested a mineral resource update to evaluate the remaining resources of the Barruecopardo deposit in June 2023.

That technical report aims to cover all areas of the mining operation, with focus on the Mineral Resource Estimation, such as:

- QAQC and interpretation of all the assay data received from Saloro
- Construction of grade wireframes using the entire DDH and RC dataset
- Extraction of data falling inside the new wireframes
- Statistical analysis (KNA, grade distribution, top cut discussion, variography)
- Ordinary kriging of WO_3 composites into 6x6x5m parent blocks, allowing sub-blocking to 1.5x1.5x5m
- Inverse distance squared (ID2) estimation of the deleterious elements As, P, S
- Model validation
- Resource Classification

4.2 Overview of geology and mineralisation

The deposit area is part of the Central Iberian Zone (CIZ) of the Iberian massif. The basement rocks are formed of two discordant overlaying metasedimentary units and a large volume of granitic variscan rocks that intruded into those metasediments.

The Palaeozoic metasediments are part of the Shist-Grauwacke Complex (CEG) divided into "Complejo de Alamo and the Upper Serie" and secondly a series composed of Quartzites and shists, aged lower Ordovician.

Predominant rocks in the area are massive intrusive granites and a metamorphic sediment sequence. The granite intrusions took place during the variscan age (326-311 Ma) and have been deformed during the variscan orogeny, with later reactivations during the alpine orogeny. The sediments are of Palaeozoic age.

All rocks are heavily deformed, showing 3-4 deformation phases. Mayor orientations trending NNE-SSW (10-40º) and NW-SE (120-140º).

4.2.1 Regional geology

The area of Barruecopardo is shown on the Vilvestre 1:50.000 map from IGME, the Spanish Geological and Mining Institute, number 449.

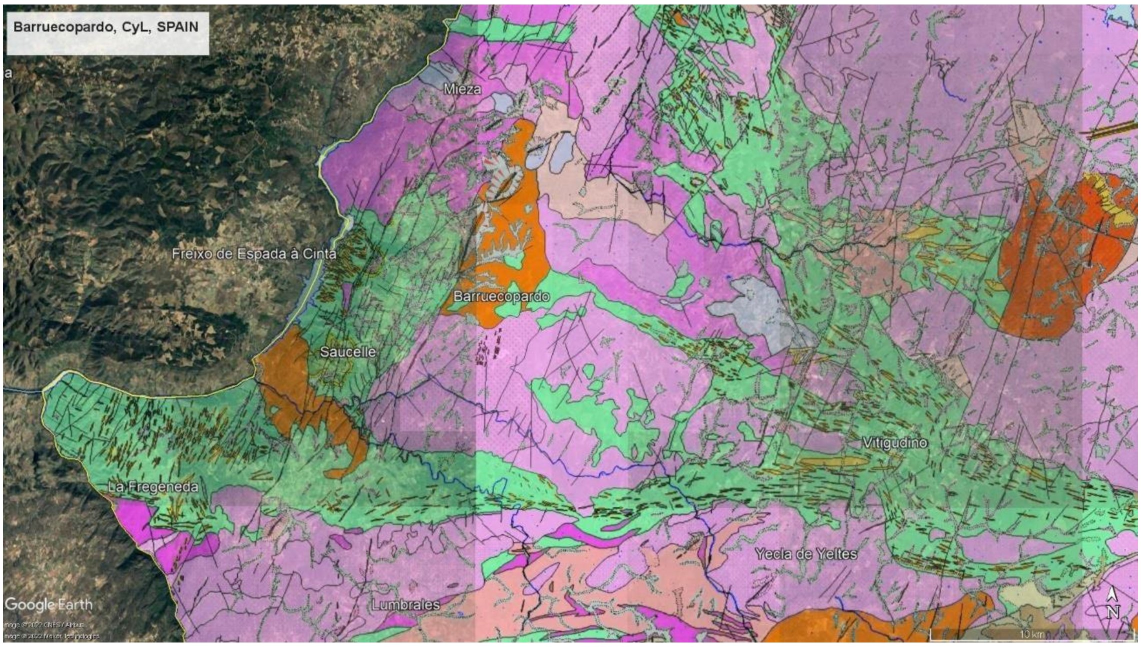


Figure 4-1 Regional Geology Spain (IGME) on Google Earth

Predominant are the different granite units from orange to pink colours and the shists of the CEG, the shist greywacke complex in green.

4.2.2 Deposit geology

On a deposit scale, all mentioned lithologies are present. Most significantly and well visible in the open cut are the veinlets containing the Scheelite and Wolframite mineralisation. These target formations are interpreted to be extensional, dilatational structures.

In several studies and constant geological and structural work by the Saloro geologists, their sub verticality and continuous alignment has been demonstrated with the deepening of the open pit operation.

Four main units are present (see map below):

- 13: Granite "Ala de Mosca", of medium to large grain size
- 14: Zone of occurrence of quartz dikes, and 14a pegmatites
- 18: Granite of Barruecopardo
- 19: Metasediments (pellitic-psamitic) with quarzitic intercalations

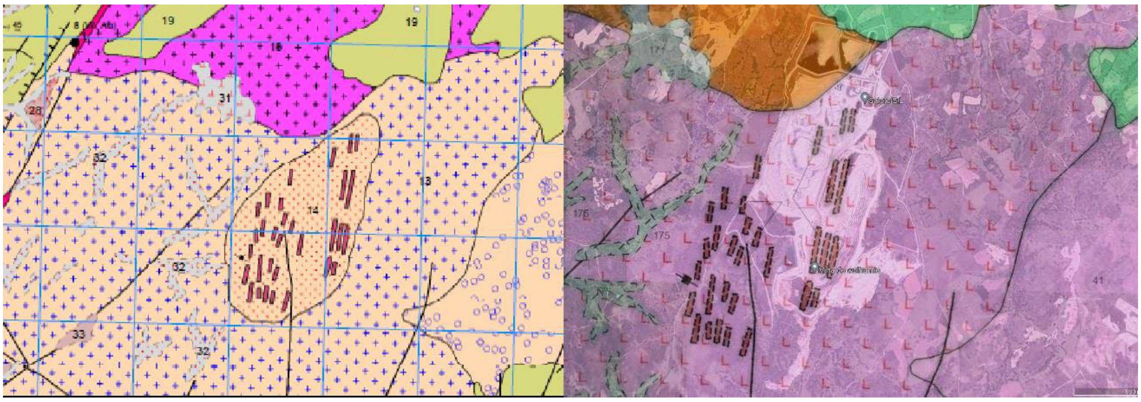


Figure 4-2 Barruecopardo mine on Geological map IGME (left) and geology superimposed on Google Earth

In Figure 4.2, the air picture shows the mine area with its main target being the pegmatites, aligned 15ºNNE. West of the open cut is another area with abundant pegmatites which might indicate further exploration potential.

4.2.2.1 Geological model

The Barruecopardo Tungsten mineralisation is hosted within a pegmatitic lens inside a larger granite occurrence called the “Ala de Mosca Granite”. Within this complex a frequent occurrence of quartz veins is present. The mineralised vein swarms observed as narrow sheeted vein systems are interpreted as dilateral structures formed during tectonic activities of variscan age. Those spaces have then been filled during the active period and are the host of mineralisation.

4.2.2.1.1 Structures

Significant tectonic events occurred during the Variscan orogeny, which were then reactivated during the alpine orogeny. Two main orientations of structures exist in the area being NW-SE (mainly dextral) with a general dip of 40-60 degrees towards S-SW. Those are well visible in the

Grauwacke Shist Complex to the West. Secondly and predominantly visible granite complex proximate to the mine area are NNE-SSW (mainly sinistral), dipping steeply to the SSE. Both orientations may show minor vertical movements.

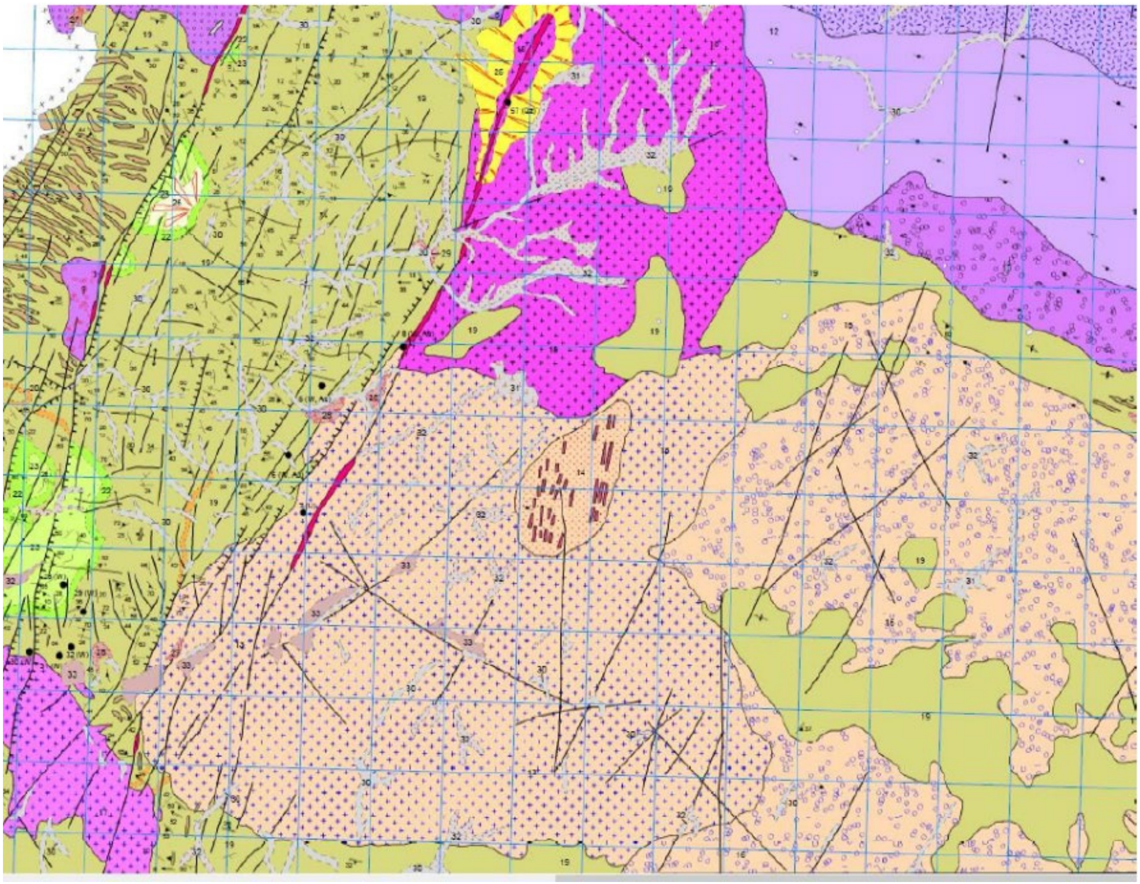


Figure 4-3 Extract from MAGNA50 sheet 449 "Vilvestre" with the Barruecopardo deposit area in the centre

With the mine site in the centre of Figure 4.3, the orientation of the main structures indicated by IGME (Instituto Geológico y Minero de España) on the 1:50k geological map. Their main orientations are: NNE-SSW and ENE-WSW.

4.2.2.1.2 Mineralisation

Mineralisation occurs within the pegmatitic veinlets cutting through the granite complex.

Two main Tungsten minerals are present. Predominant is Scheelite ($CaWO_4$) which is fluorescent under UV light and to a minor extent Wolframite ((Fe, Mn) WO_4). Other abundant minerals are Quartz, muscovite, pyrite, chalcopyrite and arsenopyrite.

During the geological logging, all samples (DD and RC) are checked under UV light, to detect possible Wolfram mineralisation. Attention is paid to all quartz occurrences with origin from veins, if distinguishable.

4.2.2.1.3 Veins

The mineralised veins are oriented along strike with a main orientation of NNE 10-15º and usually range between 1mm and 10 cm of thickness.

Figure 4-4 Vein swarm within the open pit. Veins marked in blue are mineralised. Dimension from left to right: 3m

4.2.3 Deposit type

The Barruecopardo deposit is interpreted as a sheeted vein system deposit, with its veins being filled after hydraulic fracturing during the orogenic phases.

The predominant orientation of the subvertical mineralised veins is NNE 10-15º, which corresponds to the main stress orientation during the variscan and later the alpine orogeny.

An important role on the system and deposit type has a certain intensity of greizenization in proximity of the mineralised veins.

Figure 4-5 Barruecopardo northern pit wall with subvertical vein swarms and/or fractures (lower picture interpreted)

4.3 Exploration and drilling

4.3.1 Exploration

Exploration has been taken place in form of surface mapping in the prospective northern and southern extensions of the Barruecopardo deposit.

As a result, one DD hole has been targeted in the south extension of the deposit (BD048) and three more into the area of its northern extension (BD045, BD046 and BD047), to serve both purposes, deposit extension drilling and exploration.

All of them showed mineralised intercepts at various levels.

4.3.2 Drilling

In this report it is referred to all diamond drill holes (DD), and all reverse circulation drill holes (RC) drilled by Saloro since 2006 and until May 2023, being the latest holes drilled so far.

Specific QAQC procedures and protocols are in place and followed by Saloro personal concerning drilling, logging, sampling, and data entry, and can be reviewed in several internal documents such as “QAQC Protocol Saloro 2019” or “Core Drilling May 2021”. Those are discussed throughout the following chapters.

4.3.2.1 Drilling methods

Two drilling methods are used, Diamond drilling (DD) and Reverse Circulation drilling (RC).

4.3.2.1.1 Diamond drilling

Diamond drilling, with wireline core retrieval. Predominant core diameter is HQ (63.5mm) nominal core diameter. Occasionally PQ diameter 85mm has been used to drill the top hole.

4.3.2.1.2 Reverse circulation drilling

Reverse Circulation (RC) drilling was employed for grade control precision drilling, using suitably sized compressors in combination with a 140mm diameter face sampling hammer.

4.3.2.2 Drill sample recovery

Saloro DD typically recorded overall core recoveries more than 90%, which is considered acceptable.

Saloro RC drill samples are collected over 1m intervals through a cyclone. Plastic sample bags are strapped to the cyclone to maximise sample recovery. Individual sample bags are not weighed to assess sample recovery, but a visual inspection is made by the Company geologist to ensure all samples are of approximately equivalent size. All inspections for recovery are considered as appropriate.

4.3.3 Sample preparation and analysis

The detailed sample analysis is described in the MRE report; in this case, a few brief notes are made.

Designation of sample intervals is visual from drill core following geological aspects and with help of UV light in the core shed, to detect the fluorescent tungsten mineral scheelite. Sample intervals of 1m are preferred. The selected intervals are cut into half core and sent for analysis to the internal lab, where they are prepared for pressed powder pellet XRF analysis.

A QAQC protocol has been adapted by Saloro for all assay stages, which includes blanks, standards, sample duplicates and lab pulp duplicates. Results are acceptable for RC samples. DD duplicate analyses are challenging. It is interpreted that the reason for this low correlation between quarter core samples is the high nugget value.

- Correlation of the quarter core sample duplicates is low for the totality of the samples. Due to the small number of samples not all grades are covered to generate better information. Nevertheless, the elevated nugget value is well reflected by those results, and they are thus considered as acceptable. RC samples show good correlation between the sample and a duplicate sample taken from the same bag.

- Correlation of pulp duplicate are considered acceptable for both DD and RC.
- DD and RC blank samples show both acceptable results with 6% and 5% respectively slightly above the detection limit of 0.002% WO_3, as communicated by the lab.
- The results of umpire samples are considered as good and do not indicate issues with analytical grades.

4.4 Estimation and reporting of mineral resources

The MRE for the Barruecopardo deposit has been reported based on the guidelines defined in the JORC code (2012 edition). The MRE has been classified as a Measured, Indicated and Inferred Mineral Resource of 24.4 Mt at an average grade of 0.195 % WO_3. The following table reports the MRE using a 0.05%WO_3 cut-off grade, all values in the table are rounded to reflect confidence levels in the estimate.

Table 4-1 Barruecopardo Mineral Resource Estimate as of 9th November 2023

Category	Tonnes (Mt)	Grade (WO_3 %)	Contained Metal (t of WO_3)
Measured	10.05	0.191	19,204
Indicated	10.46	0.174	18,200
Inferred	3.86	0.259	9,993
Grand Total	24.37	0.195	47,527

For this resource estimation and with the aim to upgrade the deposit, all RC holes and all DD holes drilled by Saloro since 2006 have been used. Special attention was given to the DD holes drilled since May 2022. These aimed to fill existing gaps or extend known mineralisation in the upper part of the deposit and to better inform the deeper areas of the Barruecopardo prospect.

4.4.1 Data integrity

All geological and chemical data, as well as collar coordinates and drill hole deviations have been validated for this MRE. The entire DD and RC dataset is considered to be of good quality and has been used for this estimation.

All data used for this MRE has been supplied by Saloro. Some new drillhole data originates from the 13 diamond holes drilled since May 2022. The topography used for this estimation is the latest topography from June 2023.

4.4.2 Database

A breakup of those drillholes, samples and the time they were drilled is tabulated below (Table 4.2).

Table 4-2 Drillhole statistics (*av. depth calculated only for DD holes and excluding 2021-22 short holes)

Hole type	No. of holes	Metres drilled	Av. depth	No. of samples	Areas drilled	Year drilled
DDH	57	11,033.05	194	6,066	all	2006-2007-2008
DDH	33	7,716.80	234	1,353	all	2010-2011-2012-2015
RC	378	17,456.00	46	11,662	1-2-3-4-5	2018-2019-2020
DDH	27	451.25	17	468	1	2019-2020
DDH	13	4,013.90	309	1,578	6	2021-2022
DDH	13	4,772.40	367	1,510	6 and 7	2022-2023
Total general	521	45,443.40	276*	23,637		

4.4.3 Comparison RC vs. DD samples

For this report all available samples RC and DD samples have been used. This is different to earlier estimations, where for the resource model only DD holes were used and for the grade control model only the RC sample data was used. To validate this step, both datasets have been analysed before compositing to 5m composites.

Table 4-3 Basic statistics DDH and RC initial 1m samples

All samples	DDH&RC	only DDH	only RC
mean	0.126	0.152	0.099
error	0.005	0.008	0.005
standard deviation	0.53	0.64	0.38
sample variance	0.28	0.41	0.14
curtosis	214	162	278
coeff. of asymmetry	12.07	10.64	13.43
min	0	0	0
max	16.505	16.505	10.574
no. of samples	12197	6287	5910
confidence level (95%)	0.009	0.016	0.01

Table 4-4 Basic DD 1m sample domain statistics

DDH samples	DDH_D1	DDH_D2	DDH_D3	DDH_D4	DDH_D5	DDH_D6	DDH_D7	DDH_D8	DDH_D9
mean	0.049	0.083	0.098	0.175	0.149	0.093	0.133	0.173	0.193
error	0.014	0.016	0.026	0.012	0.018	0.034	0.042	0.043	0.055
standard deviation	0.17	0.4	0.35	0.64	0.66	0.5	0.45	0.96	0.74
sample variance	0.03	0.16	0.12	0.4	0.43	0.25	0.2	0.93	0.54
curtosis	32	158	58	114	106	121	35	184	32
coeff. of asymmetry	5.47	11.46	6.97	9.07	9.28	10.28	5.57	12.38	5.47
min	0	0	0	0	0	0	0	0	0.001
max	1.218	6.207	3.531	11.829	10	6.356	3.506	16.505	5.208
no. of samples	144	624	187	2938	1380	211	115	508	180
confidence level (95%)	0.028	0.031	0.051	0.023	0.035	0.068	0.083	0.084	0.108

Table 4-5 Basic RC 1m sample domain statistics

RC samples	RC_D1	RC_D2	RC_D3	RC_D4	RC_D5	RC_D6	RC_D7	RC_D8	RC_D9
mean	0.019	0.019	0.034	0.138	0.066	0.005	0.002	0.053	0.01
error	0.007	0.004	0.011	0.008	0.006	0.001	0	0.009	0.003
standard deviation	0.06	0.08	0.12	0.47	0.23	0.01	0	0.19	0.01
sample variance	0	0.01	0.01	0.22	0.06	0	0	0.04	0
curtosis	29	78	72	197	137	7	7	51	3
coeff. of asymmetry	5.18	8.36	7.94	11.58	10.05	2.72	-2.63	6.55	1.99
min	0	0	0.002	0	0	0.002	0	0	0
max	0.395	0.909	1.189	10.574	4.036	0.028	0.002	1.931	0.052
no. of samples	73	526	116	3308	1360	29	8	468	22
confidence level (95%)	0.014	0.007	0.022	0.016	0.012	0.002	0.001	0.017	0.006

Analysing the data individually and any of the 9 modelled volumes (domain 1-9), it was observed that both datasets correlate very well with each other and are therefore considered valid to be used as a whole, to estimate the Barruecopardo resource model.

4.4.4 Drill hole and Modelling Extensions

As a reference for drill holes and modelling, the latest topography is used, dating June 2023. The thirteen holes drilled since May 2022 had maximum depths of up to 474m, extending to a total vertical depth of 300m RL. This enabled to better explore areas that only had little information previously.

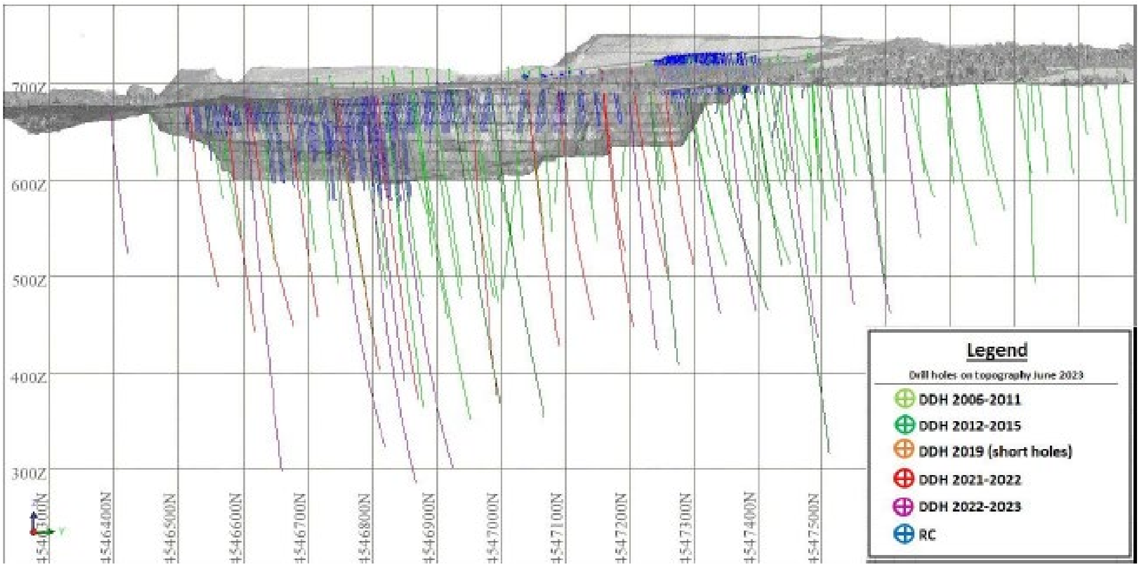


Figure 4-6 Long section SSW-NNE with current topography showing open pit and drill holes (z exaggerated by 1.5)

4.4.5 Estimation and modelling techniques

4.4.5.1 Topography

As a base for topography, the inhouse generated drone-based topography, dated June 2023 was used. Resolution is down to centimetric. Coordinate projection and datum is ETRS89, UTM29N.

4.4.5.2 Wireframes

Wireframes were constructed using the chemical data from the diamond drill holes and the RC holes that where initially drilled for grade control. Lower limit for a sample to be included into a wireframe was 0.04% WO_3, allowing internal but no external wate. A total of nine individual and well-defined wireframes have been constructed around the geological information and respecting 5m composite sample intervals.

Apart from domains 4 and 5, which include more massive mineralisation and some internal waste, the other domains are narrow, likewise respecting the 5m composite length and an SMU of 6x6x5m.

4.4.5.3 Composites

The initial sample composite length of 1m was taken to 5m composites for the MRE. Reason for that was mainly the operational aspect, where it is not possible to mine very thin vein swarms as they occur in Barruecopardo, but rather include those into larger intervals. By doing so, even isolated veins have been integrated into a sample length of 5m, allowing for internal waste if weighted composite grades remain above a nominal minimum grade of 0.05% WO_3.

Challenging with this approach is the geostatistical analysis, due to a smoothing effect over such intervals. To overcome this issue, most of the geostatistical work was done on the initial 1m samples and findings where then applied to the final work.

With the smoothing effect through 5m compositing, no further top cutting has been applied to the composited 5m sample population, where the overall grade was almost identical for both populations but individual 5m composite grades were reduced significantly (see Table 4.3).

4.4.5.4 Block Model

The model is a rotated block model, aligning along with the main orientation of the mineralised vein swarms which is 15º NNE. The rotation is applied around the y axis to minimise any dilution which might occur through misalignment between mineralisation and blocks.

The extension of the block model is approximately 1800m in NNE-SSW direction and 800m across strike in WNW-ESE direction. Vertical extension is between 755m and 300m RL.

Table 4-6 Block Model Extensions

Type	y (ETRS)	x (ETRS)	z (RL)
Minimum Coordinates	4546414	695564	300
Maximum Coordinates	4548178	696386	755
User Block Size	6	6	5
Min. Block Size	1.5	1.5	5
Rotation	15	0	0

The final model is populated with the following attributes per block, shown in the Table 4-7.

Table 4-7 Block model attributes

Attribute name	Type	Decimals	Background	Description
as	Float	3	0.005	Arsenic grade (%) from ID^2 estimation
class	Integer	-	9	1=measured, 2=indicated, 3=inferred, 9=not classified
density	Float	2	0	Density constant of 2.62 g/cm^3
domain	Integer	-	0	Estimation domain / wireframe
p	Float	3	0.004	Phosphorus grade (%) from ID_2 estimation
pass	Integer	-	0	Ordinary Kriging Estimation Pass 1,2,3
s	Float	3	0.005	Sulphur grade (%) from ID^2 estimation
wo3	Float	3	0.002	Tungsten oxide grade (%) from OK estimation

4.4.5.5 Domain statistics

Assay data from all 9 domains was extracted individually and analysed statistically. Those values are displayed in the table below. In reference to 14.3 (Comparison RC vs. DD samples), the data has been analysed individually and as a hole for the 1m and 5m composites.

To be mentioned are:

- Average grade per domain and as a hole is significantly lower than in previous MRE, as the process of differentiation of the mineralised vein swarms is meant to be controlled further down the line through tight soft boundaries (search ellipse) within the domains.
- Curtosis is indicating the “peakiness/flatness” of the distribution of the dataset. With all unsampled intercepts set to background value (0.002% WO_3), this value has increased.
- Coefficient of asymmetry (skewness) is elevated for the same reason as Curtosis. Over 90% of the data within the domain wireframes are below 0.2% WO_3, the dataset has a strong positive skewness.
- The 5m composites used for the estimation are smoothening out the samples to a point, where no further top cut has been applied (see as well 14.6.2). This new approach was requested by the client’s chief geologist. As geostatistically the 1m samples are more representative than the 5m composites, most of the geostatistical analysis was done on the 1m composites. Findings where then applied to the 5m estimation.

Domain 4 has been selected as a base for the estimation and variogram modelling due to its larger sample distribution and for being statistically most representative for the rest of the deposit. The other domains show more irregular distributions or have a smaller number of samples available, which makes the statistical analysis less representative.

Table 4-8 Basic sample composite statistics

1m vs. 5m comps	1m composites		5m composites	
	all domains	domain 4	all domains	domain 4
mean	0.126	0.156	0.125	0.153
error	0.005	0.007	0.006	0.009
standard deviation	0.53	0.56	0.28	0.3
sample variance	0.28	0.31	0.08	0.09
curtosis	214	147	59	49
coeff. of asymmetry	12.07	10.19	6.18	5.49
min	0	0	0	0
max	16.51	11.83	4.53	4.53
no. of samples	12197	6246	2286	1202
confidence level (95%)	0.009	0.014	0.012	0.017

4.4.5.6 Kriging neighbourhood analysis KNA

With the objective to best define the estimation parameters, a kriging neighbourhood analysis using the 1m composites for their better geostatistical representation has been performed, testing different estimation parameters. As the deposit has been estimated and analysed multiple times before, some of the previously parameters have been adapted from earlier estimation processes, or due to general agreements, such as parent block size. The quality indicators, kriging efficiency (KE) and the conditional bias slope (CBS) have been used to determine optimum values.

Significant for new estimations with more samples available and different drill spacing is the number of samples to be used to estimate one block. Too many samples for one block will result in excessive smoothing of the block grades, resulting in an artificially homogenous model. Too little samples per block will result in poor kriging efficiencies and non-representative estimates.

The two main parameters that have been tested is the minimum/maximum number of samples and the dimension of the search ellipsoid, which is defined by the range of the model. Further tested were maximum samples per hole, maximum vertical distance, discretisation points and sub block size.

Then, those preferred parameters have been applied to the final estimation using the 5m composite samples.

4.4.6 Resource estimation method

The software package used to perform the resource estimation is Surpac Geovia.

The model has been built to include all DD and RC drill holes in proximity of the Barruecopardo open pit operation and within its mining concession. The model is a rotated block model, to line up with the direction of the mineralised vain swarms, striking at 15º NNE. Parent block size is 6x6x5m (x-y-z), allowing two times sub blocking in x and y direction, for a maximum resolution of 1.5x1.5x5m subblocks.

Tungsten was interpolated using ordinary kriging (OK) in a three-pass estimation process, with an ellipsoid opening after every pass, to include a larger volume within every individual mineralised wireframe. A background value of 0.002% WO_3 has been assigned to all blocks below surface as a "waste rock" value, before the estimation.

The composite grades were analysed individually by domain. No top cut value has been applied to the composites. This change in methodology is mainly due to the fact that for the estimation, 5m composites were used, instead of 1m composites previously. As grades are smoothed out during the compositing process from 1m to 5m and including barren areas, no further cut in grade is being applied.

The resource estimation method consists of the following points: separate validation of deleterious elements, application of top cut to avoid a nugget effect, definition of ordinary krigging parameters and explain the estimation process. It is explained in detail in section 14.6 of "JORC TECHNICAL REPORT Mineral Resource Estimation of Barruecopardo Tungsten deposit" dated 2023.

4.4.7 Classification

The choice of the appropriate category of Mineral Resource depends upon the quantity, distribution and quality of data available and the level of confidence that attaches to data.

The current estimation of the Barruecopardo Tungsten deposit is based upon on criteria defined in the JORC Code (2012 Edition), such as:

- Confidence in the geological model
- Drillhole spacing
- Data and/or sample spacing
- Data Quality (QAQC)
- Geostatistical analysis and geostatistical indicators generated during the MRE
  Experience and lessons learned from, and in comparison, with earlier MRE

4.4.8 Use of geological criteria

Geological and structural criteria was considered during the construction of the estimation wireframes. Internal structural data and findings from other studies raised confidence on the orientation of the wireframes.

4.4.9 Tonnage factors

Tonnage was estimated using the in situ dry bulk density value of 2.62g/cm3 for the entire deposit.

4.4.10 Validation of resource estimation

The estimation has been validated in four steps:

- Comparison of initial and final grades
- Comparison of composite and block model grade distributions (histograms)
- Looking at trends (swath plots)
- Section by section (visually)

The complete validation of resource estimation is shown in section 14.10 of "JORC TECHNICAL REPORT Mineral Resource Estimation of Barruecopardo Tungsten deposit" dated 2023.

5 Geotechnical assessment

Saloro SLU. requested Leandro Alejano (Professor of Rock Mechanics - School of Mining and Energy Engineering - University of Vigo) to carry out a geomechanics stability study of Barruecopardo open pit slopes, to a target depth of 290 m. This section summarises the analyses, results and conclusions of the original report: *"Report of the slope stability in deepening the Barruecopardo mine to 290m"* or in Spanish *"INFORME DE ESTABILIDAD GLOBAL DE LOS TALUDES DE LA MINA BARRUECOPARDO PARA SU REPROFUNDIZACIÓN HASTA 290 m*", dated March 2024.

5.1 Background and scope

This latest report is the basis on which the 2024 MinignSense ORE report is based. It also describes the different approaches through time for the slope configuration at the Barruecopardo open pit.

The significant geotechnical pit slope studies for the Barruecopardo open pit have been:

- Feasibility Study Barruecopardo Tungsten Project Spain – By Clayton Reeves. CSA Global (UK) (CSA). April 2012.

Features of the pit design included a bench height of 10m and a batter angle of 70º, with geometric differences in the east and west. The inter-ramp angle on the west was designed at 55° but incorporated a double-benching system whereby alternate berms are 5m and 2m wide to accommodate the 70° bench face angle. This configuration was adopted on all walls except the east wall, which was designed at 50º and maintained 5m wide berms. Regarding the ramp, it was designed with grade 10 and a ramp width of 15, 20 and 25m.

- C.E. BARRUECOPARDO, Nº 6.432-11 PROYECTO DE EXPLOTACIÓN. Sadim. July 2012.

The features of the pit design are the same as those described within the feasibility study quoted above.

- GEOMECHANICAL CHARACTERISATION OF THE SALORO CUT SLOPES / CARACTERIZACIÓN GEOMECÁNICA DE LOS TALUDES DE LA CORTA DE SALORO. Golder Associates Global Ibérica. April 2020.

This study analysed the rock mass quality based in Q parameter, RMR index and Geological Strength Index (GSI). The results were divided in superficial (including slopes) and deep massif. The results of superficial massif demonstrate that the worst rock quality values are linked to the area of influence of the faults and, as depth of slopes increase, rock quality also increases, with low quality on top of the slope and high or very high quality at the base of the slope. Deep massif was studied with historical boreholes and the results show that the rock quality increases with depth with bad or very bad rock values for the first 20 meters and medium quality to very high quality thereafter.

Golder proposed optimizing the geometry of the open pit creating 15m height and 75º angle benches, with 5m berm width.

- REPORT OF THE STABILITY IN DEEPENING THE BARRUECOPARDO MINE TO 290 m / INFORME DE ESTABILIDAD GLOBAL DE LOS TALUDES DE LA MINA BARRUECOPARDO PARA SU REPROFUNDIZACIÓN HASTA 290 m. Leandro Alejano. March 2024.

Latest report, explained in short in the following sections.

5.2 Approach

5.2.1 Petrographic characterization

A petrographic analysis of the mine rocks has been carried out at the petrographic laboratory of University of Vigo. Two types of lithologies have been analysed: granite (monzogranite) and hornfels of bio quartz and biotite. This analysis is essential as a basis for the study on the two lithologies present in the open pit. The following figure shows the approximate areas with these lithologies (brown area = hornfel).

Figure 5-1 View of the east slope of the cut from the southwest, showing the areas where hornel appears. A. Lejano. 2024

5.2.2 Laboratory characterization

Laboratory characterization of the intact rocks has been carried out, with results grouped according to lithologies. The laboratory tests performed for the characterization are as follows:

- Density test
- Uniaxial compression test
- Indirect tensile strength test
- Triaxial compression test
- Elastic parameters estimation
- Hoek-Brown failure criterion

- Tilt test

In summary, both the granite and hornfel present high strength (110 and 120 MPa, respectively) and corresponding Hoek-Brown friction “m” parameters 29 and 13. The Table 5-1 hows the geomechanical parameters obtained from the tests.

Table 5-1 Intact rock parameters characterization 2024.

		Granite		Hornfel	
	Parameter (unit)	Media	Standard desviation	Media	Standard desviation
Masic	Density	2.63	0.006	2.79	0.07
Elastic parameter	Young's modulus E (g/cm^3)	53.2	7.1	62.5	7.3
	Poisson's ratio (Mpa)	0.25	0.03	0.3	0.05
Parameters of direct simple strength	Simple compressive strength, s_c (Mpa)	112.8	20.1	118.8	31.1
	Simple compressive strength, s_t (Mpa)	11.5	2	19.7	1.7
Parameters of Hoek-Brown strength	s_{ci} (MPa)	109	-	120.6	-
	m (-)	29	-	13	-
Friction contacts	Friction angle (º)	28.9	0.5	30.1	0.8

5.2.3 Field characterization

The rock mass was characterized based on the measurement of a sample of discontinuities taken at the mine. Additionally, data collected in the initial characterization report by Golder (2020) and geotechnical characterization and monitoring data in bi-monthly reports by Saloro and MiningSense were taken into consideration.

This has allowed characterization of the rock mass as good to medium geotechnical quality with a GSI of 62. 4 main joint sets have been identified, 3 sub -vertical ones and a sub-horizontal one, all of which hardly affect the stability of the slopes. An additional secondary joint set appears dipping at around 50º towards W, which can locally cause planar failure slope stability problems, as already happened in the southeast corner of the pit. These joints occur locally and are often not too persistent, which limit instability issues; however, it is strongly recommended to follow its outcropping in the slopes and monitor them in detail. The Table 5-2 shows the parameters measured for each joint sets.

Table 5-2 2024 Discontinuities parameters

Set		J1 sub-ver.	J2 sub-hor.	J3 sub-ver.	J4 sub-ver.	J5 Lisos E
Type		predominant	predominant	predominant	predominant	local
Dip direction	º	112 (10)	295 (35)	164 (12)	64 (12)	273 (20)
Dip	º	78 (10)	18 (20)	84 (15)	84 (12)	51 (15)
Continuity	m	10 - 20	> 20	10 - 20	10 - 20	10-20 to >20
Spacing	m	0.6 - >2	>2	0.6 - >2	0.6 - >2	>2
JRC		6 (3)	6 (1)	6 (2)	8 (3)	9 (4)
JCS	Mpa	133	82	133	102	108
r (Schmidt)		47	38	46	42	40
Thickness		Closed at 1mm	1mm to 1cm	Closed at 1mm	Closed at 1mm	Closed at 1mm
Filling		Qz.	Ox.	Ox.-Qz.	Ox.-Qz.	Ox.
Meteorization	Grade	II	II-III	II	II	II
Water		Slightly wet	Slightly wet	Slightly wet	Slightly wet	Slightly wet

Some sub-vertical faults appear on the slopes, which cross the slopes normally or transversely. These types of faults are not problematic in terms of general stability; even if they tend to produce rockfalls and damage cut-benches. Anyhow, it is advisable to continue identifying faults and considering their impact on slope stability. The Figure 5-2 shows the location of the faults in the new cut designed.

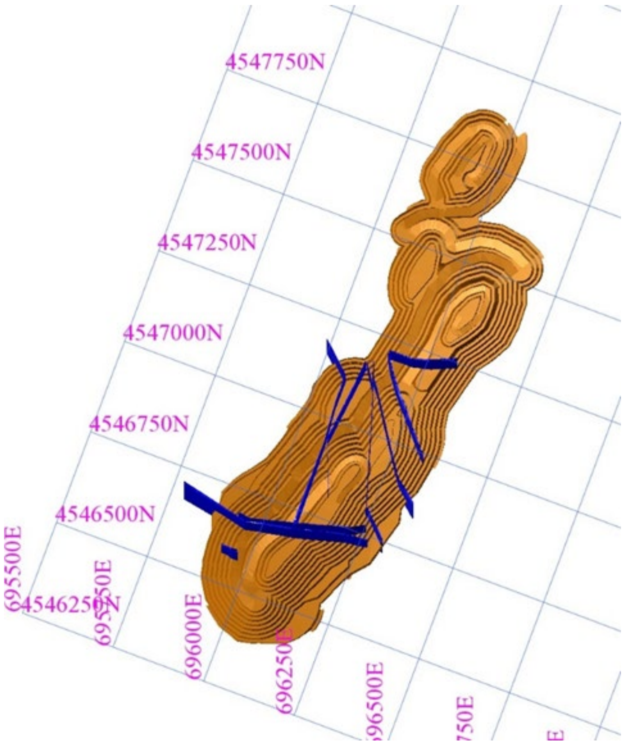


Figure 5-2 Faults overlying the open pit design

Based on intact rock parameters and the rock mass characterization, new geomechanical parameters representative of the rock mass at slope scale have been estimated. These parameters are considered realistic and moderately conservative. They are somewhat more conservative than previous parameters based The Table 5-3 Estimated 2024 Rock Mass parametersshows the estimated geotechnical parameters calculated as a function of the rock mass alteration.

Table 5-3 Estimated 2024 Rock Mass parameters

Parameters	Symbol	Highly disturbed area (0-25 m)	Weathered massif (25-55 m)	Intact massif (55-300 m)
Density (g/cm3)	ρ	2.55	2.6	2.63
Simple compressive strength of the intact rock (Mpa)	σ_{ci}	29.3	44.5	109
Geological Strength Index	GSI	28	54	62
D (deterioration)	D	0	0	0.5
Hoek-Brown's Criteria	m_b	2.522	6.383	4.748
	s	0.003	0.006	0.0063
	a	0.52	0.5	0.5
Young's Module (Gpa)	E	0.9	7.32	16.34
Poisson's Coefficient	υ	0.25	0.25	0.25

5.3 Slope configuration

For the design of final slopes, double-benching of 10m has been used, which results in final benches of 20 meters high and 75º of inclination and berms of 7 meters for the reasons given in *"Report of the slope stability in deepening the Barruecopardo mine to 290m"* (University of Vigo, 2024) as it can be seen in Figure 5-3.

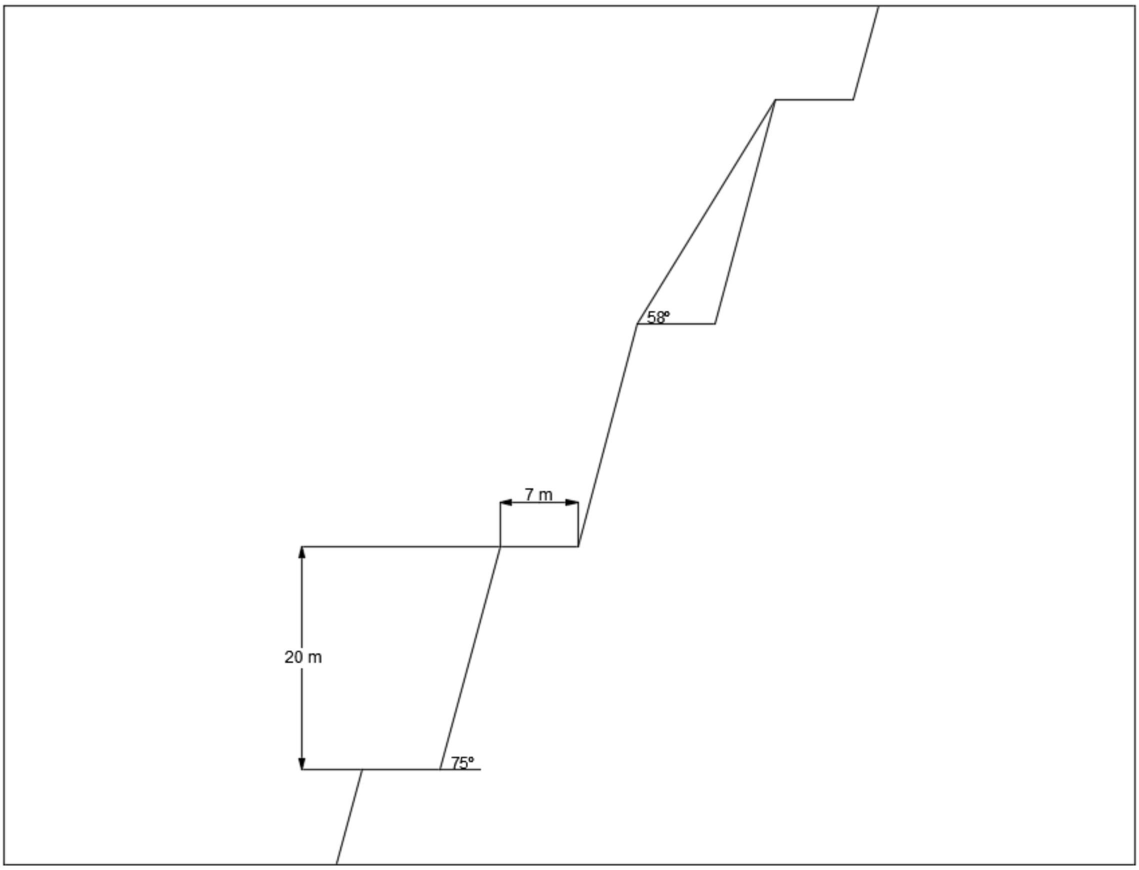


Figure 5-3 Slope configuration

5.4 Slope stability

5.4.1 Potential instabilities with structural control

With the background of joint set data collected, a review of potential structurally controlled instabilities has been performed. The potential instabilities assessed are toppling, planar failure and wedge failure.

There is a low possibility of toppling failures. Wedge instabilities might take place in a local manner (east wall) and only at the bench scale, such that fallen material will accumulate in cut-benches. The occurrence of planar failures following J5 set joints cannot be discarded, although, based on observation of the East wall, it does not seem that it will be very common or extensive. In any case, it is advisable to control these planes and follow indicative suggestions in case of incipient failures.

5.4.2 General stability of the pit slopes and conclusions

To check the general stability of the pit slopes, 4 representative sections of have been selected corresponding to mining phase 6. For these circumstances and by means of three different methods (Hoek-Bray charts, limit equilibrium and numerical FEM), safety factors have been obtained for the proposed design. Values computed are above those typically considered acceptable in open pit mine design (FoS above 1.6 and SRF above 1.4), which ensures the general stability of the open pit for the proposed design, if assumptions of structural homogeneity and absence of faults parallel to the slopes is fulfilled. The Table 5-4 shows the results of safety coefficient and SRF for the most unfavourable slopes in each area.

Table 5-4 2024 Safety and Strength Reduction Factors.

Slope height (m)	Safety coefficent Hoek and Bray's Abacus	Safety coefficient Slide (HB)	SRFCode RS2
Slope east-central	1.95	1.62	1.42
Slope east-north		1.93	1.64
Slope west-central		2.4	2.06
Slope west-north		1.92	1.86

The geotechnical report strongly suggests following the safety and geotechnical control measures typical of good mining practice. This includes updating geotechnical data and designs, if necessary; analysing all rock engineering issues at stake trying to understand the underlying causes and finding solutions and applying a slope monitoring system with associated measures that allows controlling the design response in a systematic manner.

6 Cut-off strategy

Barruecopardo is an open pit mine with a single product: WO_3 concentrate. The main mineral containing the final product is Scheelite. The ore, once extracted, follows a concentration process where the light minerals, sulphides and magnetic minerals are removed. The final price of the concentrate depends not only on the WO_3 content but also on the presence of deleterious elements and the global quality of the concentrate. The cut-off grade strategy must consider this and also the associated parameters in the operation such as the costs and expected recovery. This chapter discusses how these aspects has been considered to derive a cut-off grade strategy.

The cost estimate (chapter 13) and techno economic model (chapter 14) developed to assess RPEE have also been developed using the methods, data and assumptions described in this chapter.

6.1 Commodity price assumptions

The assumptions for the commodity (WO_3) price are based on the forecasts in the Wood Mackenzie report for the Ammonium Paratungstate (APT) (WM) for the period from 2021 to 2030. This was a report specifically commissioned by EQ Resources. There are 3 series of prices for the base case, low case and high case as shown in Figure 6-1.

The historic APT prices for the last 3 years, that is since the start of the Wood Mackenzie forecast, sourced in public releases on “Fast Markets”, are also included in the Figure 6-1, as comparison with the WM forecast.

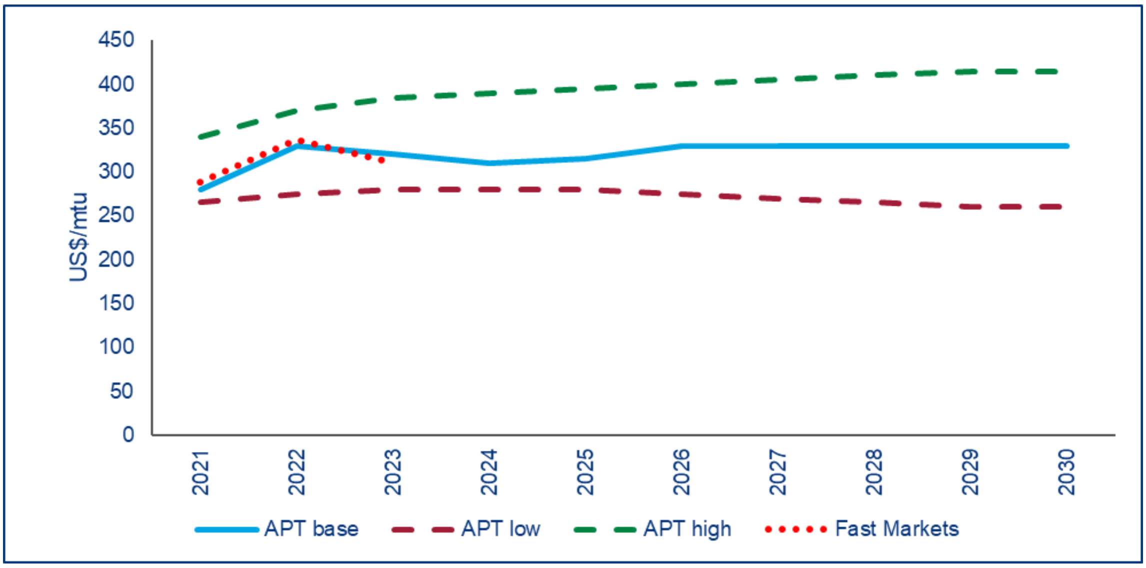


Figure 6-1 APT price comparison with of actual v forecast

MiningSense concludes that the WM forecast in 2021 is tracking reasonably with actual pricing, and that it is reasonable to use the WM base case for future forecast prices.

Saloro has provided MiningSense with their actual received APT prices based on their contractual agreements. These do not show significant variations to the ones recorded by Fast Markets.

The commodity price based on the existing information is set as for US$310/mtu for the short term and US$330/mtu for the long term for the APT.

6.2 Recovery factors

The recovery factors are based on the current plant performance and the expected improvements that began in January 2024 and will be completed within the following 18 months. These are detailed in chapter 11 .Figure 6-2shows the expected metallurgical recoveries.

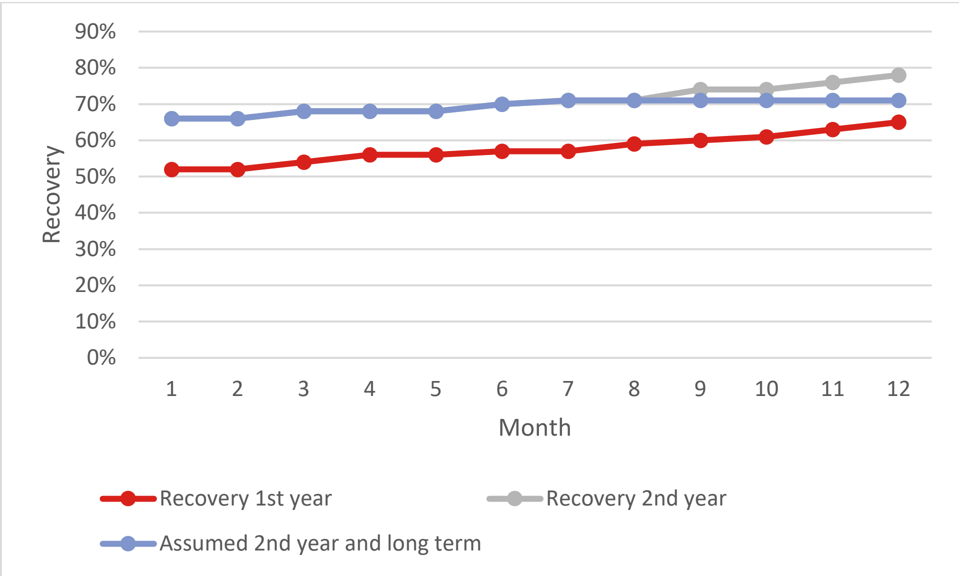


Figure 6-2 Forecasted Metallurgical recoveries

The recoveries expected by Saloro increase and reach up to 78% by the second year after the improvements and changes in the plant. The recoveries used by MiningSense to estimate reserves are 58% for the short term and 71% for the long-term. Further explanations about those assumptions are made on the section 11.3.

6.3 Royalties and tax assumptions

No taxes and royalties have been considered for the cut-off strategy, as there are no mining royalties to be paid according to the current mining permit.

6.4 Payment terms

The payment terms are based on existing Saloro contracts. Those contracts consider the following parameters:

- APT price
- WO_3 content in concentrate
- Moisture

Deleterious elements (basis for penalty):

- Molybdenum content
- Sulphur content
- Arsenic content
- Phosphorus content
- Uranium content
- Thorium content

The block model has no estimates for Uranium and Thorium content. It is populated with the other deleterious elements. In any case, Saloro operates a plant that includes magnetic separation to remove the Uranium and Thorium.

Regarding the other deleterious elements, these are all controlled through the flotation stage of processing so as to not pass the minimum acceptable limits.

Each delivery usually consists of 20 t to 24 t of concentrate, divided into 1t bulka-bags. A sample is taken from each of the bulka-bags and another sample is taken as a composite of the total batch. Therefore, two results are produced from every delivery: one as the average of the individual analysis and the other as the composite analysis. The receiving smelters conduct their own sample tests on the incoming concentrates.

Three concentrates assay results are shown in the Table 6-1. These have been checked to understand the impact on the potential selling penalties and have been compared with the contract established limits for the different deleterious elements, as per the Saloro conditions of contract.

Table 6-1 Historical concentrates produced

Parameter	Un	Value			Limits (based on 3 contracts
Date		11/01/2023	30/01/2023	15/03/2023	
Material		Scheelite conc.	Scheelite conc.	Scheelite conc.	
Lot		112/230101/20/W	114/230103/20/S	124/230303/20/X	
Net weight	kg	20.01	20.01	20.01	
Dry weight	kg	20	20	20	20
Moisture	%	0.5	0.005	0.05	1%
Content (WO_3)	%	64.983	69.293	64.514	50-60% min
Impurities					
As	%	0.38	0.3	0.42	< 0.3%
S	%	0.35	0.21	0.23	< 0.4%
P	%	1.19	1.1	1.25	< 2%
U	%	0.006	0.004	0.006	< 0.007%
Th	%	0.002	0.002	0.002	< 0.002%

6.4.1 Penalties

A review of the 12-month data from August2023 has been completed to understand the variability of these deleterious elements, and hence the likely incidence of penalties on sales contracts. The comparison is shown in Figure 6-3 and Figure 6-4 . The tables Table 6-2 and Table 6-3 summarises the incursion of penalty events for these respective periods. Noting that these two periods show before the plant improvement plan implementation, and the first semester after its' implementation has begun.

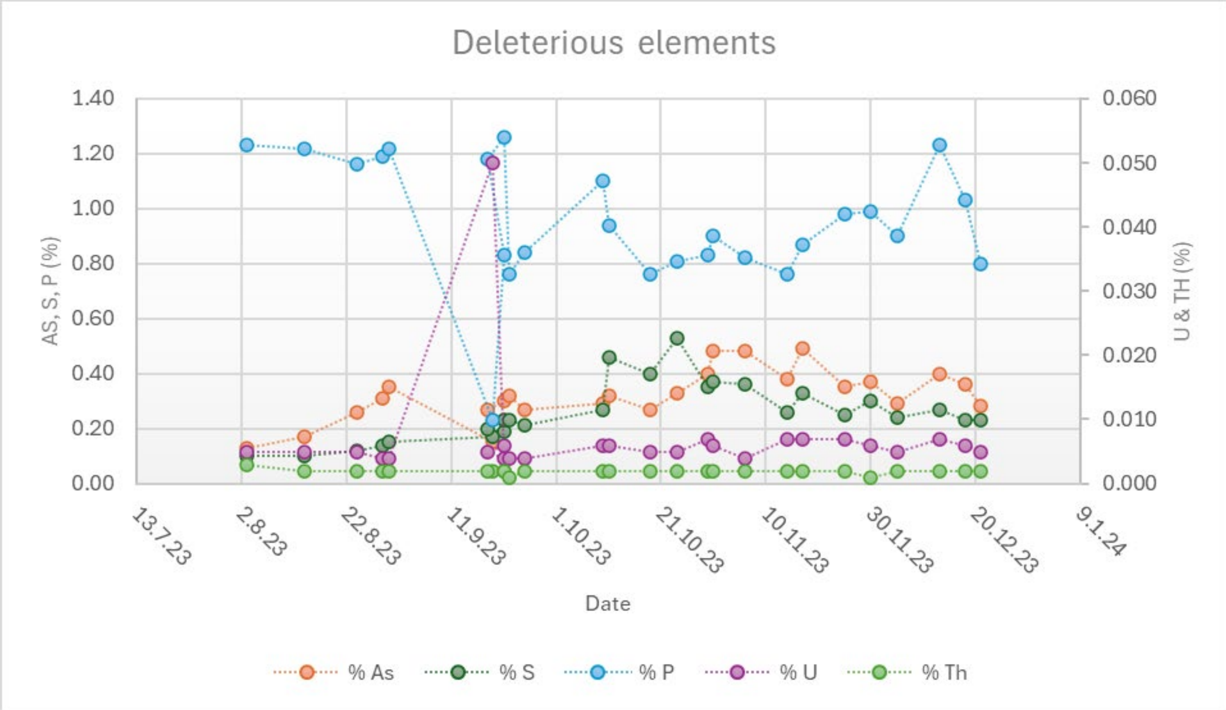


Figure 6-3 Concentrate Deleterious elements: August to December 2023

Figure 6-4 Concentrate Deleterious elements January to June 2024

Table 6-2 Deleterious elements presence in 2023 concentrates

	% As	% S	% P	% U	% Th
Limit for penalty	0.3	0.4	2	0.007	0.002
Total	26	26	26	26	26
Above the limit	14	2	0	1	1
% above the limit	54%	8%	0%	4%	4%

Table 6-3 Deleterious elements in the 2024 concentrates

	% As	% S	% P	% U	% Th
Limit for penalty	0.3	0.4	2	0.007	0.002
Total	31	31	31	31	31
Above the limit	11	1	0	3	0
% above the limit	35%	3%	0%	10%	0%

For the series reviewed arsenic (As) incurred penalties for 54% of 2023 deliveries, and 35% of the 2024 deliveries. Sulphur (S) has been above the penalty limit 8% during 2023 and 3% during 2024.

The impact of a As% being above the 0.4% threshold is a penalty of 1 to 3 US$/mtu on payable price, depending on whether the As% is above 0.4%, 0.55% or above 0.55%. The maximum As penalty results in a penalty of 1% of the selling price, and the maximum 0.55% level has never been found in the database of Saloro concentrate assays. Therefore, As penalties have been ignored in price calculations in this work.

Regarding the other deleterious elements: U caused penalties in 10% of the 2024 deliveries, and Th has had no penalties in in 2024 and only in 4% of 2023 deliveries. Both are considered as not material for this work.

As a general comment, the performance in the plant has significantly improved in terms of control of deleterious elements since the implementation of the plant improvement project, with the downward evolution of As being the most relevant

6.4.2 Payability

Payability, percentage of WO_3 metal contained in the concentrate that is actually paid, relates to the WO_3 content and the APT prices. The payability is calculated considering the actual APT price and the WO_3 content in the concentrates.

The assumption made is that the payability is 78% for the life of mine, considering that the WO_3 content in the produced concentrates will be between 60% and 70%. The Saloro plant aims to produce a 'steady' 64% WO_3 concentrate

Payability is applied as per the following formula:

$$Selling\ price\ per\ WO_3\ produced = Market\ APT\ price\ \times Payability\ (0.78)$$

The opinion of MiningSense is that payability of 78% is a very sustainable assumption based on the historical %WO_3 of the concentrates, as shown in Figure 6-5 and Figure 6-6 Note the WO_3 in concentrate is expected to return to consistency once the plant improvement plan is completed.

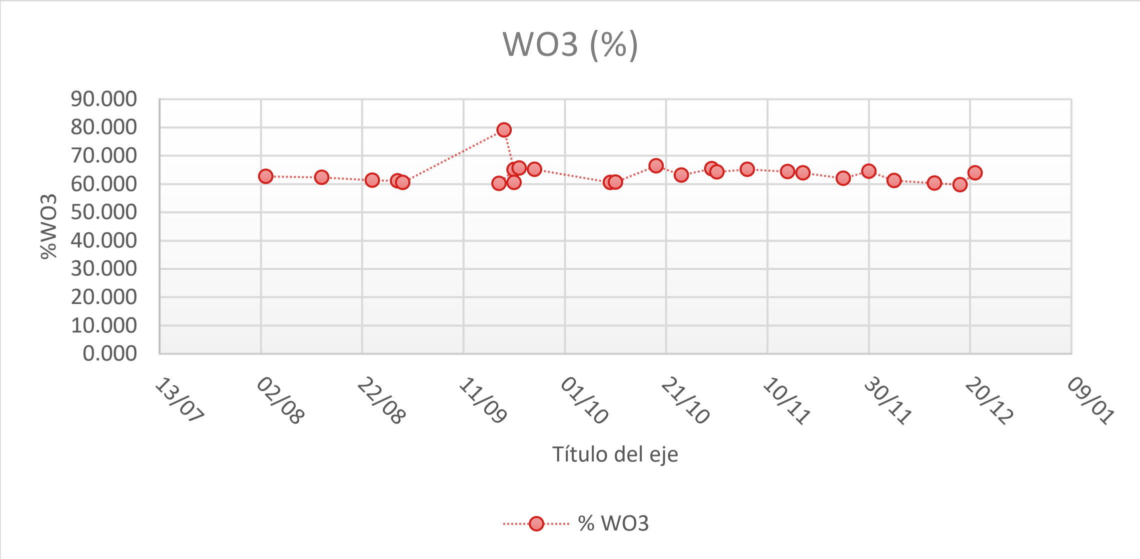


Figure 6-5 WO_3% in concentrate ; August to December 2023

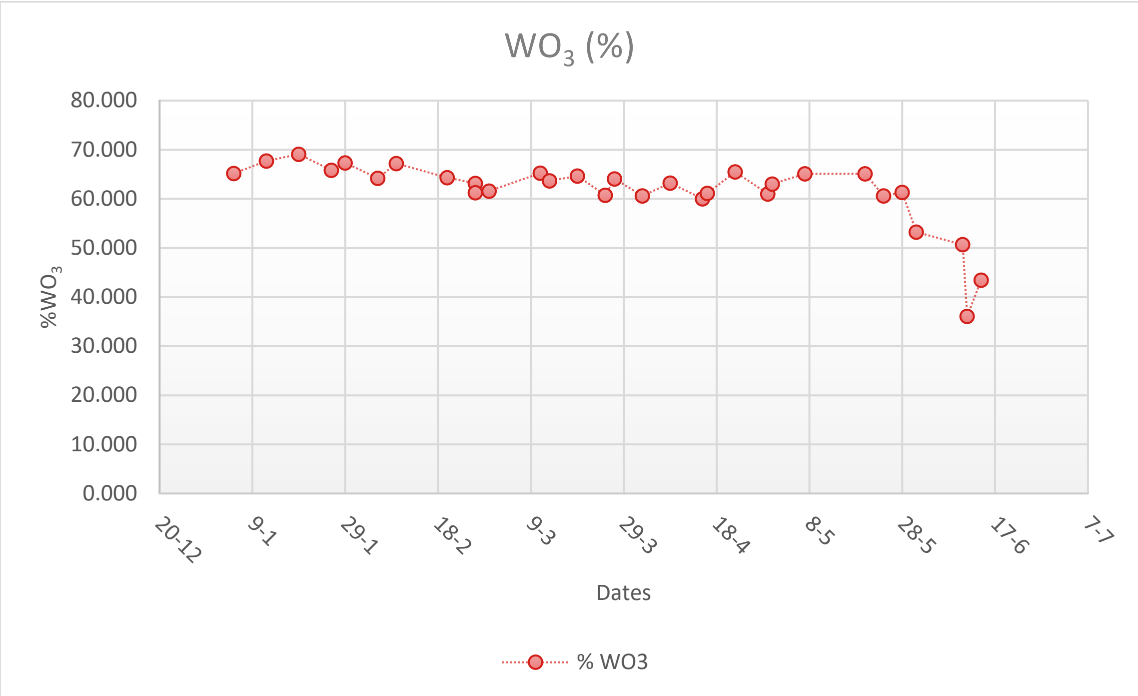


Figure 6-6 WO3% in concentrate; January to June 2024

Considering the APT prices as per WM forecast (above US$325/mtu) and considering the WO_3% in the concentrates (between 60% and 70%), the payability is potentially closer to 79% or 80%. The worst conditions (low APT price and low WO_3 in the concentrates) would imply a payability in the range of 76%-77%, therefore the potential impact on the total price paid is around 2%. So, the assumed payability of 78% is considered conservative based on the existing information.

6.5 Capital and operating cost assumption

Capital costs have not been included in the COG strategy. The expected capital costs associated with the plant improvement plan, total 630,000€. Their timing is shown in Figure 11-9.

This spend, and the other CAPEX considered in the economic model are discussed in section 14.

The operating costs used for the calculation of the COG are based on the current costs for the mine, process and general and administrative costs, as shown in Figure 6-7.

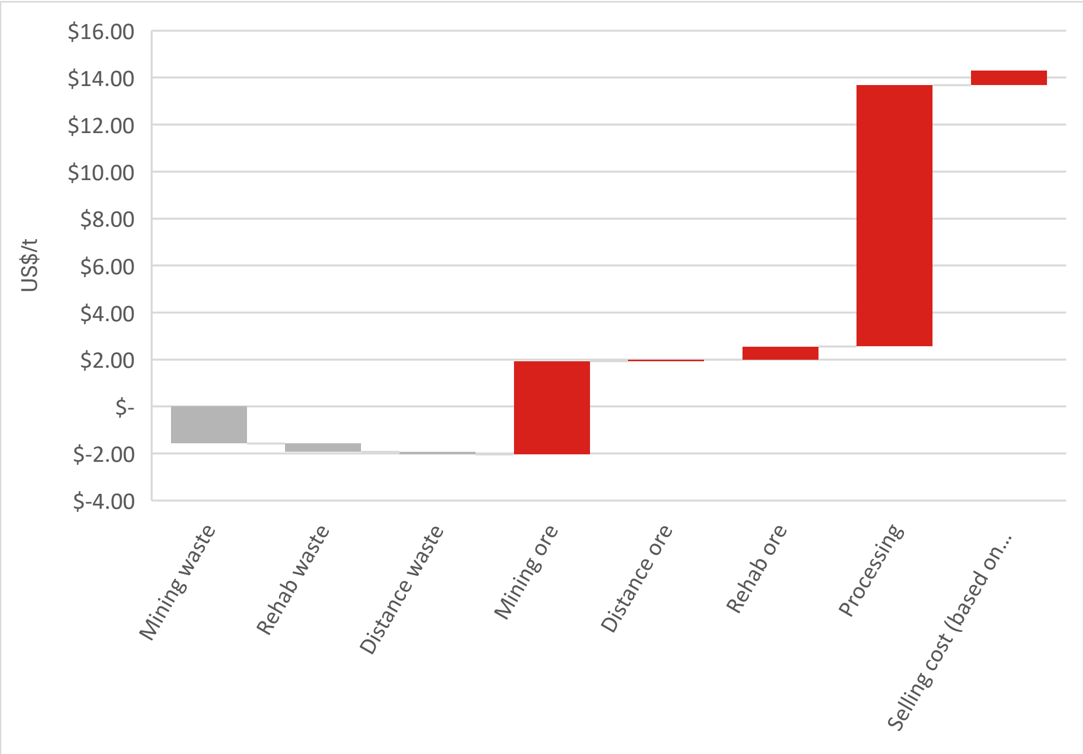


Figure 6-7 OPEX total Costs used for COG

Only the processing associated costs and administration costs, are considered to calculate the break-even cut-off grade, to differentiate ore from waste. These are shown in Figure 6-8.

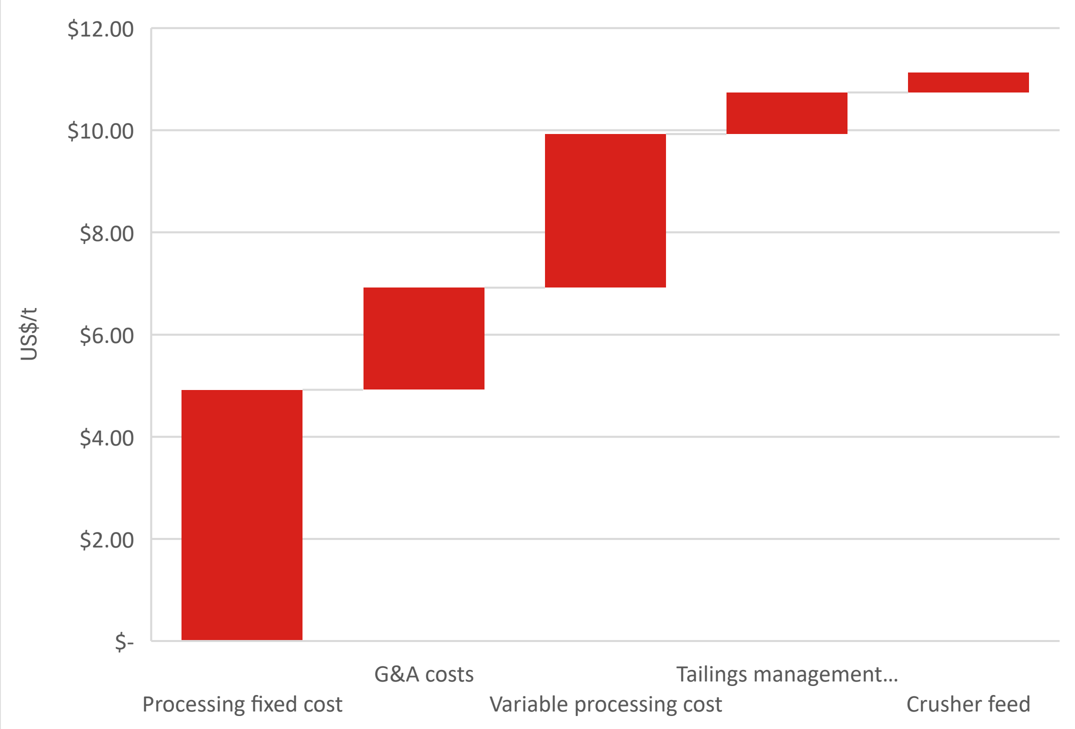


Figure 6-8 Processing cost basis for the break-even COG

6.6 Break-even cut-off grade

The break-even cut-off grade is calculated based on the well known formula shown below.

$$Cut\ Off = \frac{Processing\ and\ Admin\ Costs}{Selling\ price \times Recovery}$$

Based on the break-even cut-off grade, individual blocks can be categorised as ore or waste. The following table summarizes the break-even for the scenarios considered.

Table 6-4 Break-even cut-off grade (COG) calculation

Scenario	Selling price	Metallurgical recovery	Break-even COG
	US$/mtu	%	WO_3%
Short-term	310	58%	0.08
Long-term	330	71%	0.06

For the stockpiles the same cut-off is applied as only the processing and administration costs have been considered in the calculation of the cut-off grade.

7 Pit Optimisation and Mine design

Ore Reserve is the economically mineable part of the Measured and/or Indicated Mineral Resource, this means that a feasible design must be made to constrain the resource. The iterative optimization process described here delivers the ultimate pit-shell, and guidance for final pit design and schedule.

7.1 Resource Block Model Modification

The block model described in the section 4 *“Mineral Resource Estimate”* (MRE), saloro_202310_res_rot.mdl, is the source for this Ore Reserve Estimation.

For optimization purposes, several modifications have been performed to the MRE block model using Surpac 2023 HF 1 (x64) (31892). The purpose of these manipulations has been to include the mine operating methods, economic factors and/or specific factors which will aid the optimization used in this Ore Reserve Estimate.

These modifications are discussed in the following sections and comprise the block model regularization, modified the grade attribute for exclude inferred material in the optimization, flagging air and waste blocks, block model depletion for excluding material mined during 2023 year operations and several economic data fields included as new attributes.

7.1.1 Block Model regularization

The resource block model has been sub-blocked at 1.5x1.5x5m, although this block size is not minable, this sizing is so that the block model can be adjusted as closely as possible to the structural wireframes that define the distribution of the ore veins in the deposit. Optimization process requires a regularized block model as it is assumed the same equipment and drill and blast patterns will be used for all parts of the model. This will achieve a certain selectivity when ore and waste are outlined, and further selectivity enhanced when the mine is operated via the described grade control process.

This process includes changes in the ore, loss and dilution, that depends on the ore distribution and how the boundaries between ore and waste are modelled. No allowance for loss and dilution has been made in the resource model.

Different regularization options have been trialled to control the regularization effect of grade distribution. Attributes have been weight by density and resource class has been assigned using the most present class encountered in the sub-blocks during the regularization process.

The comparison shown Figure 7-1, Figure 7-2, Figure 7-3 and Table 7-1 show the Difference between the original resource block model and the regularization to 3x3x5m and then to the final SMU 6x6x5m block.

Table 7-1 Block model regularization effect

Model	CoG (%)	Tonnes (t)	mtu (t)	Av WO_3 (%)	Dilution (%)	Losses (%)
MRE	0.05	20,514,100	3,742,486	0.182	0%	0%
3x3x5	0.05	21,757,370	3,741,163	0.172	6%	0%
6x6x5	0.05	22,922,877	3,662,874	0.160	12%	2%

As can be seen in the Table 7-1 and the Figure 7-1, the block model selected (6x6x5) has a 12% of dilution and 2% losses, in comparison with the resource block model. The effect of the regularization up to 3x3x5m block size includes a 6% of dilution comparing with the resource model.

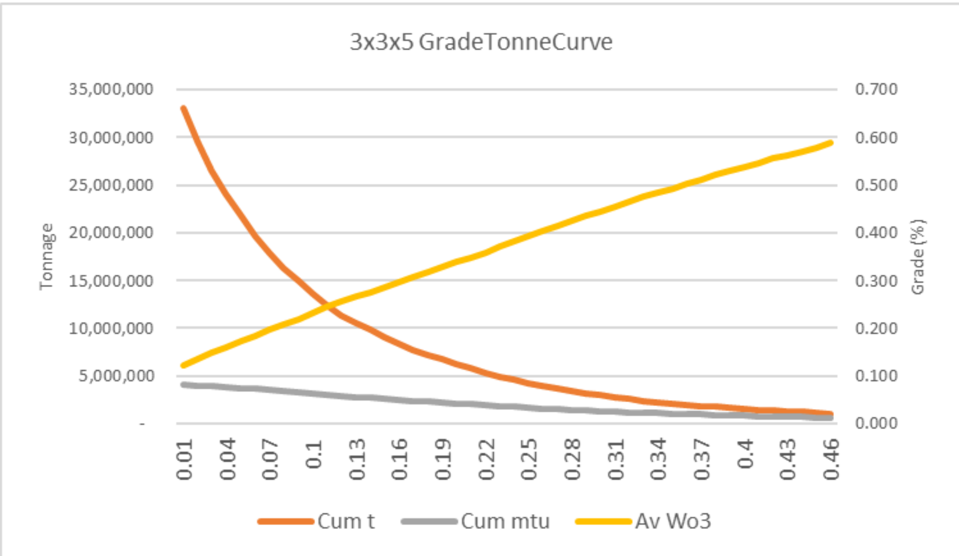


Figure 7-1 3x3x5 BM size Grade-Tonne curve

The regularization to 6x6x5 is aligned with the SMU selected, what produced a planned 12% dilution and 2% losses.

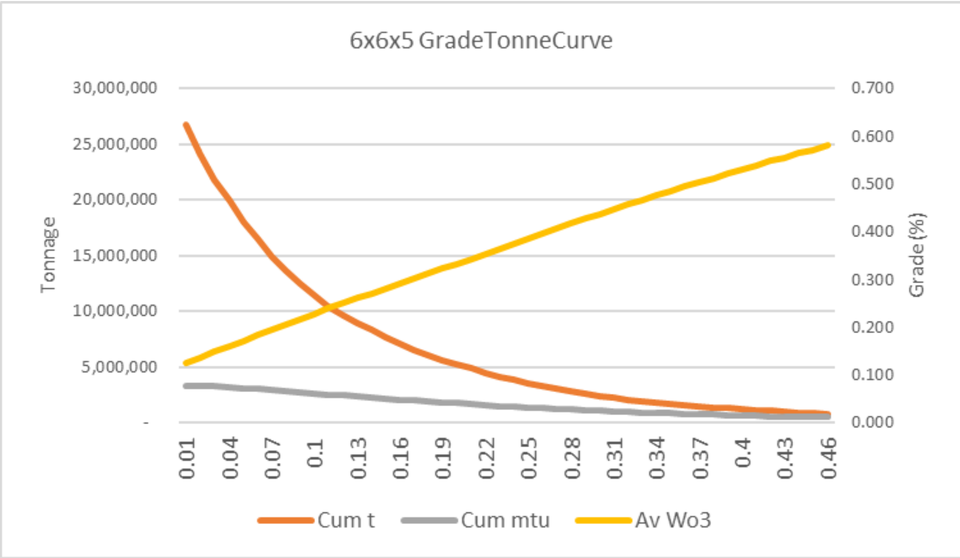


Figure 7-2 6x6x5 BM size Grade-Tonne curve

For this ORE 6x6x5m block size has been selected. This is the selective mining unit (SMU) which best represents the planned operational effects of bench heigh, drilling and blast pattern, loading equipment, grade control methodology and the ore deposit and mineralization distribution. Based on this it has been done an analysis of the different factors to conclude that:

- Bench heigh is 5m for ore and 10m for waste, adapted to the block model, it is not possible to load the material in smaller flitches as the rock (granite) does not enable a proper vertical separation after blasting. Studies done on the efficiency of the blasts recommend increasing the bench height rather than reducing it.
- Blast pattern defines the minimum sampling separation, this ranges between 3 to 4 m so it is not possible to reduce the selectivity in the separation of ore and waste.
- Excavators used for loading the material in the trucks are 120t excavators (Komatsu 1250 type) and the bucket is 7m^3 capacity. The dimension of the equipment is 4.5 to 5 m width and the trucks used in the operation are 100t capacity trucks (Komatsu 785 type) 5.1m width.
- Grade control is based on the information from the blastholes assay; therefore, it is difficult to distinguish smaller areas, as no non-blast holes are drilled or sampled. The use of UV lamp in the field is a second step to try to avoid losses in the blast polygons used to differentiate the different qualities of the blasted material.
- Mineralization and ore deposit distribution is described in the resource estimation, considering a sub-blocking of 1.5m. This minimum width is proportional to 3m, 6m, 12m. The orientation N-S of the ore and the reduced veins width make important to reduce in X direction the block size and being more flexible in Y direction.

Based on the previous aspects a 6x6x5m block size seems appropriate for the SMU, considering also that the majority of the blasts will be developed perpendicular to the mineralization and the ore distribution.

In Figure 7-3 it is shown the grade tonne curves for Resource block model and Reserve block model which cut-offs are more affected to this regularization.

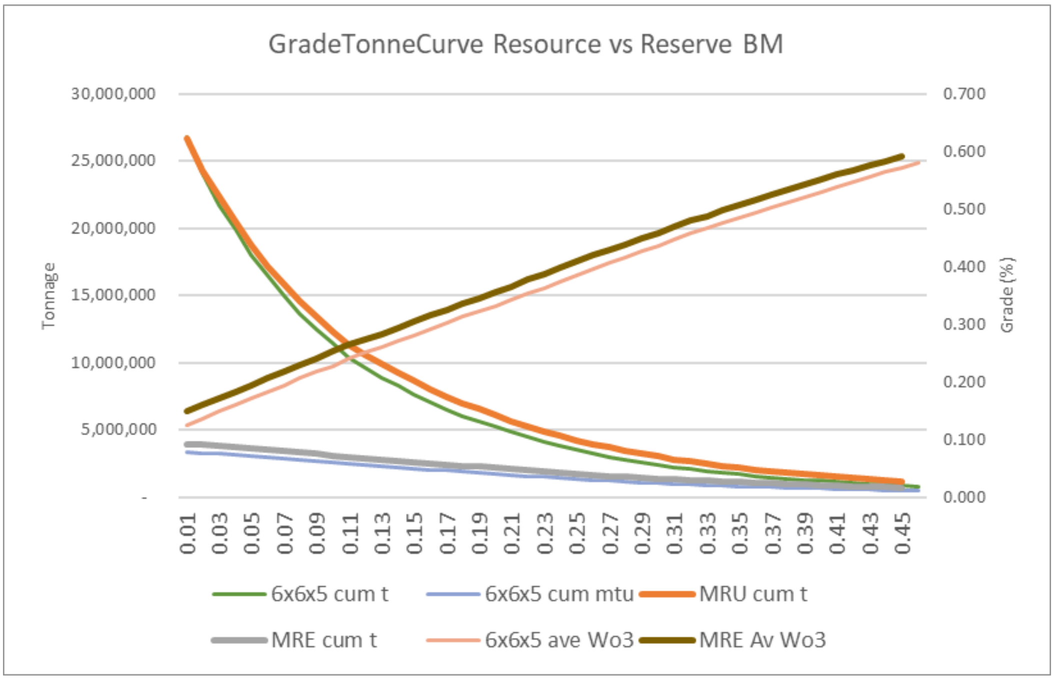


Figure 7-3 MRE vs 6x6x5m Grade-Tonne curve

7.1.2 Mine losses and dilution

Apart from the planned losses and dilution, included as a regularization of the resource block model, an operational loss and dilution is applied in the mine plan. This operational dilution is based on the Saloro performance over the last years and their experience on this deposit. The operational dilution is 15% and the operational losses 6% and comes from performance real observation.

Figure 7-4 shows blasted material, and an adjacent pattern already drilled but not blasted. Even with having drillholes (samples) each 3.5 or 3 m, it is difficult to separate ore and waste, and even more so after blasting.

Figure 7-4 Blasting area in the bench 590. April 2024

The regularization of the block model introduces a 12% dilution and 2% losses, on top of it is added the operational dilution because of the mixed produced with the blasting and with the separation of the ore material with the 7m^3 bucket excavators: 15% dilution and 6% losses. This, at the end, supposes a cumulative dilution of 29% and a total loss of 8%. The figures are aligned with the recent information recorded by Saloro.

The number could be considered high for an open pit operation, but the reality is that the orebody is almost vertical what produce a high uncertainty by using vertical holes to determine the exact location of the veins (nugget effect). Also, narrow veins are more difficult to mine and requires, to reduce the dilution, using specific equipment, blast patterns adapted and grade control drillholes.

Saloro is putting significant effort in controlling dilution, using software specialised for blast movement prediction and laboratory analysis. There is still room for optimise loss and dilution figures and in the future the SMU could be reduced with more contrasted data on the reconciliation.

MiningSense consider the loss and dilution acceptable for the current operation and believe that those figures can be reviewed in the future should their control be improved. This would have a positive impact on project economics.

7.1.3 Attributes included for reserve estimation

7.1.3.1 WO3_ms attribute

To identify measured and indicated category resources in the optimization process a new attribute named wo3_ms has been included. This attribute is built on the grade attribute coming from MRE wo3_pct and it is constrained with a cut-off of 0.05% WO_3. Using the domains defined as class 1 and 2 that correspond to measured and indicated in the attribute.

The MRE in provided resource block model has been checked that it is rotated to align with the main orientation of the mineralised vein swarms which is 15º NNE. In any case, as shown in the modifying factors description, a conservative approach has been applied for losses and dilution. This is considered appropriate at this moment. The resource categories wireframes can be found in section 4.

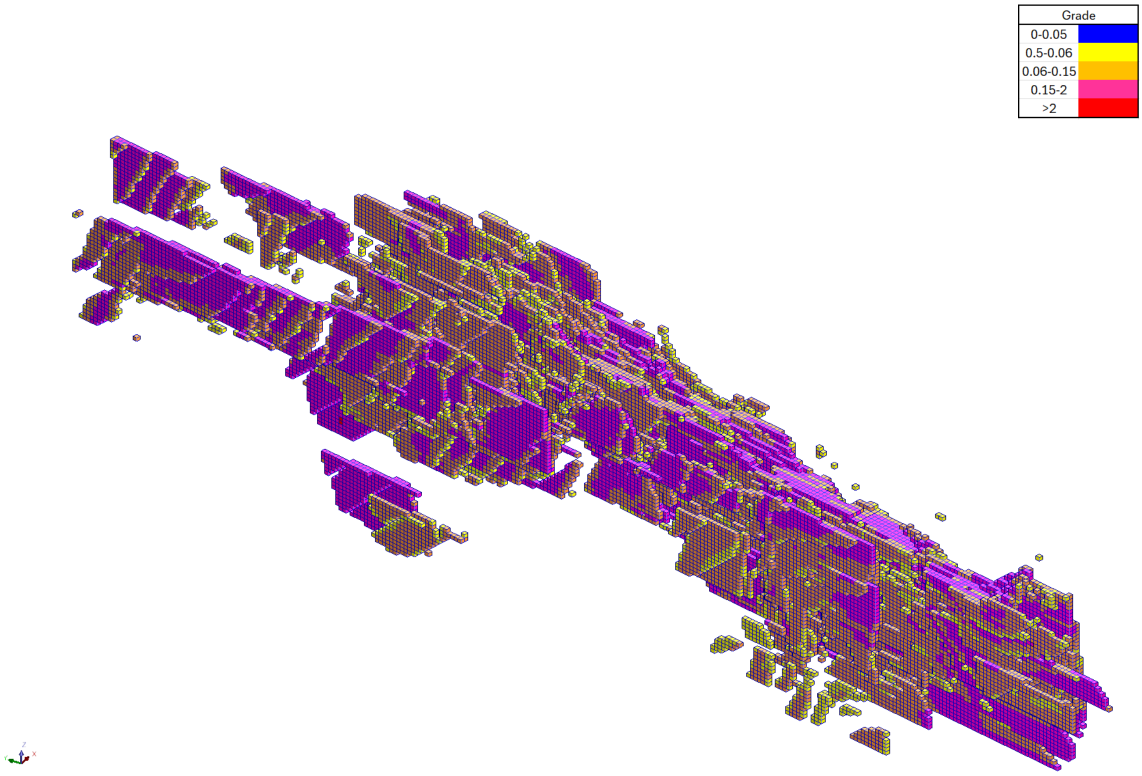


Figure 7-5 05% WO3 _pct Cut-Off

The following sections, Figure 7-6, Figure 7-7 and Figure 7-8, show how the mineralization distribution.

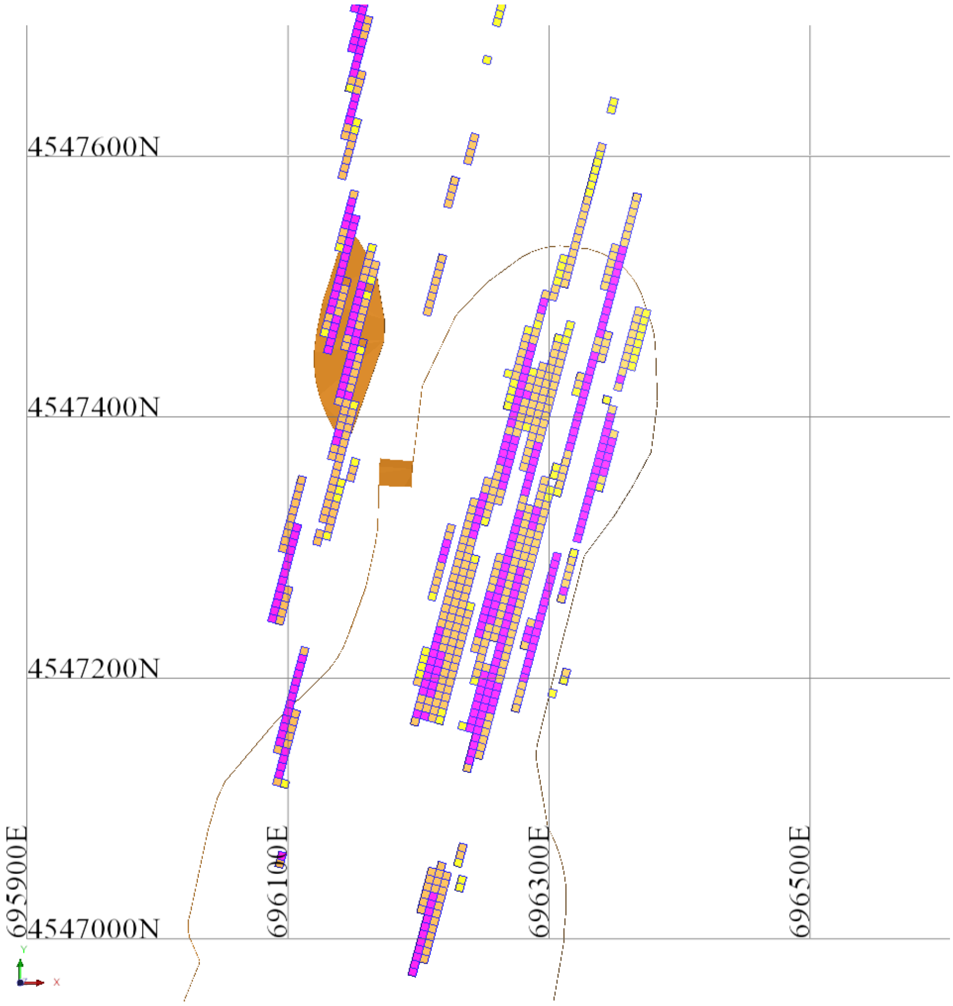


Figure 7-6 630 metre RL bench

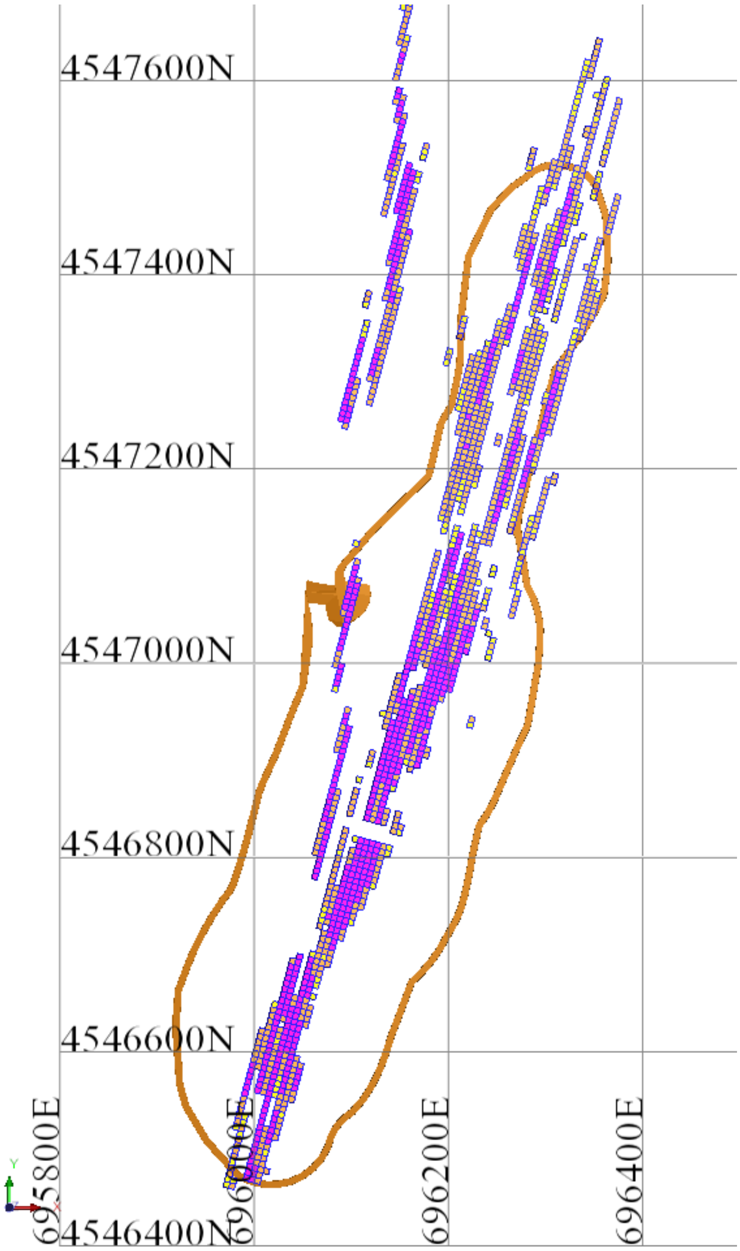


Figure 7-7 600 metre RL bench

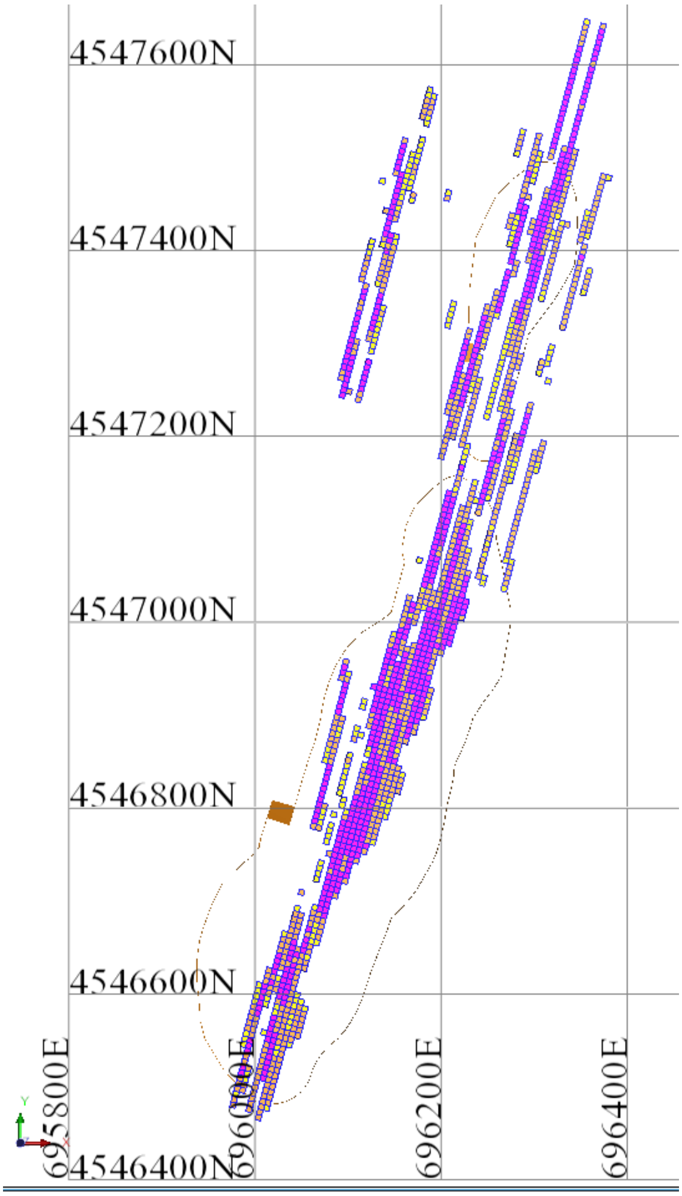


Figure 7-8 575 metre RL bench

Table 7-2 summarizes the differences when the contained inferred resource is considered, or not.

Table 7-2 wo3_pct vs wo3_ms comparison

Model	CoG (%)	Tonnes (t)	mtu (t)	Av WO_3 (%)	Dilution (%)	Losses (%)
6x6x5 Wo3_pct	0.05	22,922,877	3,662,874	0.160		
6x6x5 Wo3_ms	0.05	21,235,341	3,409,318	0.161	0%	7%

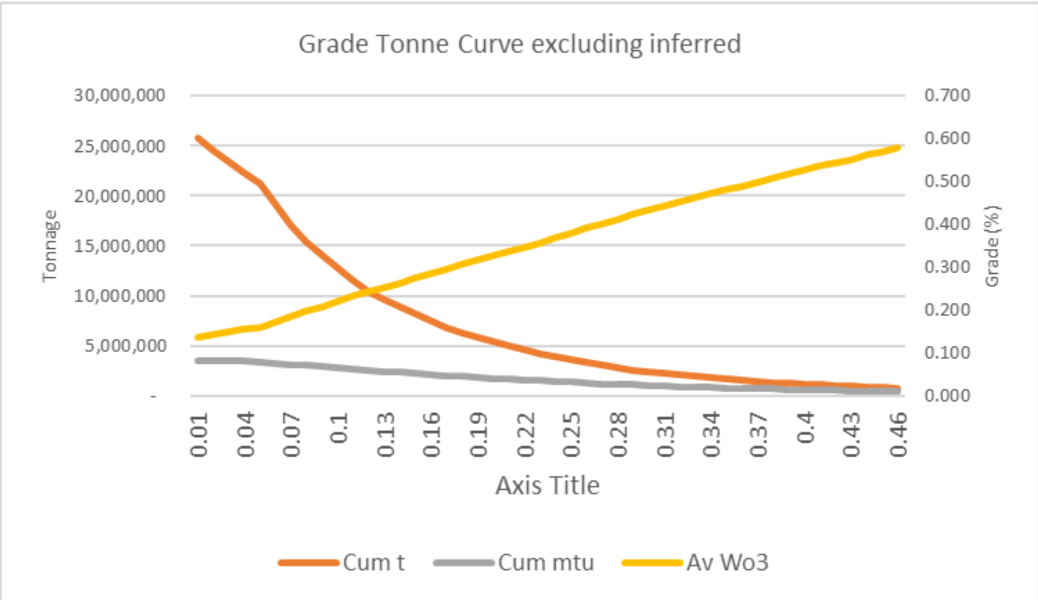


Figure 7-9 Grade-Tonne curve excluding inferred

7.1.3.2 Mined

The MRE block model, built during 2023 had bulk density coded as a model attribute below the *topo_jun23_v2pt.dtm* surface shown in Figure 7-10.

Optimization process depleted the MRE block model to account for interim mining operations, with *EXC_Diciembre2023_TOTAL_3D.dxf* surface, shown in Figure 7-11 being used.

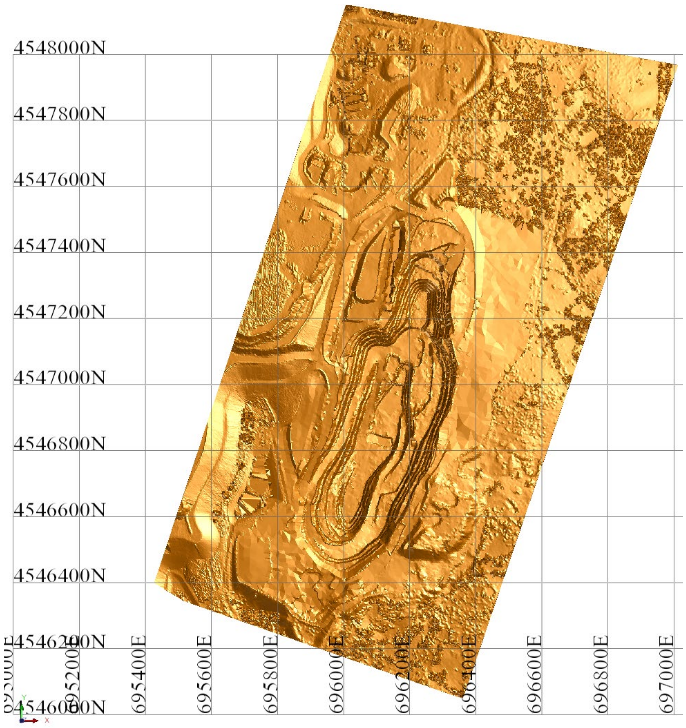


Figure 7-10 MRE topography topo_jun23_v2pt.dtm

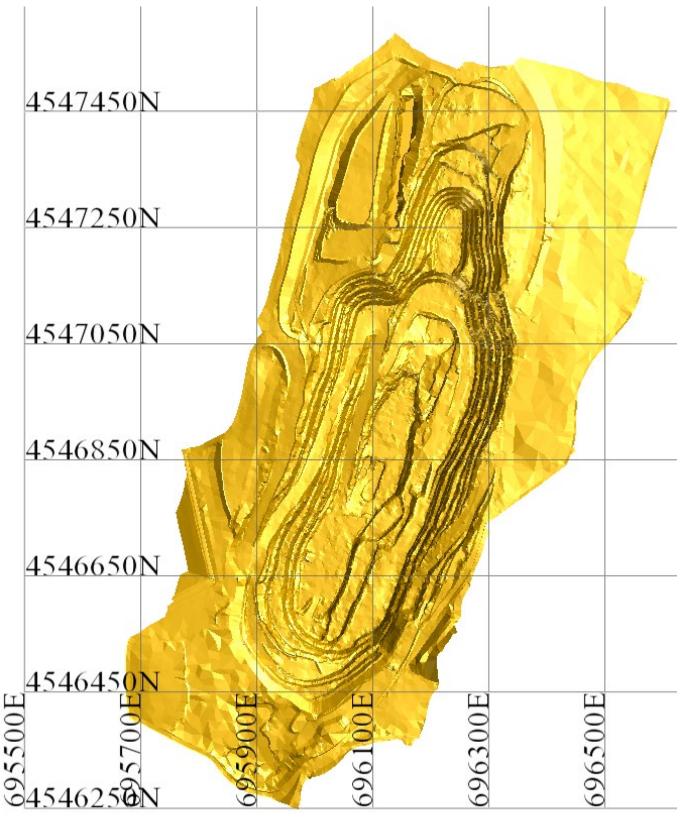


Figure 7-11 EXC_Diciembre2023_TOTAL_3D.dtm

7.1.3.3 Rocktype

Three rock types have been defined as ore, waste and air in the block model for optimization purposes. Air is assigned the bulk density 0 with reference to the topography, ore and waste are assigned by reference to attribute *wo3_ms*

7.1.3.4 Economic factors

Several economic attributes have been added to the block model for optimization purposes. Table 7-3 lists all the new attributes added Further detail on costs is included in section 7.2.

Table 7-3 Economic Attributes

Attribute Name	Description
c_db	Bench distance
c_do	Total distance for ore: distance in bench, in rampa, ex-pit to RoM stockpile and distance in RoM stockpile
c_dr	Horizontal Distance
c_dw	Total distance for waste: distance in pit based on the location of the block plus ex-pit distance plus in-waste dump distance
c_mcaf	Mining cost adjustment
c_mocu	Mine cost applied to ore per tonne
c_mwcu	Mine cost applied to waste per tonne
c_odcu	Ore distance cost per tonne
c_pcaf	Processing cost adjustment
c_pcu	Processing cost per tonne
c_sell	Selling cost per ore tonne
c_vert	Vertical distance
c_wdcu	Waste distance cost per tonne
c_zorg	Pit exit level
cog_p	Cut-off grade using utility of ore and waste
reco_p	Metallurgical recovery
rocktype	Rock type
sell	Block selling price
ton	Tonnes calculated
value	Block value
vol	Volume calculated

7.2 Pit optimization process

Several optimizations have been run in Whittle 4.5.289.0 software to evaluate the impact of changing variable factors as average slope angle, selling price and recovery.

Additional scenarios have been run including adjustment to mining and processing costs to evaluate the economics in the block model

Revenues have been varied from 30% up to 150% using 61 fixed factor and added a single pit-shell scenario with a revenue of the 200% of the selling price.

In the economic scenarios different mining limits have been controlled for the total material moved from 6.2Mt to 9Mt. A fixed plant throughput of 1.3Mt of ore is targeted per year. The 8% discounted rate per period, as agreed for this optimization. Variations in parameters have been applied individually to observe results, and not cumulatively.

7.2.1 Optimization cost model

All the cost and revenues have been included in US$ in the optimization software with the exchanged rate 1.10 €/US$ applied where the cost was provided in Euros.

Cost model elements used in the optimization are shown in Table 7-4.

Table 7-4 Optimization cost model

Optimization Base Costs		
Mine-Ore	Cost	Unit
Ore mining base cost	$ 3.97	/t
Ore Additional Distance Cost	=0.00016*(442+(Depth/0.0995-(3.14*Depth))	$/t
Ore rehabilitation cost	$ 0.55	/t
Cost Drill&Blast, Load&Transport to 1,000m	€ 1.54	/t
Grade control cost	€ 0.52	/t
Mine dewatering cost	€ 0.16	/t
Contour blast average cost	€ 0.00	/t
Mining department cost	€ 1.39	/t
Ore distance cost	0.038*(645+747+50-1000+(Depth/sin(0.1))-(3.14*Depth))€	/bcm/Hm
Rehabilitation of processing tails waste dump	€ 0.85	/bcm
Final rehabilitation cost	€ 0.17	/t
Mine - Waste	Cost	Unit
Waste Mining Base Cost	$ 1.58	/t
Waste Additional Distance Cost	=0.00016*(646+(Depth/0.0995-(3.14*Depth))	$/t
Waste rehabilitation cost	$ 0.36	/t
Processing Cost - Ore	Cost	Unit
Total processing cost	11.13	/t
Total processing cost	€ 10.12	/t
Processing fixed cost	€ 4.47	/t
G&A costs	€ 1.82	/t
Variable processing cost	€ 2.74	/t
Tailings management cost	€ 0.74	/t
Primary crusher feed,	€ 0.36	/t
Selling cost - mtu		
Selling cost	$ 3.14	/mtu

The break-even, Table 7-5, has been calculated for the different scenarios to compare with the Cut-off grade reported in the optimization.

Table 7-5 Break-even calculation

	Process	Total
COG - break-even – Calculated (US310$/mtu $ 58% rec)	0.08%	0.1%
COG - break-even (US310$/mtu $ 71% rec)	0.066%	0.081%
COG - break-even 330 (US330$/mtu $ 58% rec)	0.075%	0.093%
COG - break-even 330 (US330$/mtu $ 71% rec)	0.062%	0.076%

The break even calculated is slightly above the optimization cut-off reported by Whittle. Noticed that optimization algorithm has a variable cut-off calculation per period as there are different head grades per period and for final calculation this gives the average optimum cut-off. The cut-off as reported by Whittle has been used for mine scheduling after the design has been applied.

7.2.2 Variable factors sensitivity

The influence of having one or two ramps in the final design has been assessed.

As well as the following parameters have been varied, as described:

- Average Slope angle variation: 54 & 58
- Price scenario: 310US$/mtu & 340US$/mtu
- Recoveries: 58, 71, 78, variable

The results of this sensitivity testing is shown in Figure 7-12

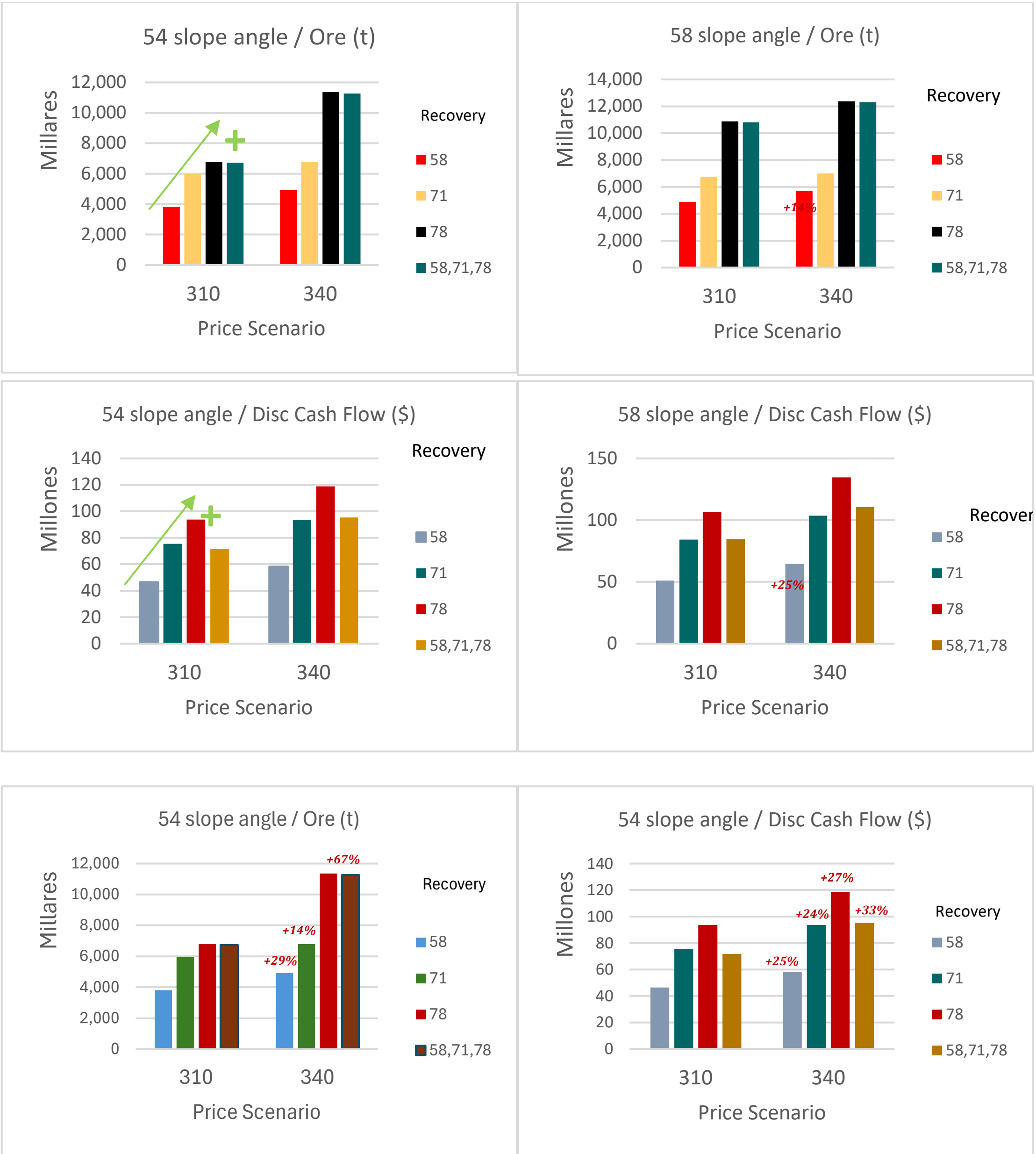


Figure 7-12 Pit optimization scenarios comparison

As shown in the Figure 7-12, the ore tonnes increase by 14% when comparing slope angle 58 vs 54 where the influence is higher for the 310US$/mtu price scenario. Cash Flow increase as an average of 15% in each case.

Assuming a realistic scenario with two ramps and average slope angle of 54 degrees for higher recoveries it is observed the impact on the ore tonnage increases up to 67%. Discounted cash Flow has a variation around the 25% for the different price scenarios.

Looking closer the recoveries variation it is seen that the 78% and variable recovery the ore tonnage reported are equivalent.

7.2.3 Pit optimization scenarios evaluation

The price discussed in section 6.1, it has been applied at 310US$/mtu price scenario for short term scenario and 330US$/MTU in long term scenario and used for selecting the ultimate pit-shell.

In the short term 58% metallurgical recovery has been used in pit optimization as relates to the first year of the plant improvement plan. Thereafter that the long-term metallurgical recovery of 71% is used.

For the long-term scenario, the status of the stockpile has been set for evaluation due are part of the ore reserves. It has been targeted 10 years of operation if feasible.

7.2.3.1 Stockpile status.

The status of the stockpiles included as part of the mining ore reserves, excluding marginal (MAR), are shown in Table 7-6 .

Table 7-6 Stockpile status as per December 2023

Stockpile status	Tonnage Dec2023	Grade	Concentrate	Concentrate grade
A	92,373	0.182		
B	125,695	0.101		
OP	54,684	0.095		
MAR	574,763	0.064		
Scalping	332,458	0.058	29,921	0.55

7.2.3.2 Short term Scenario

This short-term scenario considers a 54º slope angle, 58% metallurgical recovery and 310US$/mtu price scenario. The Figure 7-13, shows the different pit-shells and their reported revenues. The detailed optimization results can be found in the Appendix 6.

This scenario is evaluated to understand the first phase of pit design and it will be compared with the current operational design as part of the change management process in adopting this ORE. Pit shell 35 is selected gives the maximum discounted cash-flow and will supply 3 years of ore to the plant.

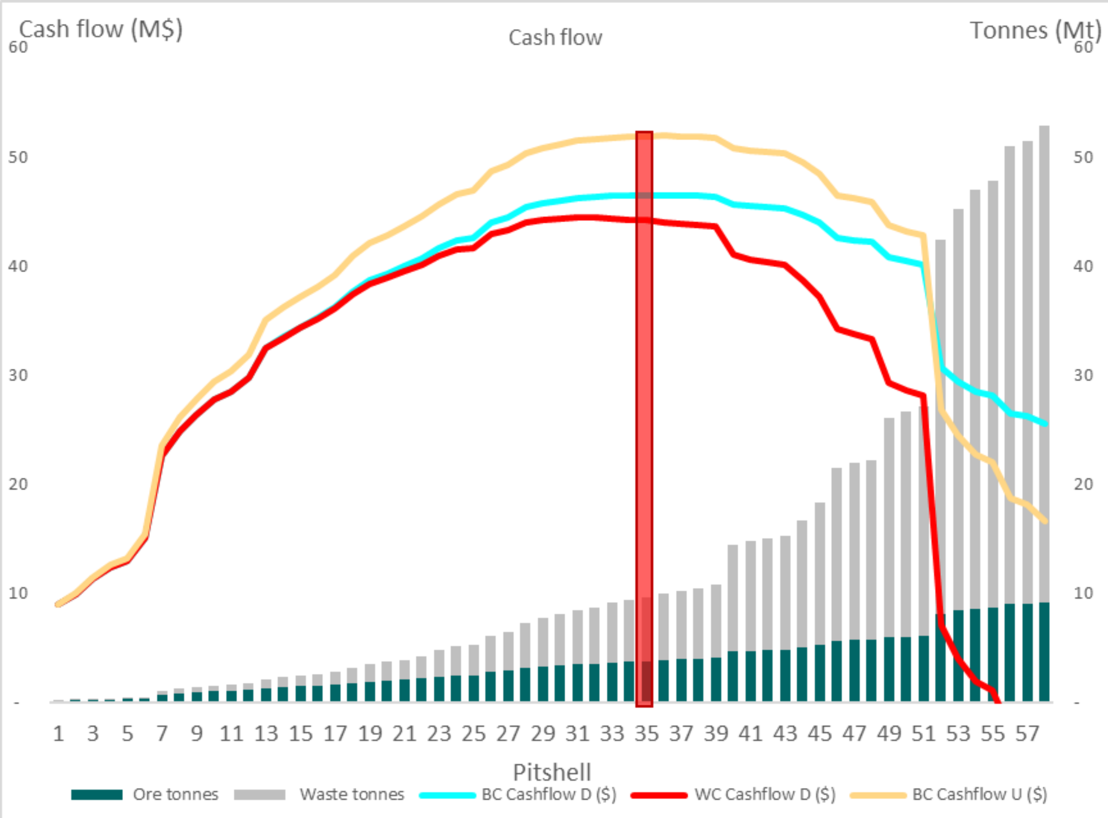


Figure 7-13 Pit by Pit Short-term graph

In **Table 7-7** summarises results for the short-term pit shell selected.

Table 7-7 Pit-shell selected Short-term Scenario

pit-shell	Disc cashflow best case	Disc cashflow worst case	Total (t)	Total waste(t)	Ore (t)	Aver grade %WO_3	COG
35pit	46,478,489	44,173,420	9,650,754	5,835,628	3,815,126	0.243	0.074

Figure 7-14 and Figure 7-15 shows the current phase design versus short-term optimised pit-shell selected in plan and section views.

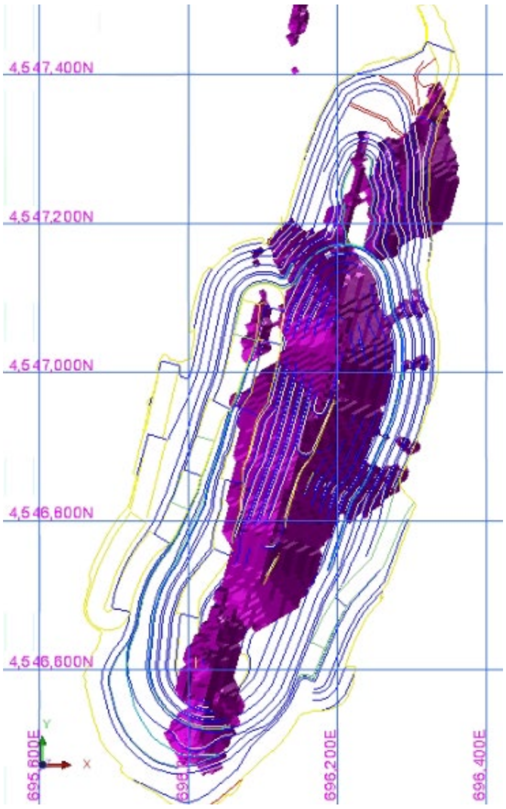


Figure 7-14 Shrot-term pit-shell selected compared with current design plan view

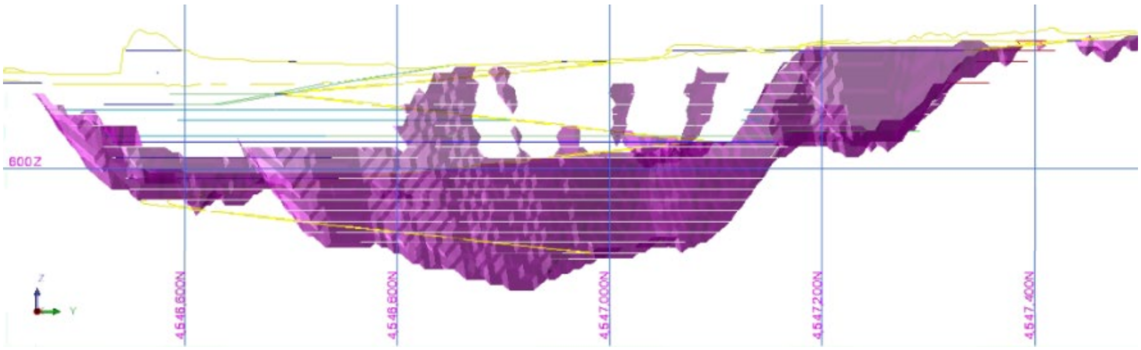


Figure 7-15 Pit-shell 35 maximum Cash flow compared with current design section view

Table 7-8 reports the contained ore by resource category.

Table 7-8 Resource Category report: pit-shell slo_54_58_310_mc_35ps_bc.dtm

Pit-shell		Cut-Off 0.06	Ore (Tonnes)	mtu	Average grade	%ore per resource category
Slope	54	Measured	4,111,030	985,379	0.24	90%
Recovery	58	Indicated	425,382	90,630	0.21	9%
Revenue	310	Inferred	44,038	8,349	0.19	1%
		Total	4,580,450	1,084,358	0.24	100%

This pit-shell selected is well aligned with the current design actually in production.

7.2.3.3 Long term Scenario

This long-term scenario considers a 54º slope angle, 71% metallurgical recovery and 330US$/mtu price scenario and it was made including the material selected as ore for the short-term scenario.

Figure 7-16, shows the different pit-shells with their reported revenues. The detailed optimization results can be found in the Appendix 6.

Highlighted in orange are the pit-shells that give the maximum undiscounted cashflow (pit-shell 36) and the pit-shell selected as ultimate (pit-shell 45).

Criteria used for selection is based on the target of more than 10Mt of ore for processing plus a balance in between ore tonnes incrementally added to the next pit-shell versus waste material increased. Notice that pit-shell 46 cashflow drops heavily compared with the selected shell 45, the amount of ore increase versus the amount of waste is adding cost and less value to the project.

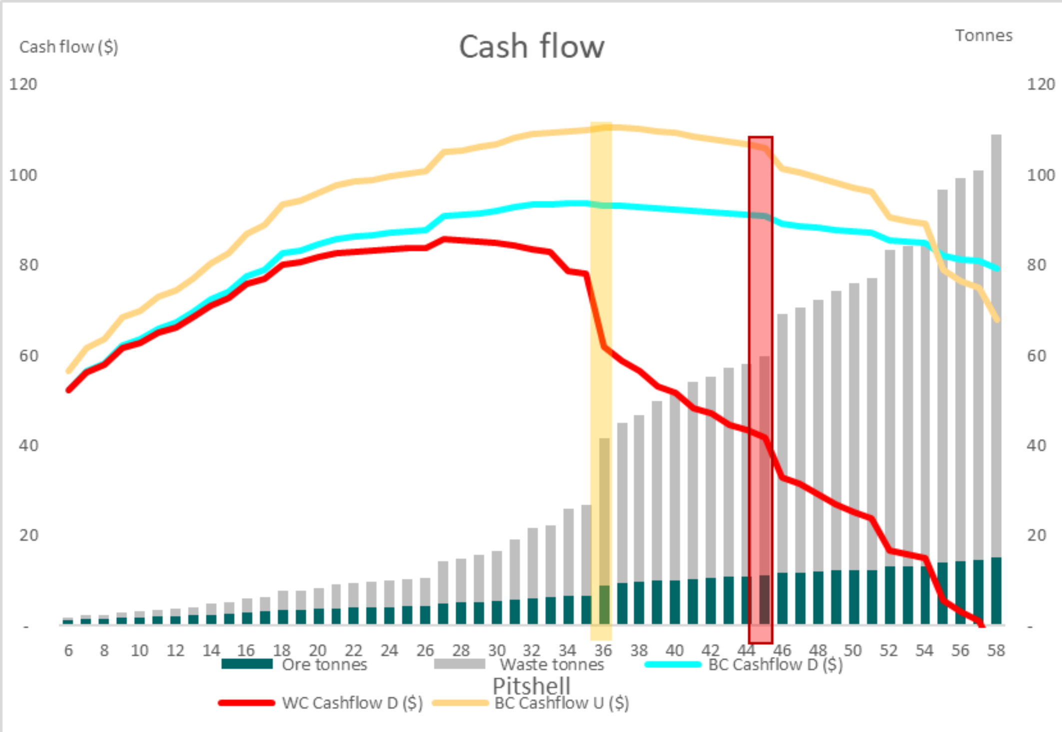


Figure 7-16 Pit by Pit Long-term Whittle Scenario graph

Table 7-9 summarises the results for the pit-shell selected.

Table 7-9 Pit-shell selected Long-term Scenario

pit-shell	disc cashflow best case	disc cashflow worst case	Total (t)	Total waste(t)	Ore (t)	Aver grade %WO_3	COG
45pit	90,909,797	41,813,189	60,009,539	48,643,129	11,108,715	0.153	0.059

As a comparison the current operations design is shown with, the two pit-shells, maximum cash flow (pit-shell 36), pit-shell selected (pit-shell 45) in plan view, Figure 7-17, and in section view, Figure 7-18.

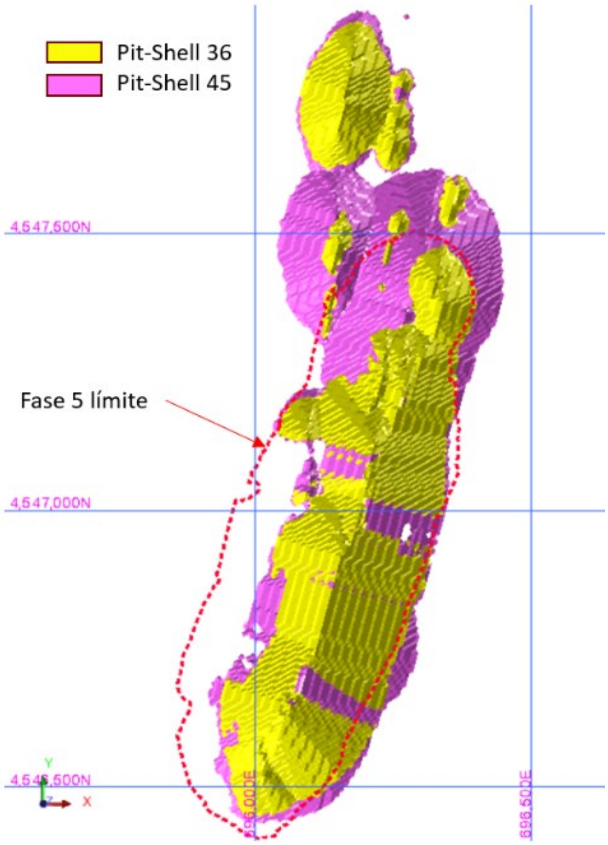


Figure 7-17 Pit-shell 36 versus Pit-shell 45 selected plan view

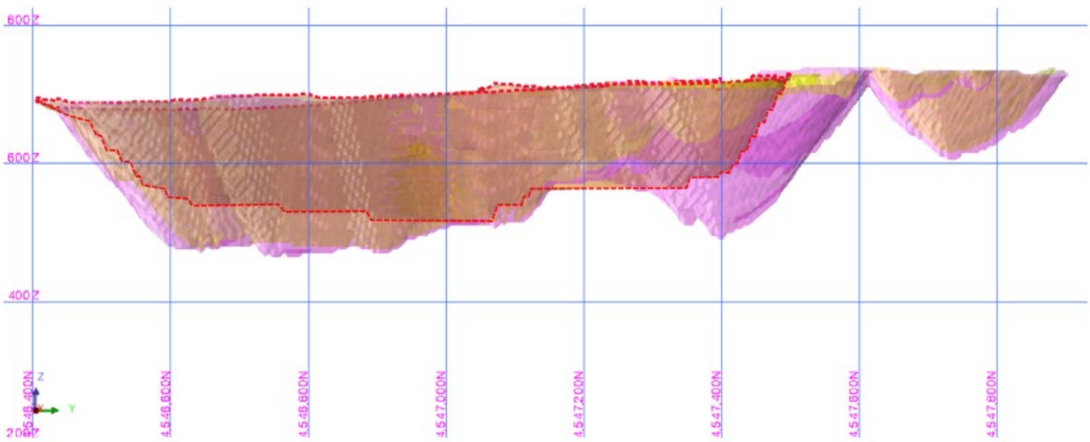


Figure 7-18 Pit-shell 36 versus Pit-shell 45 selected, section view

The long-term pit-shell selected, pit-shell 45, has been reported by resource category in the Table 7-10.

Table 7-10 Pit-shell 45 by resource category

Pit Shell		Cut-Off 0.06	Ore (Tonnes)	mtu	Average grade	%ore per resource category
Slope	54	Measured	7,274,075	1,407,169	0.193	67%
Recovery	71	Indicated	3,649,770	676,644	0.185	33%
Revenue	330	Inferred	-	-		0%
		Total	**10,923,845**	**2,083,813**	**0.19**	100%

In summary:

- This long-term scenario selected will guide the final practical design.
- The short-time scenario has shown it is closed to the current design in operation. Is for that the design slo_5ph_bottom.dtm will be defined as first phase for developing the mine design.

7.2.4 Economic scenario schedule

Once the pit-shell is selected, the schedule is run in the optimization, see Table 7-11. This optimization has no practical phase design but provides guidance as to plant feed dynamics and the use of the stockpile. The maximum material mined has been set at 8Mt per year of total rock and plant feed capacity to 1.3Mt per year.

Table 7-11 Whittle Schedule

Period	Tonne input (Mt)	Waste (Mt)	SR	Grade input WO_3 (%)	OP CF ($)	OP Disc CF ($)	OP Disc Cumm CF ($)	OP CF Cumm ($)	Tonne process (Mt)	HG stock (t)	LG stock (t)	MAR stock (t)	SCALP stock (t)	To HG Stock (t)	To LG Stock (t)	To MAR Stock (t)	To SCALP Stock (t)	From HG Stock (t)	From LG Stock (t)	From MAR Stock (t)	From SCALP Stock (t)	Minimum WO_3 Cut-Off (%)
1	1.30	6.70	5.14	0.215	15.87	14.69	14.69	15.87	1.30	92.37	180.38	242.31	29.85	0	0	0	0	0	0	0	67	0.068
2	1.30	6.70	5.14	0.226	18.34	15.72	30.42	34.21	1.30	92.37	180.38	242.31	29.85	0	0	0	0	0	0	0	8	0.068
3	1.30	6.70	5.14	0.209	13.84	10.99	41.40	48.05	1.30	92.37	180.38	242.31	29.79	0	0	0	0	0	0	0	55	0.068
4	1.30	6.70	5.14	0.21	14.41	10.59	52.00	62.46	1.30	92.37	180.38	242.31	29.72	0	0	0	0	0	0	0	76	0.068
5	1.30	6.70	5.14	0.193	10.11	6.88	58.88	72.57	1.30	92.37	180.38	242.31	29.72	0	0	0	0	0	0	0	0	0.068
6	1.30	6.70	5.14	0.155	0.86	0.54	59.42	73.43	1.30	92.37	180.38	242.31	29.29	0	0	0	0	0	0	0	427	0.068
7	1.30	6.70	5.14	0.187	8.77	5.12	64.54	82.20	1.30	92.37	180.38	242.31	28.93	0	0	0	0	0	0	0	358	0.068
8	1.22	2.79	2.28	0.194	20.91	11.30	75.83	103.11	1.30	39.99	180.38	242.31	-	0	0	0	0	52,383	0	0	28,930	0.068

7.2.5 Whittle optimization versus Block Model Reporting

Table 7-12 shows a comparison of the Whittle results, algorithm compare with the block model report, by Surpac software using the optimised shell dtm. The deviation of approximately 1%, is considered acceptable.

Table 7-12 Whittle Report vs Reserves block model report

Whittle vs Block model reporting comparison		Tonnes	mtu WO_3	Av WO_3 (%)
Whittle report	Ore	11,108,715	2,099,547	0.19
	Waste	48,643,129	-	-
Block model report	Ore	10,923,858	2,082,901	0.19
	Waste	48,365,967	124,924	-
Comparison	Ore	-2%	-1%	1%
	Waste	-1%	0%	0%
Total difference		-1%	-1%	1%

7.3 Existing mine layout and accesses

Figure 7-19 identifies key project infrastructure and facilities with the mine face position as of 31 December 2023.

The access through the main ramp to the pit is located in the Western area and follows the haul road besides the pit to the North and connects with the two entrances to the waste storage facility and the stockpile area where the ore is placed close to the primary crusher.

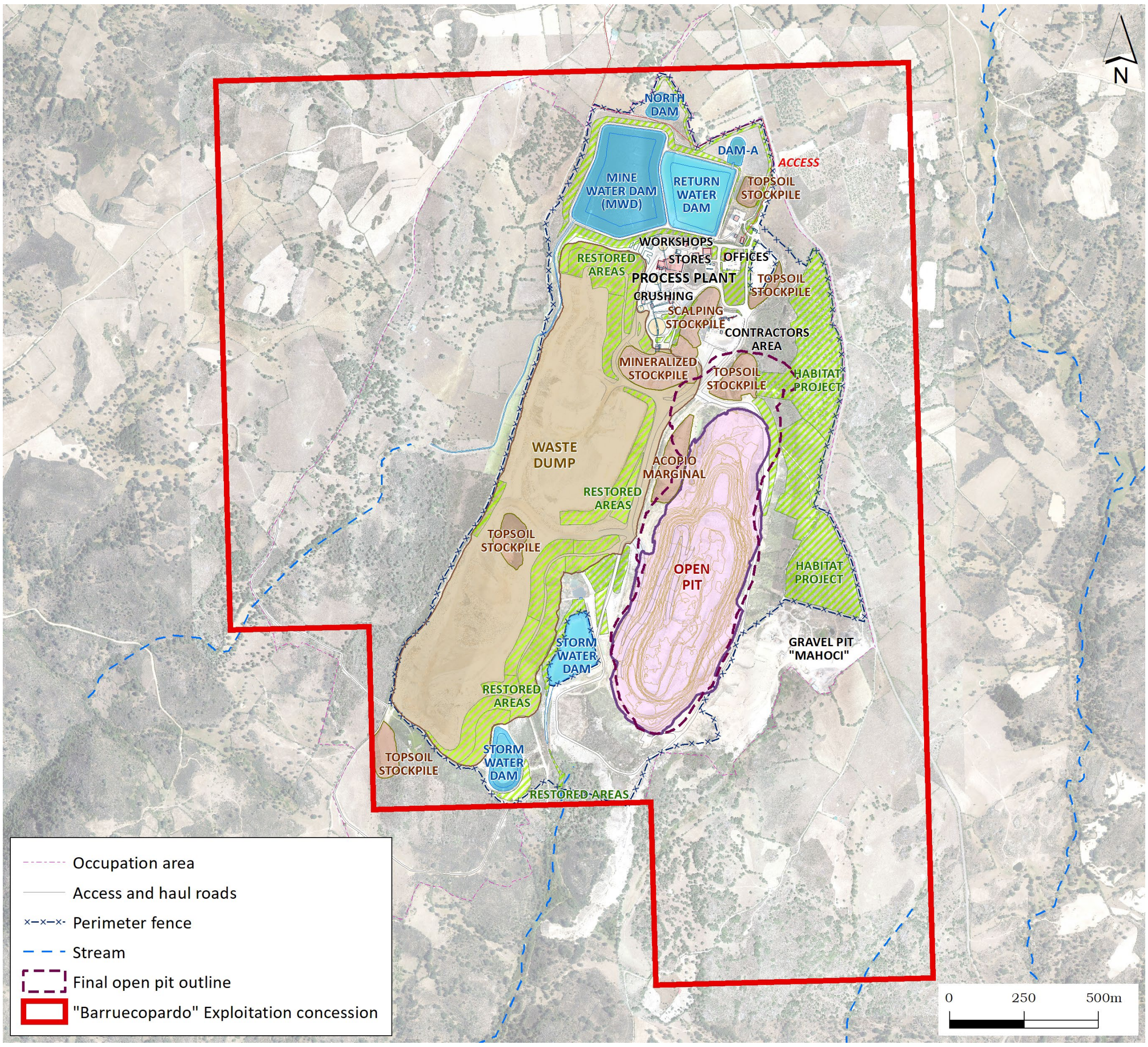


Figure 7-19 Barruecopardo mine lay-out

7.4 Ramp design criteria

The mine contractor haul fleet equipment consists of two slightly different truck models, and the ramp design considers the largest of these dimensions. These are shown in Table 7-13

Table 7-13 Trucks specifications and minimum dimension for ramp design

Fleet equipment	Width (m)	Lenght (m)	Turning radius		Minimum extra widening in ramp	Safety berm in ramp	Minimum shoulder in ramp
KOMATSU HD785-7	6.885	10.29	10.1		5.24	3	5.2
CAT 777G	6.2	10.53	14.2		3.90		

Table 7-14 summarizes the design criteria applied, following the guidance of the geotechnical report summarized in section 5.

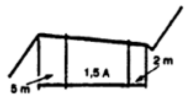
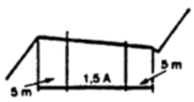
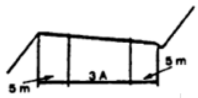
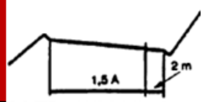
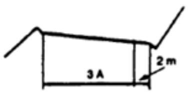
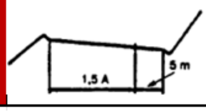
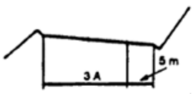
Table 7-14 Design criteria summary

Design criteria		
Ramp width	25	m
Single line ramp width	15	m
Working slope (bench face)	75	º
Overall angle	54	º
Inter-ramp	58	º
Ramp gradient	10	%
Berm	7	m
Minimum mining width	25	m

The design criteria shown in the Table 7-14 are the same criteria currently being used in the mine where A it refers to the track width.

Last four benches in the bottom of the pit have been designed with a 15m ramp width, that is allowing for single truck only passage. For reference, Table 7-15, shows the different ramp width design criteria according to the Spanish regulation "ITC Chapter VII RGNB Seguridad Minera RD 863/1985", where "A" is the bigger size truck width and shoulder is referred to a safety bound.

Table 7-15 Ramp width justification ITC RD 863/1985

Road section		Single line (m) Normal traffic		Two lines (m)	
With safety berm	withouth shoulder		17		28
	with shoulder		20		31
Without safety berm	withouth shoulder		**12**		**23**
	with shoulder		15		26

7.4.1 Final Pit design

Final pit design (Pit 11 version 11, Figure 7-20 & Figure 7-21) has been performed via several iterations so as to optimize material ore/waste balance and is aligned with the optimised pit-shell selected.

After that, practical phases have been designed for planning purposes with a minimum of 25 meters in between phases.

Once phase design is included in Whittle the Whittle DCF drops 1.6M€ if phase 5 is included, therefore it has been excluded.

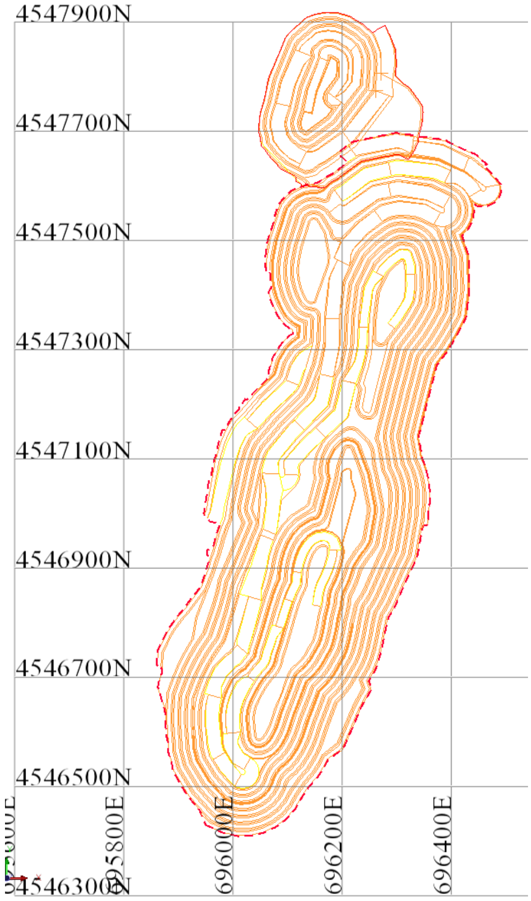


Figure 7-20 Initial Pit Design plant view

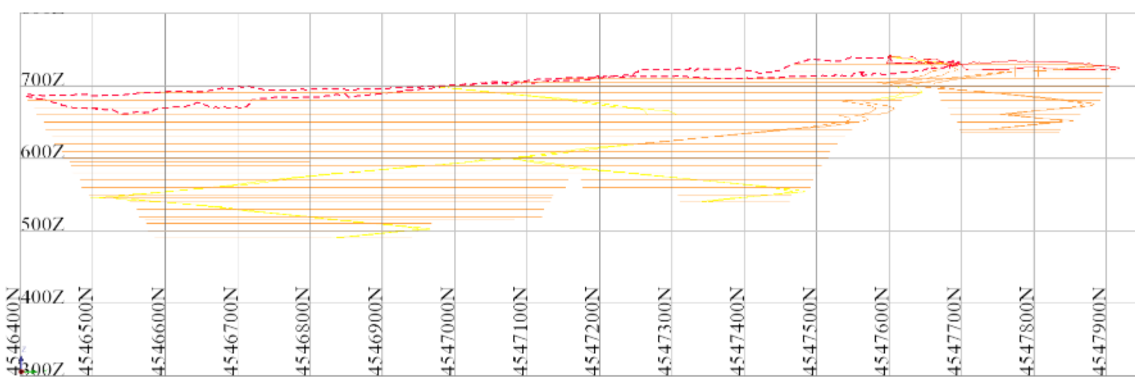


Figure 7-21 Initial Pit Design section view

As a result, phase 5 is not taken into consideration in the production plan, final design considered for schedule is shown in Figure 7-21 in plain view. Section view of the final design it is shown in Figure 7-22.

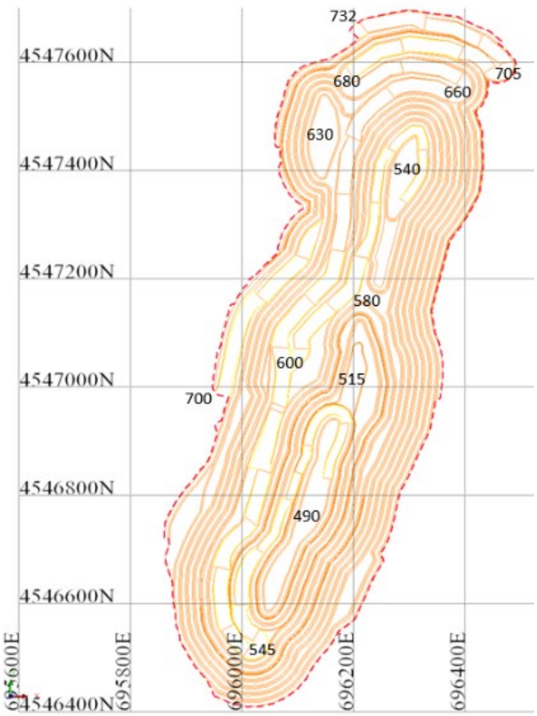


Figure 7-22 Final Pit Design

Figure 7-23 shows the strings of the final pit design compared to the pit-shell selected, where it can be seen how the North area is sterilized. Figure 7-24 represents the section view of the design compared to the pit-shell selected.

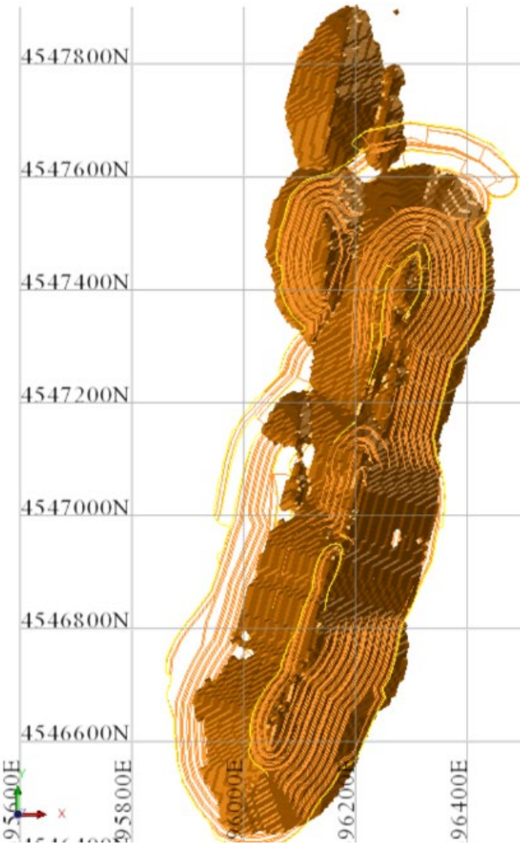


Figure 7-23 Final Pit Design vs Pishell plan view

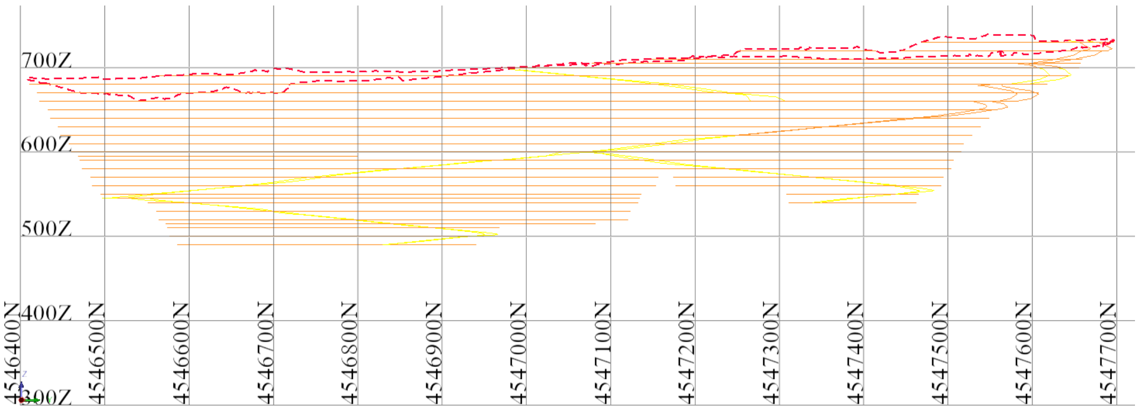


Figure 7-24 Final Pit Design section view

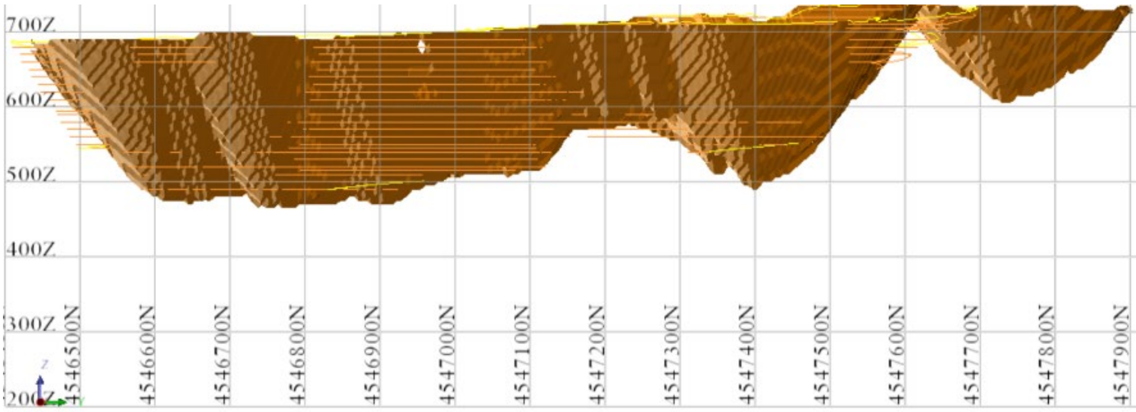


Figure 7-25 Final Pit Design vs Pishell section view

Figure 7-26 shows in purple the blocks where part of the pit-shell selected and are not included in the final design, that is the Phase 5. The material excluded comprises, including loss and dilution, a total of 339,945t of ore at an average grade of 0.25% WO_3 and 5.4Mt of waste.

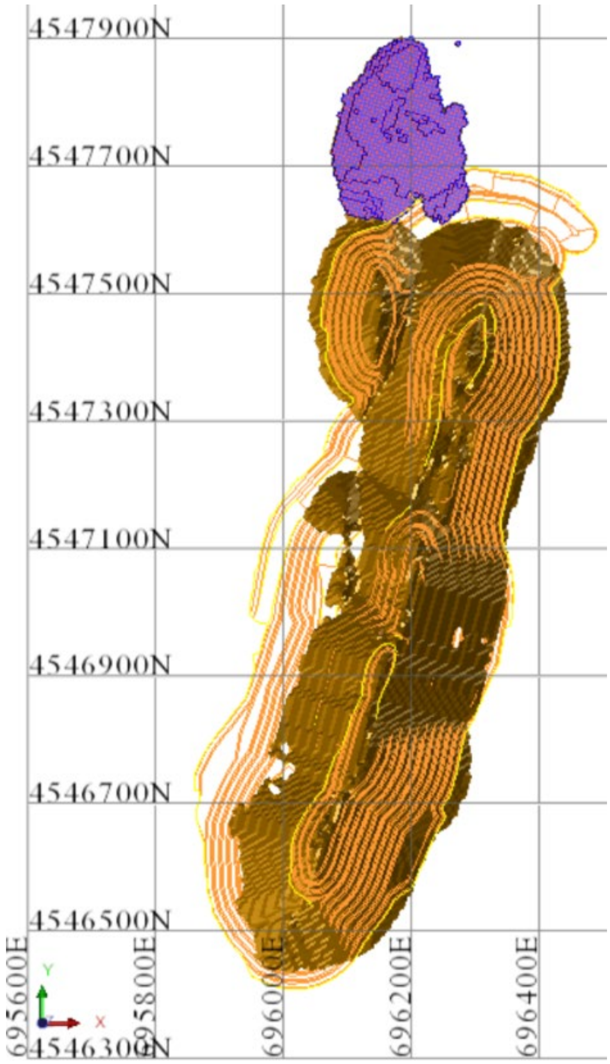


Figure 7-26 Blocks excluded for pit-shell comparison, ultimate pit-shell and final design

Table 7-16 compares the reserves block model cut with the final pit-shell to the final pit design. These figures do not include operational loss and dilution, and the North area is excluded.

Table 7-16 Optimization vs Design comparison

Optimization vs Design comparison		Tonnes	mtu WO_3	Av WO_3 (%)
Optimization	Ore	10,609,385	1,991,439	0.19
	Waste	43,272,186	-	-
Design	Ore	10,236,302	1,846,080	0.18
	Waste	54,237,305	-	-
Comparison	Ore	-4%	-7%	-5%
	Waste	25%		
Total difference		20%	-7%	-5%

A total of 4% less ore tonnes with a drop of 5% in the average grade is included when the pit shell is converted to an operational design, and 25% extra waste material added.

7.4.1.1 Phases overview

The following figures show the scale and dimensions of the different phases considered for the reserve estimation.

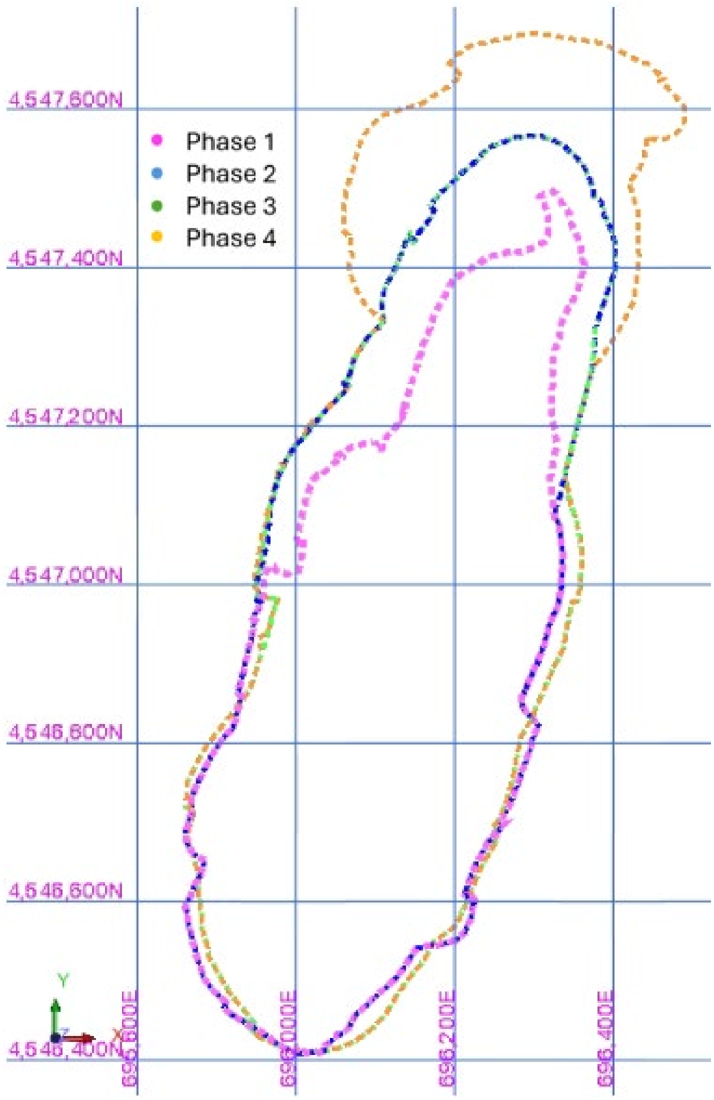


Figure 7-27 Phases design overview Plan view

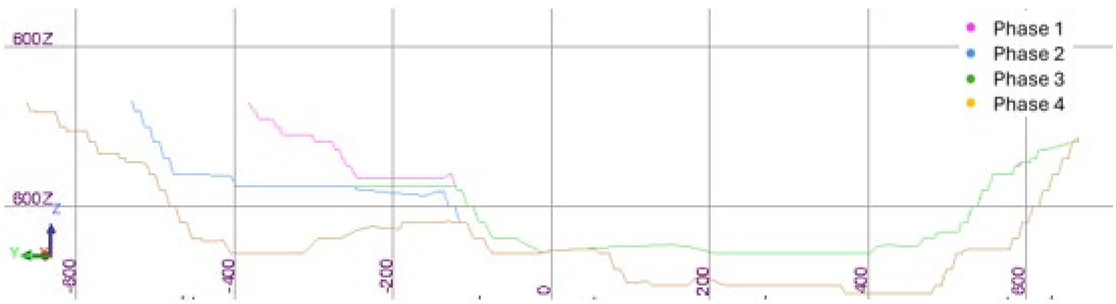


Figure 7-28 Phases design overview section view

Table 7-17 summarizes the type of material reported by phase and split in low grade for ore with grade above 0.059%WO_3 and High grade above 0.15% WO_3.

Table 7-17 Design physicals by phase

		Loss and dilution included					
	Phase	LG ore	HG ore	Total ore	Waste	Total	SR
Tonnage	1	1,596,533	2,221,490	3,818,023	5,408,365	**9,226,388**	1.42
	2	1,142,083	589,941	1,732,024	12,304,245	**14,036,269**	7.10
	3	1,427,412	1,233,157	2,660,569	19,386,105	**22,046,674**	7.29
	4	1,817,273	1,037,554	2,854,827	16,309,449	**19,164,276**	5.71
	Total	**5,983,301**	**5,082,141**	**11,065,442**	**53,408,165**	**64,473,607**	**4.83**
mtu	1	147,857	644,152	792,009			
	2	101,263	125,810	227,073			
	3	130,596	291,116	421,711			
	4	165,117	240,169	405,286			
	Total	**544,833**	**1,301,247**	**1,846,080**			
WO_3 Grade	1	0.093	0.290	0.21			
	2	0.089	0.213	0.13			
	3	0.091	0.236	0.16			
	4	0.091	0.231	0.14			
	Total	**0.091**	**0.256**	**0.17**			

The next section describes each phase

Phase 1 -The proposed phase for exploitation continues to follow the mine's current philosophy, assuming the current phase 5 as phase 1 of the new reserves. This strategy allows the current operation to smoothly transfer to the design that includes the new reserves of the project.

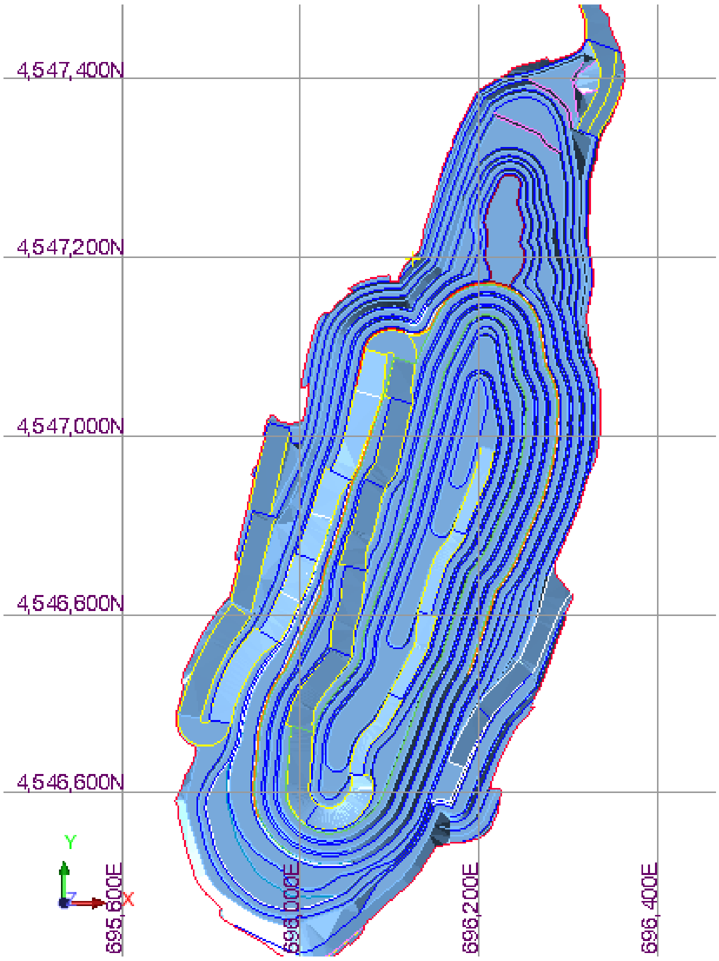


Figure 7-29 Phase 1 - Reserve Estimation

Phase 2 - After a number of iterations and considering the development of the different phases selected in Whittle to minimize risk, it is observed that the initiation of phases, after the phase 1, focuses on the northern area with a small phase.

To ensure access and due to the significant distance between the western and eastern exits for moving material to the stockpile and waste dump, the final decision was to enter to the new phase (phase 2) from the west, which minimize de hauling distance to the waste dump and the stockpile.

Another objective for developing this second phase was to secure enough ore to supply at least one year of production to the plant. After several tests and seeking the highest possible operability, a phase 2 was designed to connect with the ramp of phase 1 at elevation 625 (currently phase 5), thereby improving access and minimizing waste. Following the same criteria than in the phase 1, the phase 2 for operational purposes will be renamed as phase 6.

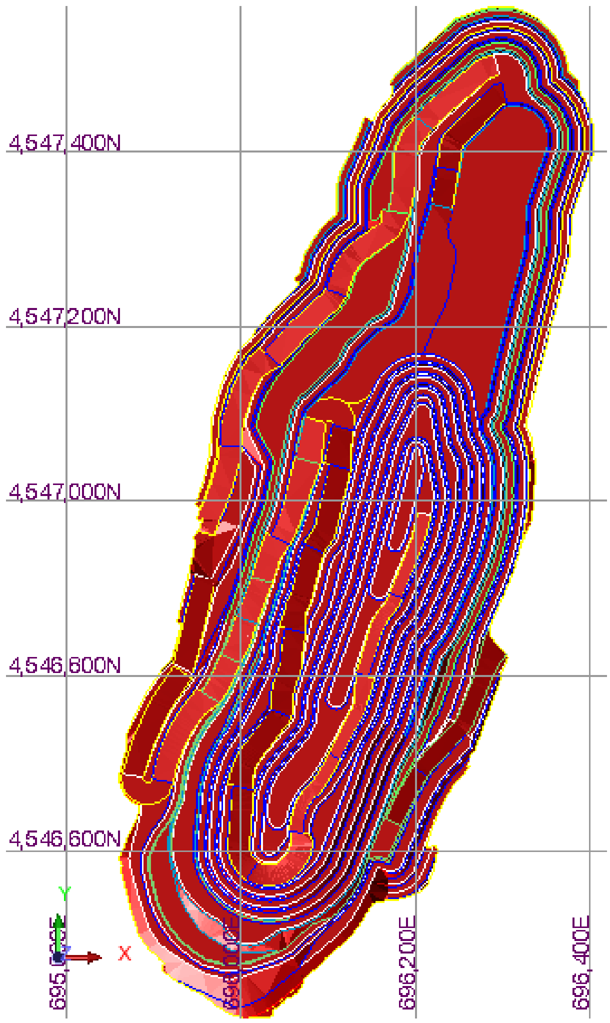


Figure 7-30 Phase 2 - Reserve Estimation

This second phase provides 1.7 Mt of ore and 12.3 Mt of waste including loss and dilution, maintaining a O:W ratio of 1:7.1.

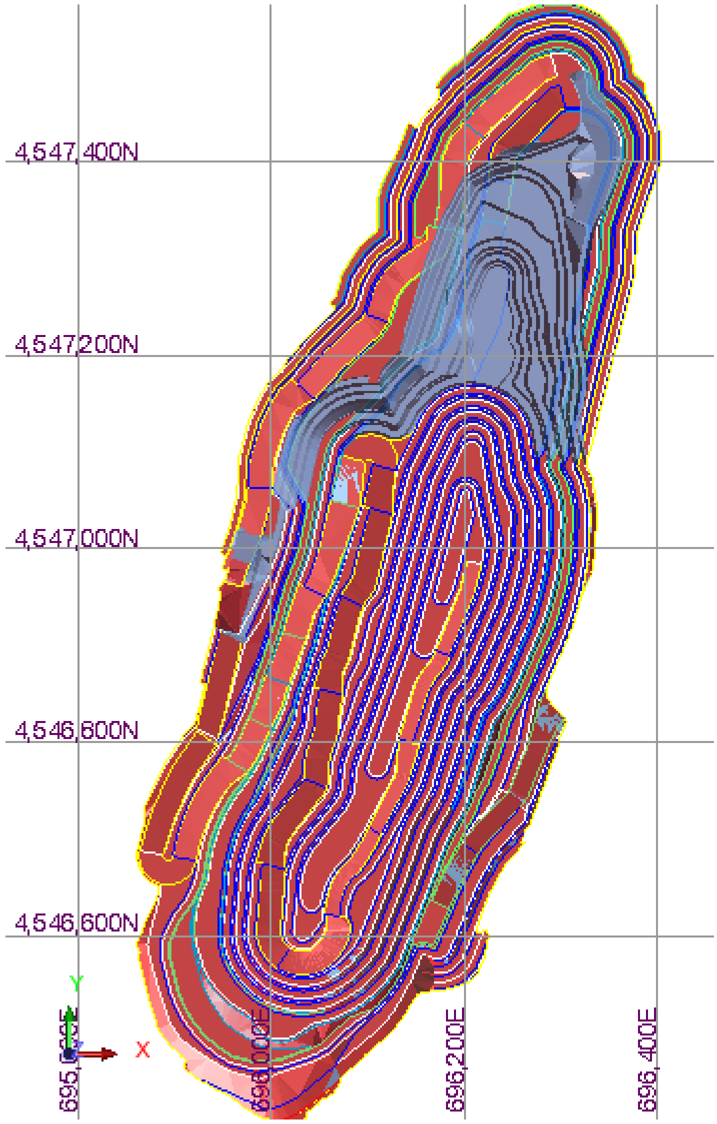


Figure 7-31 Phase 2 - Comparison with Phase

The previous figure shows the inclusion of phase 2, corresponding with the ramp connection through the north with the current switchback at level 625, and maintaining the south as it is in the phase 1.

Phase 3- Once this second phase is obtained, and with the goal of maintaining multiple operational phases simultaneously, we aimed to develop a phase in the south that connects with phase 2 to the level 625 and provides sufficient workspace (25m) between this phase and phase 1, which is executed in the south.

After several trials, it was determined that the southern contour of the final design did not allow for an intermediate phase with enough space. Therefore, the southern contour of the final phase was adopted, and a connection was made with phase 2. This approach resulted in a phase development that alternates work in the northern and southern areas. The phase 3 for operational purposes will be renamed to phase 7.

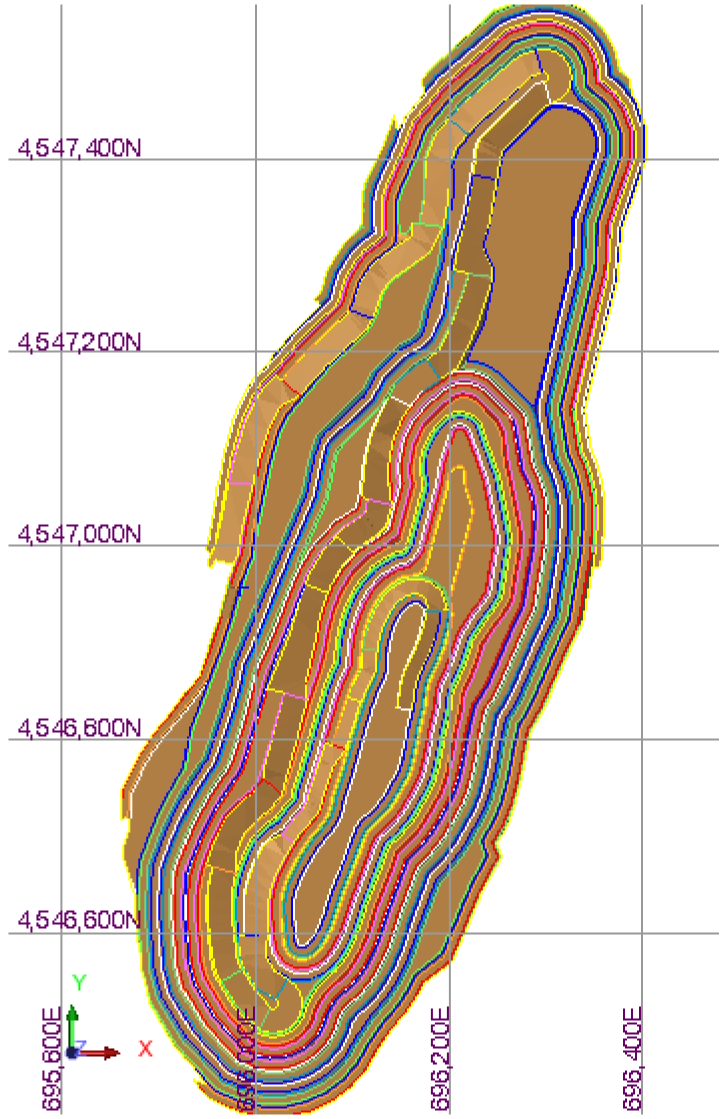


Figure 7-32 Phase 3 - Reserve Estimation

After defining these two phases, the tonnage evaluation was performed again to maintain an equivalent waste/ore ratio across all phases, resulting in phase 3 having 2.7Mt of ore and 19.4Mt of waste including loss and dilution, that means O:W ratio of 1:7.29.

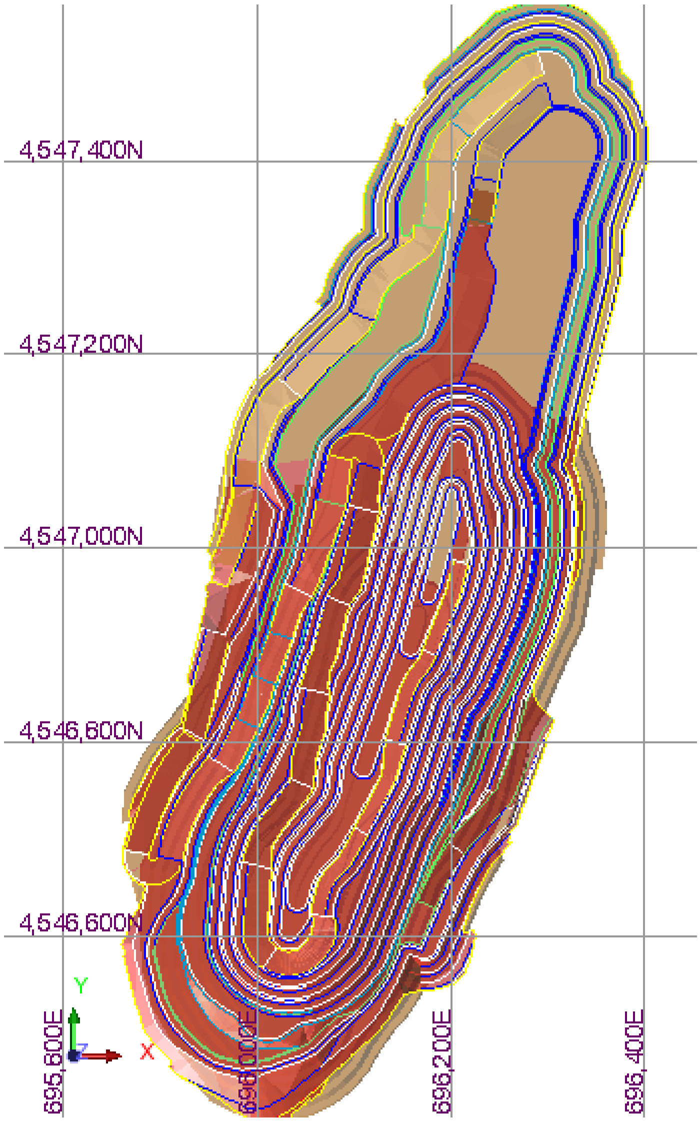


Figure 7-33 Phase 3 - Comparison with Phase 2

The Figure 7-33 shows the expansion of the phase 3 in comparison to phase 2, maintaining the same shape in the north and expanding to the south.

Phase 4- Final phase- To conform to the final phase's contour in the northern area, which extends to a depth of 540, the goal was to minimize additional waste for phase connections. The objective of this new phase was to conform to the predefined contour and connect the ramp with the ramp of phase 3. Consequently, the ramp of the final phase was redesigned, creating a bifurcation at platform 610 to access the bottom of the centre part of the design and at the same time to connect the ramp with phase 3 at elevation 690. Final pit/phase 4 at operation will be renamed as phase 8.

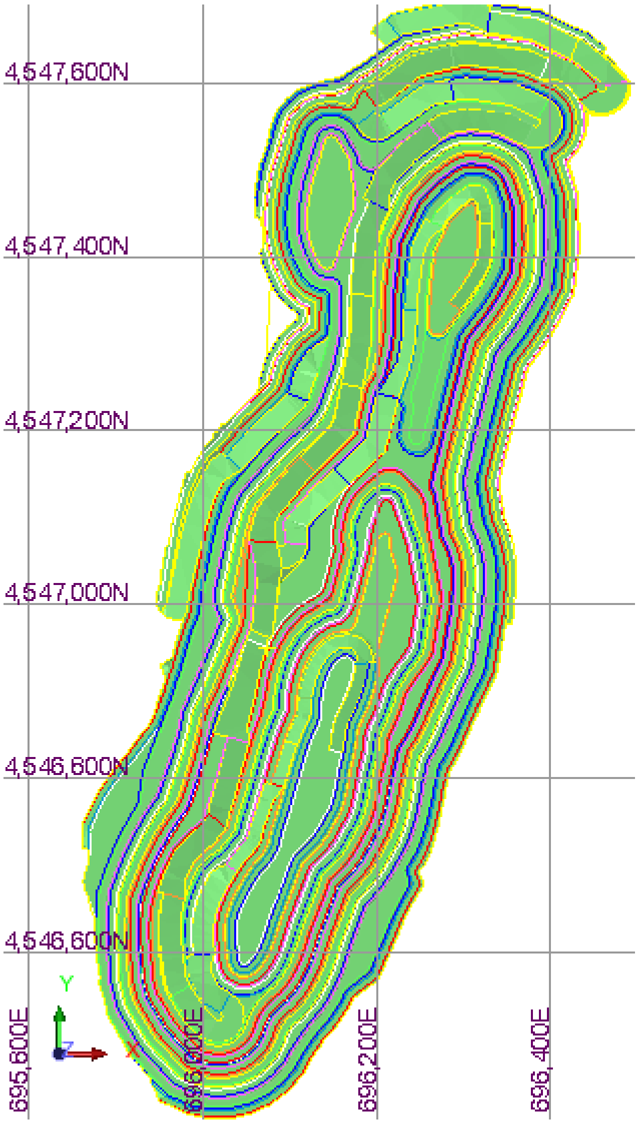


Figure 7-34 Final Phase (Phase 4) - Reserve Estimation

As a result, the final phase provides a movement of 2.9Mt of ore and 16.3 Mt of waste including loss and dilution, and ratio O:W of 1:5.71.

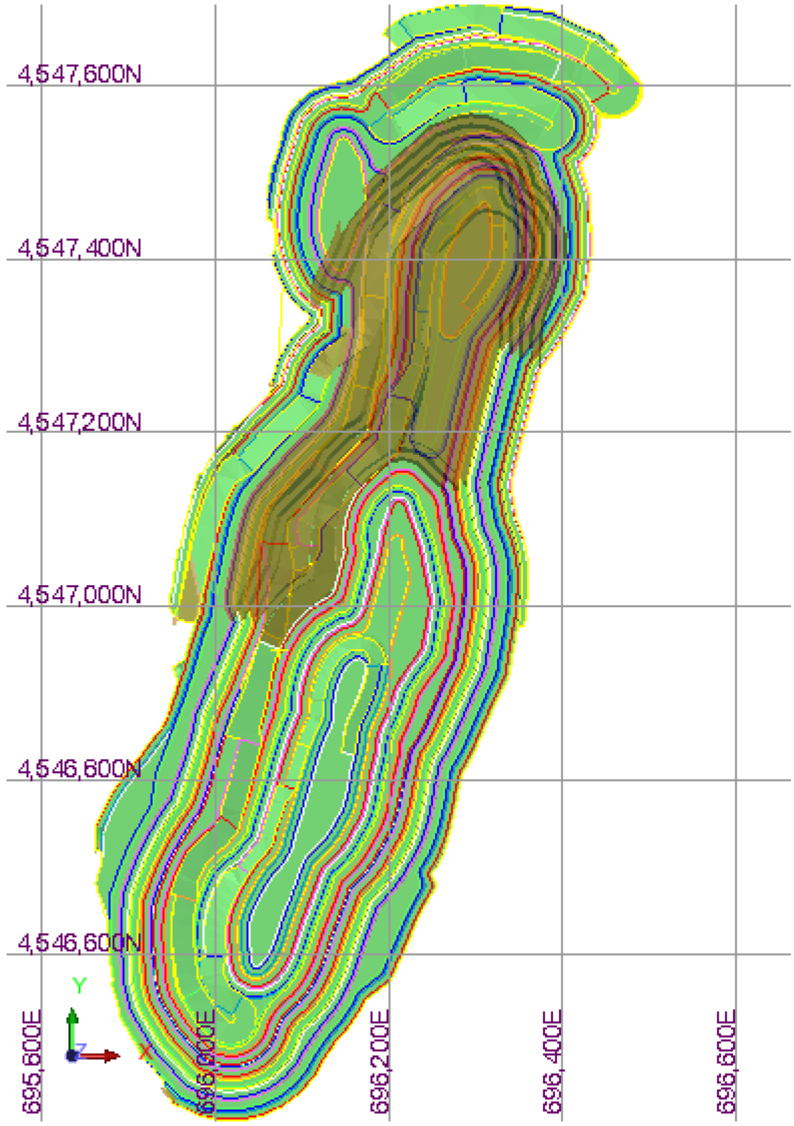


Figure 7-35 Final phase - Comparison Phase 3

As there can be seen at the Figure 7-35, the expansion of the final phase in comparison with the previous phase (Phase 3) is a pushback to the north.

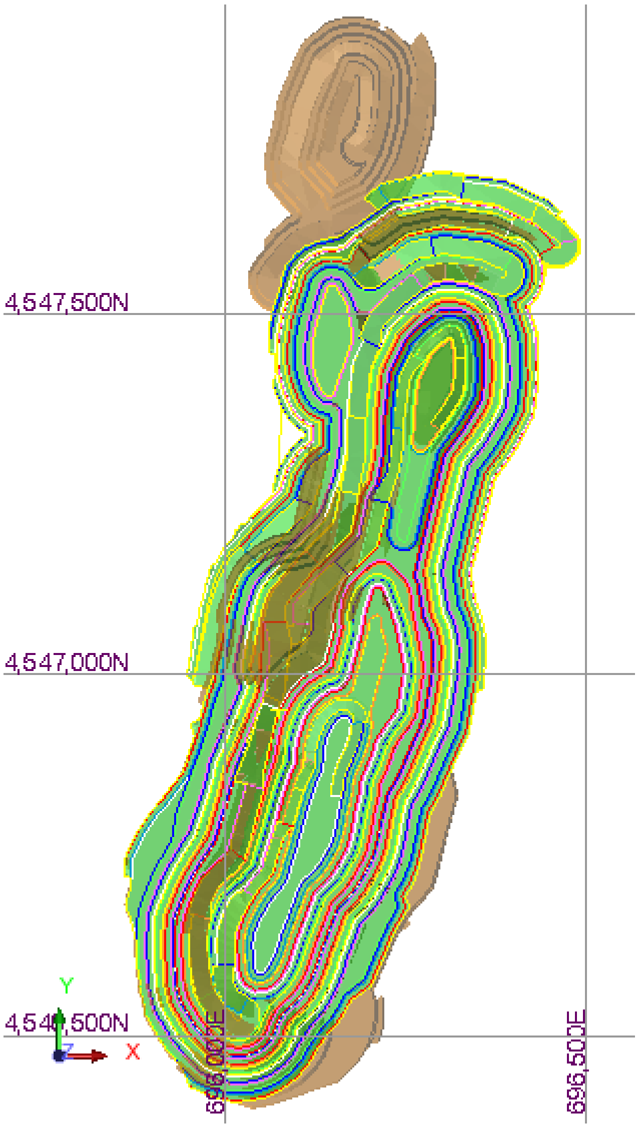


Figure 7-36 Final Design P11 Comparison with Final Design

The final design which was previously performed has been changed to maintain accessibility of all the phases and to reduce the waste if possible

Design phases criteria - The design criteria for all phases followed the geotechnical guidelines established in the geotechnical report as discussed previously.

7.5 Water management

The water management system is based on controlling water flows to separate clean water from the process water. Aiming to minimise the discharge of used water into the natural environment and optimize the use of water in all process during the LoM.

Surface drainage system to collect run-off water outside the pit and all facilities are maintained to optimize the water balance and to minimize the environmental impact. See Figure 7-19

The drainage network consists of 4 water ponds lined with high-density geosynthetic plastic (PEAD) equipped with their own pumping systems. Several local sumps and an external drainage system collects pit bottom water and rainfall and delivers that water to the ponds. After settlement this is then sent to the water treatment plant, from where it goes to either the process plant or discharged off-site.

- Main water dam (MWD) with capacity to contain 664,900m^3 clean water is placed on the North of all mining facilities. This dam supplies the clean water for the process plant and for dust control equipped with electric water pump system.
- Pond A. This contained water from the process and the sources of the project, has capacity to contain 261,000m^3 placed besides the main water dam to its East. This deposit is equipped with electric water pump system for pump to the water treatment plant.
- Pond B and D are the ponds collecting underground water and run-off water and it is placed downstream of the waste dump. They have capacity to storage 91,000m^3 and 82,000m^3 and water from them is pumped to Pond A for after that being pumped to the water treatment plant.
- North sump. Deposit placed North MWD and pond A. Collects natural basin water and it is discharged as it is clean water in the ditch besides waste dump or can be pumped to MWD if it is required.
- Bottom of the pit sump. To keep active faces, dry in pit operations water must be pump from the bottom of the pit using diesel pump systems to pond A.
- Process plant sump. Between process plant and pond, A it is placed a small sump to collect run-off water from process plant area and waste dump North area and will be pumped to pond A.
- West overflow channel. This 1.3km length channel, in case a big rainfall event occurs, will be used as MWD overflow channel. Discharge point is placed in the natural bed around deposit.
- External drainage system. Approximately 1.8km of open ditches controls the run-off water to divert water from the operations toward South area and North sump.
- Internal drainage system. Approximately 3.0km of ditches manage the run-off water that ends inside the project and are pumped to ponds B, D, process plant sump and finally pumped to pond A for water treatment plant final destination.

The water table level is monitored through a series of perimeter observation holes. An underground and surface monitoring plan is in place to detect any early-stage change in the performance of the aquifers.

As a result, water has been successfully managed since operation started and has never really interrupted production on a prolonged basis.

8 Mine Schedule

The pit has been scheduled out to the Life of Mine (LoM) exhausts the reserves. Scheduling has been at monthly for the first two years, quarterly the following two and yearly for the remaining LoM. Reports are shown here are summarised at an annual level. The existing stockpiles form part of the ore reserves, Table 8-1, shows the status as of 31 Dec 2023. These have been depleted to their levels as of 31 May 2024, for the mining conducted in the interim, and have then been included in the mine plan.

The production plan targets 1.45Mt of ore the first year and then ramps up to the target of 1.8Mtof ore per year of ore feed to the process plant. Ore feed could come from either existing stockpiles, or ore direct mined from the pit. The business objective is to produce 107,520 mtu of payable concentrate per year at a con grade of 64% WO_3.

Table 8-2 shows the LOM mine plan by phases in each year, with Table 8-3 showing the plant feed and concentrate production for the same periods. The mine plan table shows the potentially deleterious elements of arsenic, sulphur and phosphorus. This table also shows the pit bottom RL for each phase at the end of each year, to appreciate vertical advance.

In this production plan, material coming from the pit has been prioritised for feeding the crusher. Higher grades are available in the first years and the stockpile is active during the first year to minimize the size of the stockpile.

The stockpiles securing consistent plant feed if any disruption occurs in the pit, and in the last two years it optimizes the process plant head grade.

Table 8-1 Stockpile status included in the Production Plan

Stockpile status	Tonnage Dec 2023	WO_3 Grade	Concentrate	WO_3 Concentrate grade
A	92,373	0.182		
B	125,695	0.101		
OP	54,684	0.095		
MAR (not included)	574,763	0.064		
Scalping (concentrate included)	332,458	0.058	29,921	0.55
To plan				
HG (A stockpile + Scalping)	122,294	0.272		
LG (B stockpile + OP stockpile)	180,379	0.099		

To note:

- Phase 2 starts during July 1st year
- Current marginal ore stockpile updated on September 24 material has been included in this plant feed plan during the years 5 and 6.

- Fleet equipment capacity and assignment has not been calculated nor considered a limit on the plan. The current installed fleet has a maximum annual capacity of some 9Mt which should be adequate for first year but may be adjusted in future years . Truck fleet numbers per period considering the haulage to destinations should be calculated in the medium-term planning. As can see in the resulting mine plan, total material movement does reduce last two years, and this will be offset by longer haulage duties for trucks.
- Drill capacity has not been calculated nor considered as a LOM planning restriction. and assignment and access should be solved in the short-term plan.

  The lack of consideration of equipment restrictions on the mine plan is also a reflection that the mine is operating in a semi-rural region of Spain, which is well supported by service providers. Extra fleet units can generally be sourced from within the region with adequate notice.

- No waste dump, or destination planning has been considered.
- No inferred material coming from the pit has been included in this plan to be as much as realistic as possible due the total contained in the final design is minimum.

8.1 Mine Production Plan

The plan is considered feasible for a LOM style plan, although adequate short-term planning will be required to successfully operate the mine.

The LOM plan targets 1.8Mt of ore per year sent to the process plant, it has been made to overcome the ore shortage during years 6 that the pit is delivering to the process plant, by including the ore stockpiles at a total of 1.2Mt of ore. The size of the stockpile increases to cover in pit ore shortage due vertical development in phase 3 which is the main ore production during this year after phase 4 is exhausted.

To avoid interferences between Phase 1 and Phase 3, Phase 4 starts in year 3 to provide ore on time. Phase 3 starts in year 4 after Phase 1 is completely developed. Hence year 3 to year 5 need to mine significant waste directly from the pit. Phase 1 ore will long last as an ore source for longer period as phase 2 needs to be developed quickly when it becomes available. The upper benches of Phase 3 are scheduled during the first year of production at a maximum rate of 15.2kt per day during the last half of the year, what will required a carefully short-term planning to sequence the operations due narrow working areas.

Figure 8-1 summarizes the production plan on a yearly basis. This also shows the ore and waste tonnage contribution by phase in each period. Mine plan detailed per year is summarised in Table 8-2 and total material to store, waste and tailings, are shown in Table 8-4 assuming dry density for the tailings of 1.8 t/m^3 and for the waste produced a swell factor of 1.25 and a 0.9 compact factor.

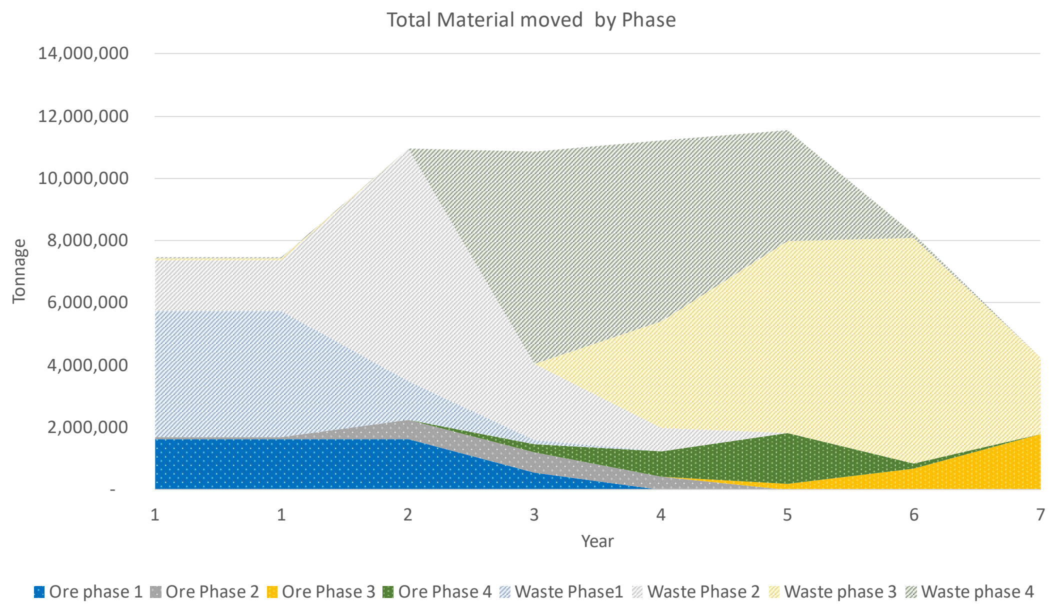


Figure 8-1 Mine Ore and Waste Production Plan per Phase

The production plan targets of 1.3Mt of ore during first year of production and targets 1.7Mt of ore sent to the crusher during the rest of the LoM, mine production by phase and per year are shown in Figure 8-2. In Figure 8-3 shows the average WO_3 mined grade and mtu contained and recovered.

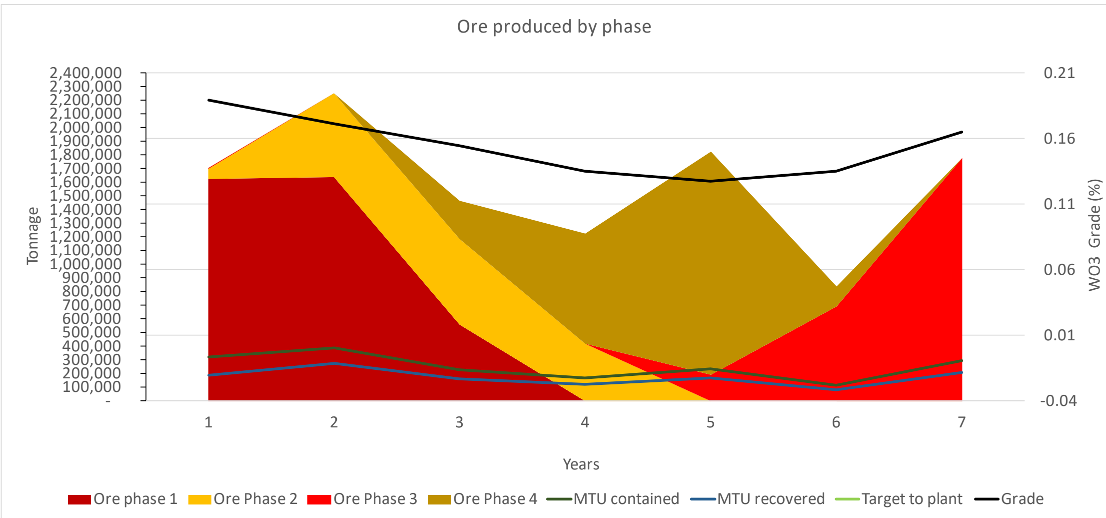


Figure 8-2 Mine Ore Production Plan per Phase

In Figure 8-2 and Figure 8-3 the waste production is summarized per year and by phase.

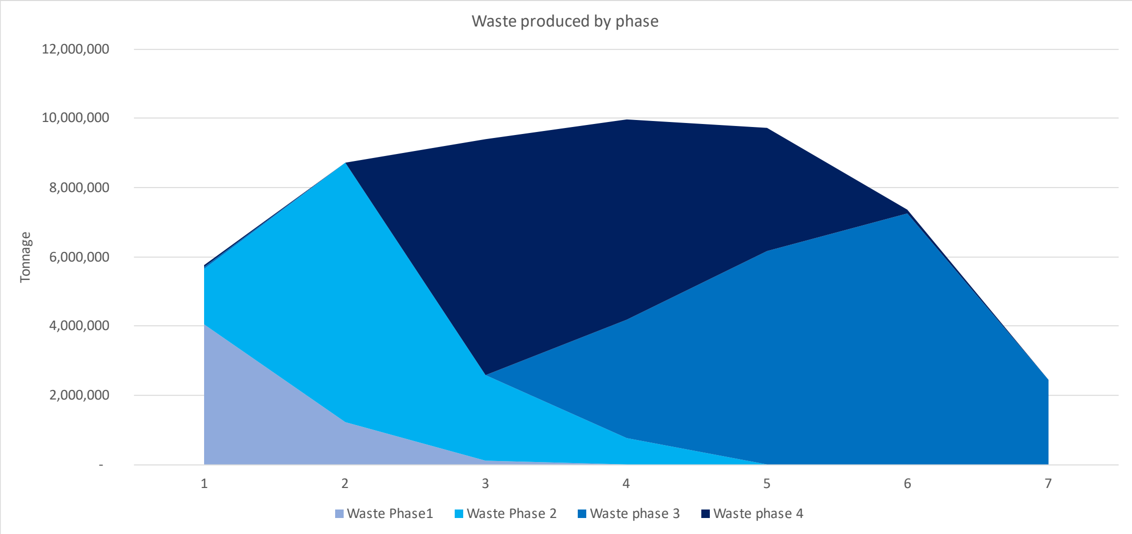


Figure 8-3 Mine Waste Production Plan per Phase

Penalties productions are included in Table 8-2.

8.2 Plant feed

This production plan has prioritized material coming from the pit for feeding the crusher. The 1,45Mt of ore process plant feed production is achieved in this production plan during the first year and continues targeting 1.8Mt during the rest of the LoM facing a shortage during year 6 that will deliver 1.2Mt of ore. This is due phase 4 is exhausted and the only provider of ore would be Phase 3 with a vertical development that becomes the bottleneck. The 107,520mtu targeted to deliver is been achieved. Higher grades are available in the first years of mining, and the stockpile grows until year 3 when becomes more active to support plant feed.

Payable Concentrate production is achieved in every period but year 6, this becomes more difficult to achieve due ore shortage and as the mine head grade drops due the pit develop progress for finalize sourcing the plant from Phase 3.

Table 8-3 shows the plant feed per year including the stockpiles contribution.

In Figure 8-4 it is shown the different contributors in this plant feed production, the average head grade and the mtu contained and expected.

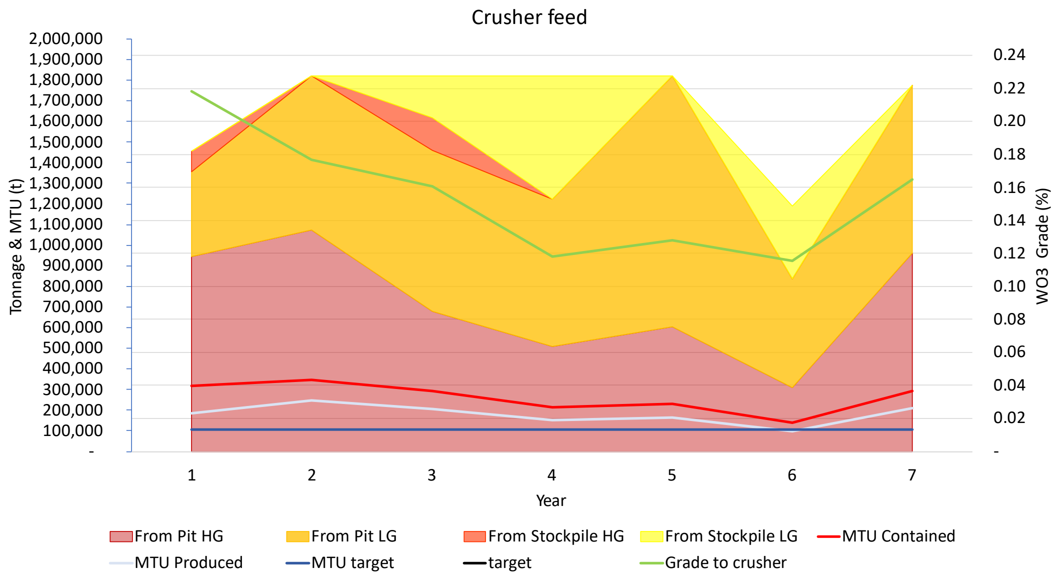


Figure 8-4 Plant feed Production Plan

8.3 Stockpile balance

During the first two years the stockpile grows to accumulate 0.97Mt of ore as Phase 1 needs to be developed before Phase 3 starts operation, so as to avoid interferences in operation. Currently stockpiles become difficult for operators manage when they approach 300kt in size is for that it will be needed a stockpile action plan for extend the stockpile size. A stockpile of 262kt of ore (approximately eight weeks feed) is desirable to prevent the process plant from being inhibited by short term production issues inside the pit.

Table 8-5 shows the stockpiles balances per year.

8.4 End of year phase position

Figure 8-5 below, after the mine plan tables, shows the end of year face position coloured by phase according the LoMP. The pit bottom level for each phase is shown on Table 8-2. As can be seen vertical advance is reasonable in the first 4 years. After year 5th it appears in Phase 4 needs to reach 60m vertical advance, equivalent to 12 benches and Phase 3 requires 60m vertical advance during years 6 and 7. This is where the pit is significantly narrower, as it approaches pit-bottom, and the tonnage per vertical metre reduces significantly.

8.5 Production tables

Below physical production has been summarized per year.

Table 8-2 Mine Plan Physical

Time	Item	Unit	1	2	3	4	5	6	7	Total
Phase 1	Waste	Tonnes	4,045,997	1,237,962	124,403	-	-	-	-	5,408,363
	Ore	Tonnes	1,626,733	1,636,222	555,182	-	-	-	-	3,818,136
	Total	Tonnes	5,672,730	2,874,184	679,585	-	-	-	-	9,226,499
	EoP Bottom	RL	570	540	525-520-515					
	Ore - S	%	0.13	0.13	0.13	-	-	-	-	0.13
	Ore- AS	%	0.05	0.06	0.08	-	-	-	-	0.06
	Ore- P	%	0.08	0.09	0.09	-	-	-	-	0.08
Phase 2	Waste	Tonnes	1,610,887	7,471,718	2,468,343	753,295	-	-	-	12,304,243
	Ore	Tonnes	71,925	614,076	628,677	417,376	-	-	-	1,732,054
	Total	Tonnes	1,682,812	8,085,793	3,097,021	1,170,671	-	-	-	14,036,297
	EoP Bottom	RL	715-710-705-700	665-660						
	Ore - S	%	0.05	0.07	0.10	0.12	-	-	-	0.09
	Ore- AS	%	0.03	0.05	0.05	0.04	-	-	-	0.05
	Ore- P	%	0.19	0.11	0.07	0.07	-	-	-	0.09
Phase 3	Waste	Tonnes	63,104	-	-	3,443,866	6,166,642	7,254,143	2,458,352	19,386,107
	Ore	Tonnes	2,040	-	-	319	192,363	689,723	1,776,173	2,660,618
	Total	Tonnes	65,144	-	-	3,444,185	6,359,005	7,943,866	4,234,525	22,046,725
	EoP Bottom	RL				650	605	545	485	
	Ore - S	%	-	-	-	0.09	0.11	0.11	0.11	0.11
	Ore- AS	%	-	-	-	0.48	0.04	0.03	0.07	0.06
	Ore- P	%	-	-	-	0.02	0.08	0.04	0.07	0.06
Phase 4	Waste	Tonnes	46,837	-	6,798,682	5,786,337	3,562,559	115,030	-	16,309,445
	Ore	Tonnes	-	-	277,128	803,621	1,628,832	145,306	-	2,854,887
	Total	Tonnes	46,837	-	7,075,810	6,589,958	5,191,391	260,336	-	19,164,332
	EoP Bottom	RL			690-685-680-675	625-620-615	555	540		
	Ore - S	%	-	-	0.09	0.09	0.12	0.10	-	0.11
	Ore- AS	%	-	-	-	0.48	0.04	0.03	0.07	0.16
	Ore- P	%	-	-	-	0.02	0.08	0.04	0.07	0.05
Total	Waste	Tonnes	5,766,825	8,709,680	9,391,429	9,983,498	9,729,201	7,369,173	2,458,352	53,408,158
	Ore	Tonnes	1,700,698	2,250,297	1,460,987	1,221,316	1,821,195	835,029	1,776,173	11,065,695
	Total	Tonnes	7,467,523	10,959,977	10,852,415	11,204,814	11,550,396	8,204,202	4,234,525	64,473,853
	Strip Ratio		3.39	3.87	6.43	8.17	5.34	8.83	1.38	4.83
	Ore - S	%	0.12	0.11	0.11	0.10	0.12	0.11	0.11	0.11
	Ore- AS	%	0.05	0.06	0.05	0.33	0.04	0.03	0.07	0.08
	Ore- P	%	0.08	0.09	0.06	0.04	0.08	0.04	0.07	0.07

Table 8-3 Plant feed Plan

Ore Feed by Source	Units	1	2	3	4	5	6	7	Total
From Pit HG	Tonnes	946,205	1,074,091	677,646	509,877	603,627	308,408	962,532	5,082,386
From Pit LG	Tonnes	409,612	744,930	783,341	711,439	1,215,377	526,621	813,641	5,204,960
From Stockpile HG	Tonnes	99,976	-	157,433	-	-	-	-	257,409
From Stockpile LG	Tonnes	-	-	200,666	597,930	-	354,374	-	1,152,970
Plant Feed - Total	**Tonnes**	**1,455,793**	**1,819,021**	**1,819,086**	**1,819,246**	**1,819,004**	**1,189,403**	**1,776,173**	**11,697,725**
Plant Feed WO_3 Grade	%	0.22	0.18	0.16	0.12	0.13	0.12	0.16	0.16
mtu Content in feed	Tonnes	317,808	347,726	292,046	215,249	232,395	137,624	292,643	1,835,490
Metallurgical Recovery	%	58	71	71	71	71	71	71	69.2
mtu Produced	Tonnes	184,329	246,885	207,352	152,826	165,000	97,713	207,777	1,261,883

Table 8-4 Total waste produced to store

Material to store	Units	1	2	3	4	5	6	7	Total
Waste	BCM	2,277,443	3,418,219	3,665,297	3,947,371	3,776,506	2,814,718	938,303	20,837,857
Tailings	Tonnes	1,455,793	1,819,021	1,819,086	1,819,246	1,819,004	1,189,403	1,776,173	11,697,725
Total to store	DCM	3,370,897	4,856,064	5,134,062	5,451,485	5,259,126	3,827,337	2,042,354	29,941,325

Table 8-5 Stockpile Balance

StockPile	Status	Unit	1	2	3	4	5	6	7	Total/Max
Low Grade	Opening	Tonnes	180,379	384,127	815,403	614,737	352,182	354,374	180,379	815,403
		WO_3 Grade	0.10	0.09	0.09	0.09	0.07	0.07	0.10	0.09
	In	Tonnes	344,881	431,276	-	-	2,192	-	344,881	778,349
		WO_3 Grade	0.15	0.09	-	-	0.09	-	0.15	0.11
	Out	Tonnes	-	-	200,666	597,930	-	354,374	-	1,152,970
		WO_3 Grade	-	-	0.03	0.02	-	0.07	-	0.14
	Closing	Tonnes	384,127	815,403	614,737	352,182	354,374	-	384,127	815,403
		WO_3 Grade	0.09	0.09	0.09	0.07	0.07	-	0.09	0.08
High Grade	Opening	Tonnes	122,294	157,433	157,433	-	-	-	122,294	157,433
		WO_3 Grade	0.27	0.31	0.31	-	-	-	0.27	0.30
	In	Tonnes	-	-	-	-	-	-	-	-
		WO_3 Grade	-	-	-	-	-	-	-	-
	Out	Tonnes	99,976	-	157,433	-	-	-	99,976	257,409
		WO_3 Grade	0.08	-	0.19	-	-	-	0.08	0.14
	Closing	Tonnes	157,433	157,433	-	-	-	-	157,433	157,433
		WO_3 Grade	0.31	0.31	-	-	-	-	0.31	0.31
Total	Opening	Tonnes	302,673	541,561	972,837	614,737	352,182	354,374	302,673	972,837
		WO_3 Grade	0.17	0.15	0.12	0.09	0.07	0.07	0.17	0.11
	In	Tonnes	344,881	431,276	-	-	2,192	-	344,881	778,349
		WO_3 Grade	0.15	0.09	-	-	0.09	-	0.15	0.11
	Out	Tonnes	99,976	-	358,099	597,930	-	354,374	99,976	1,410,379
		WO_3 Grade	0.08	-	0.10	0.02	-	-	0.08	0.14
	Closing	Tonnes	541,561	972,837	614,737	352,182	354,374	-	541,561	972,837
		WO_3 Grade	0.15	0.12	0.09	0.07	0.07	-	0.15	0.11

The Figure 8-5shows the evolution of the pit at the end of each year in the LoM. The colours indicate the phase at which the mining blocks correspond.

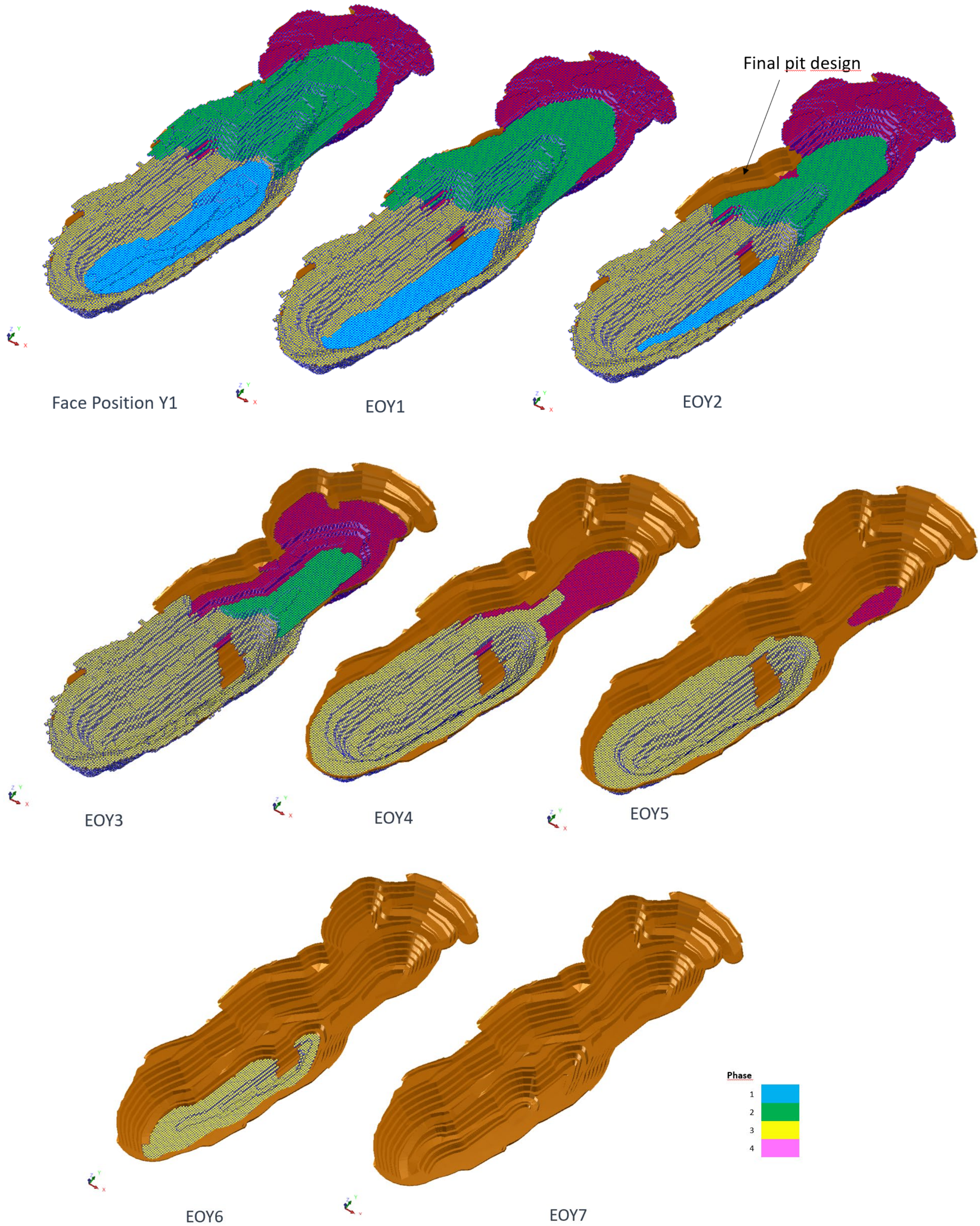


Figure 8-5 End of year phase position

9 Waste Storage Facility

Saloro waste storage facility is located 100m from the existing western pit boundary. The design considers that storage needs to allow for both the filtered tailings produced in the processing plant which are co-disposed with the waste coming from the pit. Both types of materials to be placed in the waste dump as Non-Acid Forming (NAF).

The latest version of the waste dump permit was submitted in February 2021 and was approved in November 2021. This application and permit follow the Spanish RD 975/2009 legislation applicable for this type of facility. The design criteria considers both technical and environmental elements. The footprint of the waste storage facility covers area of previous mine activities and prioritizes the use of lower ecological value areas for reducing the environmental impact.

This is close to the open pit operation however it does not compromise the final pit design, as used in this ORE. Nevertheless, the current approved design for waste storage, cannot contain all of the waste requiring to be stored by the mine plan considered for this ORE. This is why a new waste storage design must be submitted for approval to the regulators.

The exiting waste dump is partially filled with material mined since 2019 and is at approximately 75% of approved capacity already. Figure 9-1 shows the final design of the current waste dump.

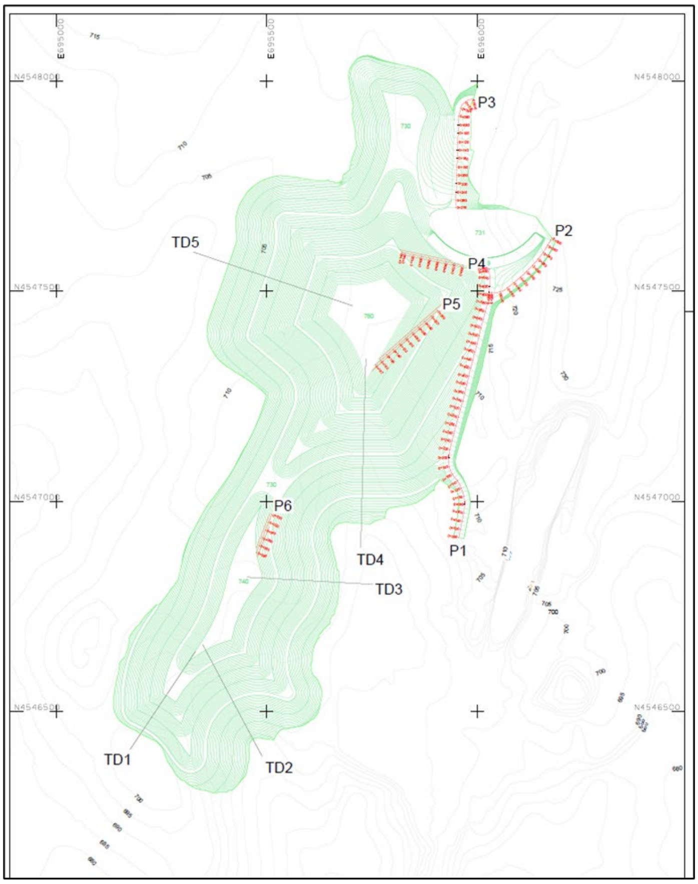


Figure 9-1 Actual Waste Dump Project

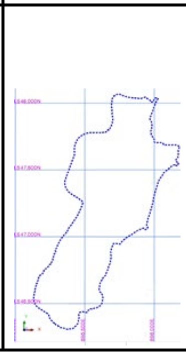
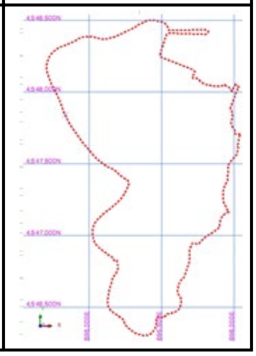
Three different access connects the waste storage facility with operations, as shown in Figure 9-1 by the red hashed tracks. above. Access P1 connects the pit exits from phases 1, 2 and 3. P2 services phase 4 and gives access from the stockpile area.

The waste material generated in the project from the it and the majority of the plant is characterized as inert, thus Non-Potentially Acid Forming. The waste produced in the back end of the processing plant, after the flotation and magnetic separation, is classified as non-inert. This represents a minor fraction of the total waste produced and is managed by using an external agent to transport this non-inert material to an external authorised facility.

Within the existing design approved for the waste dump, the surface water is collected and connected with several water ponds and the underground water is controlled by series of internal drains which collects and send water to the water process plant.

The waste storage design has undergone several modifications over the project life as set out in Table 9-1.

Table 9-1 Waste Storage Desing Summary

		Original Waste dump	**Waste dump (2021)**	**Waste dump to be presented 2024**
Volume (Reports)	*m3*	20.68	19.3	Not presented-
Volume* (Topography 9-2alculate.)	*m3*	Not available	25.2*	68.8*
Area (as per Projects)	*Ha*	76.4	80.3	164.2
Maximum elevation	*masl*	782	775	790
Footprint	-			

* Indicates where the volumes have been recalculated with the same topography (*inter_topo 1_topo2*) to have better support the actual volumes, due to differences with calculations based on topographies used in the historical reports.

Initially, the waste dump design (green in figure) was planned to be located to the west of the pit, extending to the north and west and allocating a capacity of 20.68 Mm3 of waste (Volume reported in the Exploitation Project). The reported surface in the projects for its approval was 76.4Ha. In 2021, a new waste dump project was submitted to the Mines and Environment Administration, which avoided the expansion to the north, compensating this with an extension to the south, with a global increase of the affected surface but lower waste dump height. This new project design, Figure 9-2, is the one currently approved and has a capacity of 25 Mm^3 as per topographic calculation.

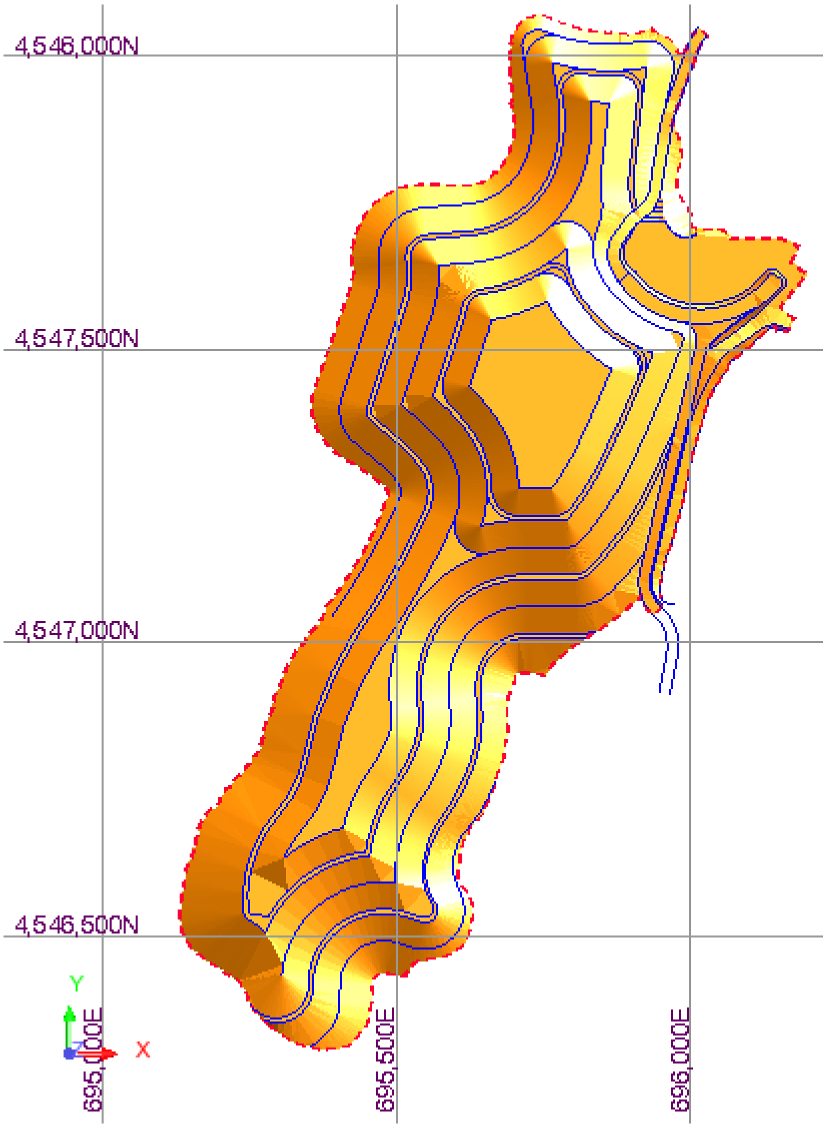


Figure 9-2 Waste dump design 2021 (Currently approved)

For the current waste dump design approved in 2021, the material already backfilled is 19.3 Mm^3, leaving a remaining 5.9 Mm^3 as represented in the figures and table below, where the strings show the final design, and the solid area indicates the current situation of the waste dump as per the end of May 2024.

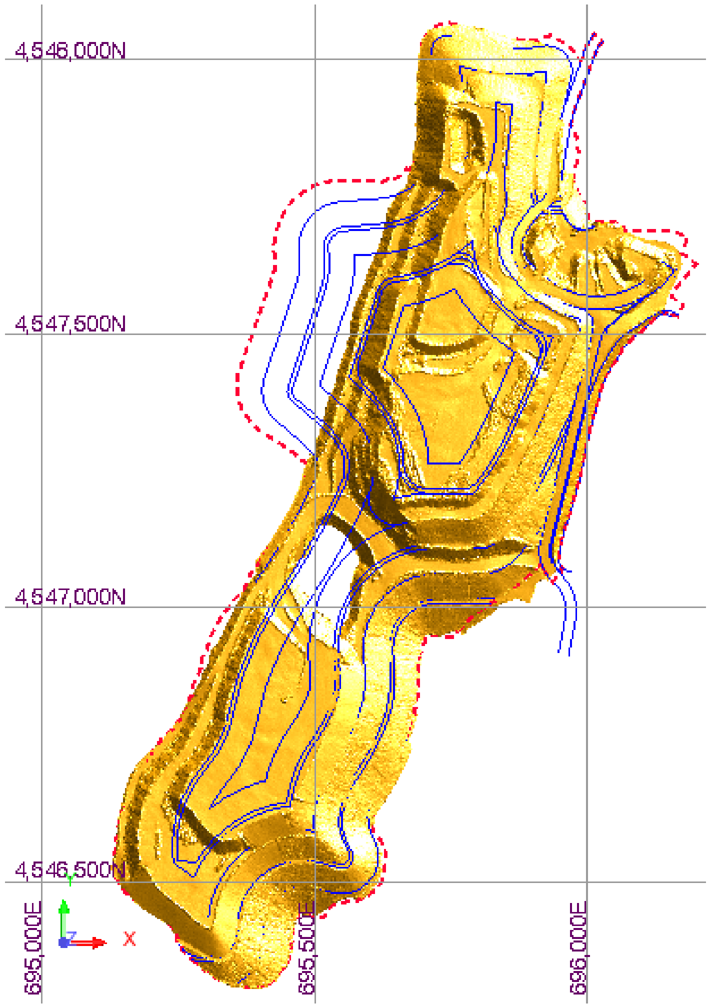


Figure 9-3 Waste dump situation in May 2024

A waste dump section is shown in the following figure, showing in purple the available space to the final design.

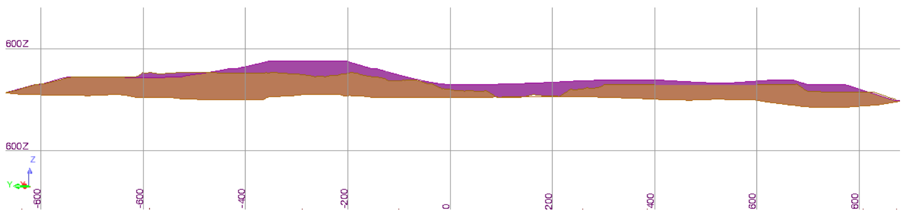


Figure 9-4 Section of waste dump situation in May 2024

Table 9-2 Remaining volume of the waste dump approved

Waste dump design (2021)	Volumen (Mm3)
Total capacity	25.2
Stocked material (May 2024)	19.3
Remaining volume to fill	5.9
* Calculated by Topo	

With the 2024 reserve estimate, the volume of material to be managed for the remaining LOM is 29.9Mm^3, being 6.5Mm^3 for tailings and 23.4Mm^3 of swollen and compacted tailings that it is expected to be completely filled by the beginning of October 2025.

In parallel to the development of the reserve estimation, a LOM waste storage design has been developed to define the maximum required footprint and volume capacity. This considers possible environmental conditions, design restrictions and basis, and oversizing the facility so as to be able to accommodate extra material that could be required by a future increase in the reserves. This new waste dump design is expected to be submitted to the regulators for permitting in 2024. This administrative process is expected to take up to two years from the date of submission.

The design criteria of the waste storage facility is shown in Table 9-3.

Table 9-3 Waste Storage Facility Design Criteria

Waste Dump design criteria	
Slope angle	33 degrees
Berm width	8m
Bench height	10-30m
Final slope angle after reclamation	18/20 degrees
Swelled density	2.3t/m3
Swell factor	25%
Ramp width	25m
Ramp gradient between	7/10%
Averall slope angle	16 degrees
Heigh above ground	90m
Total volume capacity	69.4Mm^3

The aim is to submit the largest possible volume for the waste storage to accommodate as much material as possible. This approach is intended to avoid another new submission for another new design in the future, even if the 2024 proposed volume is not fully utilised by project end. The design, shown in red shading in Figure 9-5, will serve as a reference for material management in the new waste storage facility design.

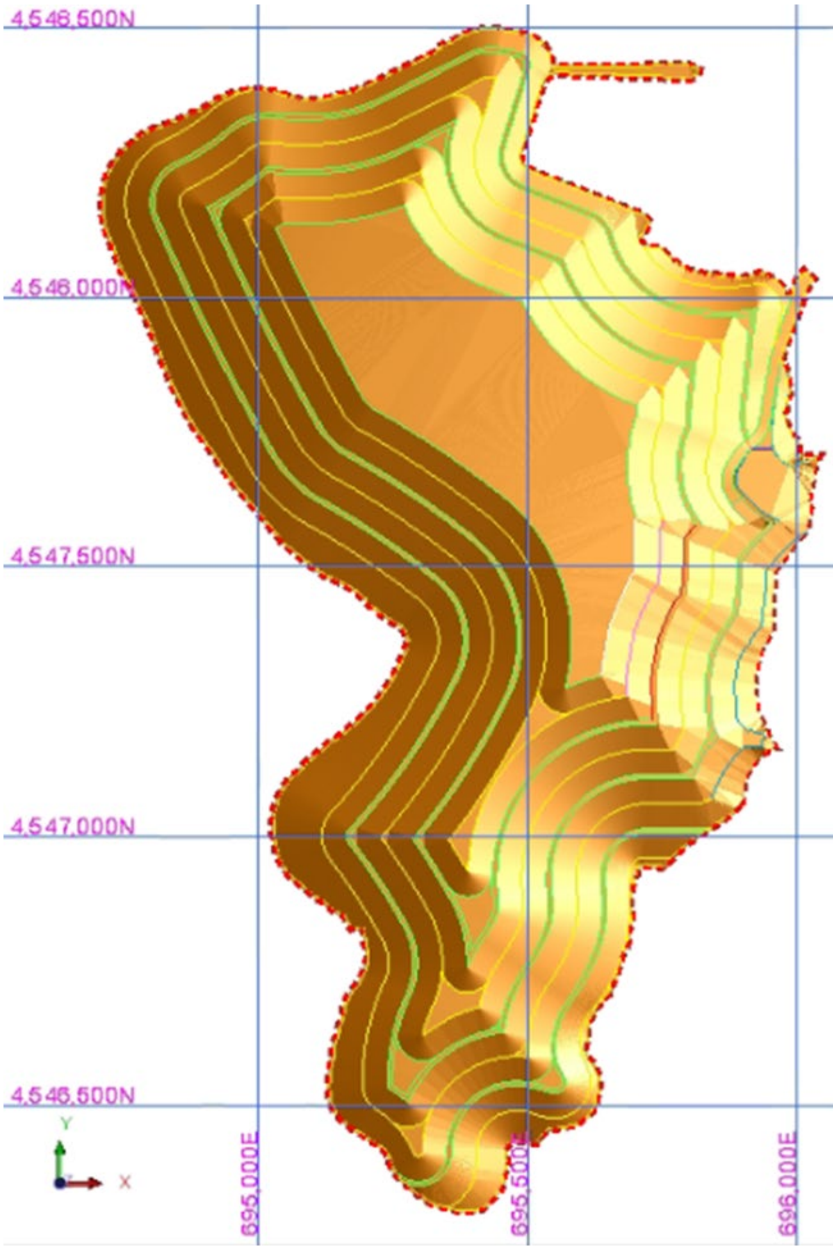


Figure 9-5 Final Waste Dump

The mass balance considering this final waste dump is shown in Table 9-4.

Table 9-4 Waste dump mass balance for Reserve Estimation 2024

** Calculated by Topo_Origen*	Volume	% Total Waste	Aver Density	Tonnes
Taillings	6,315,620	21%	1.8	11,368,115
Waste	23,442,589	79%		53,408,165
Total swelled and compacted volume	**29,758,208**			
Total Waste Dump capacity (Design 2024)	68,800,000			
Stocked material at the waste dump (May 2024)	19,303,219			
Remaining volume to fill (Design 2024)	49,496,781			
Total waste to be stocked on the Waste dump	**48,551,733**			
% Occupation of waste dump (Design 2024)	71%			
Waste dump design (2021)	**Volumen (Mm3)**			
Total capacity	25.2			

Figure 9-6 shows the footprint of each design, being the 2024 design the largest, represented in red, the currently approved in blue, and the original project permit in green.

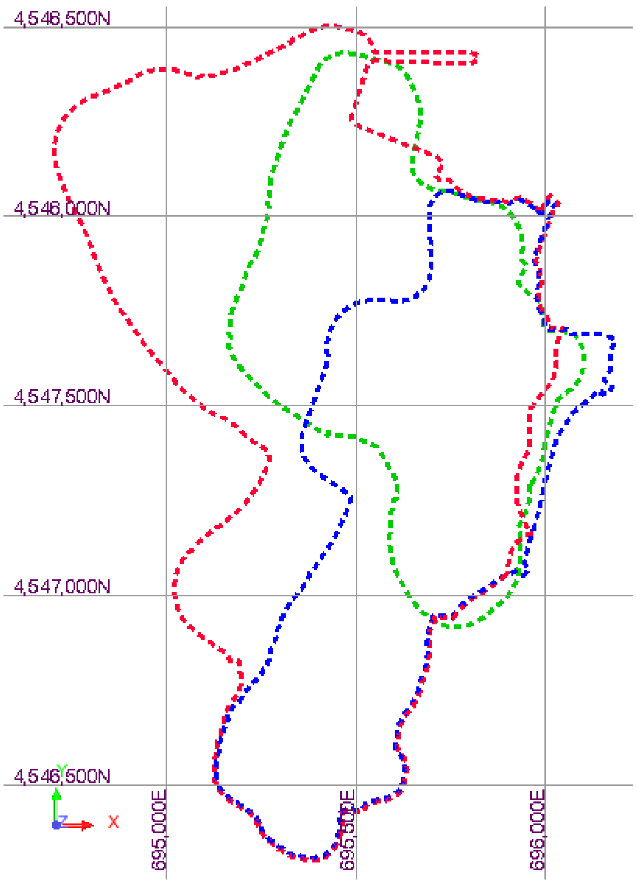


Figure 9-6 Waste dumps footprint comparison

The proposed expanded footprint fits inside the concession limits without risking operations as shown in Figure 9-7.

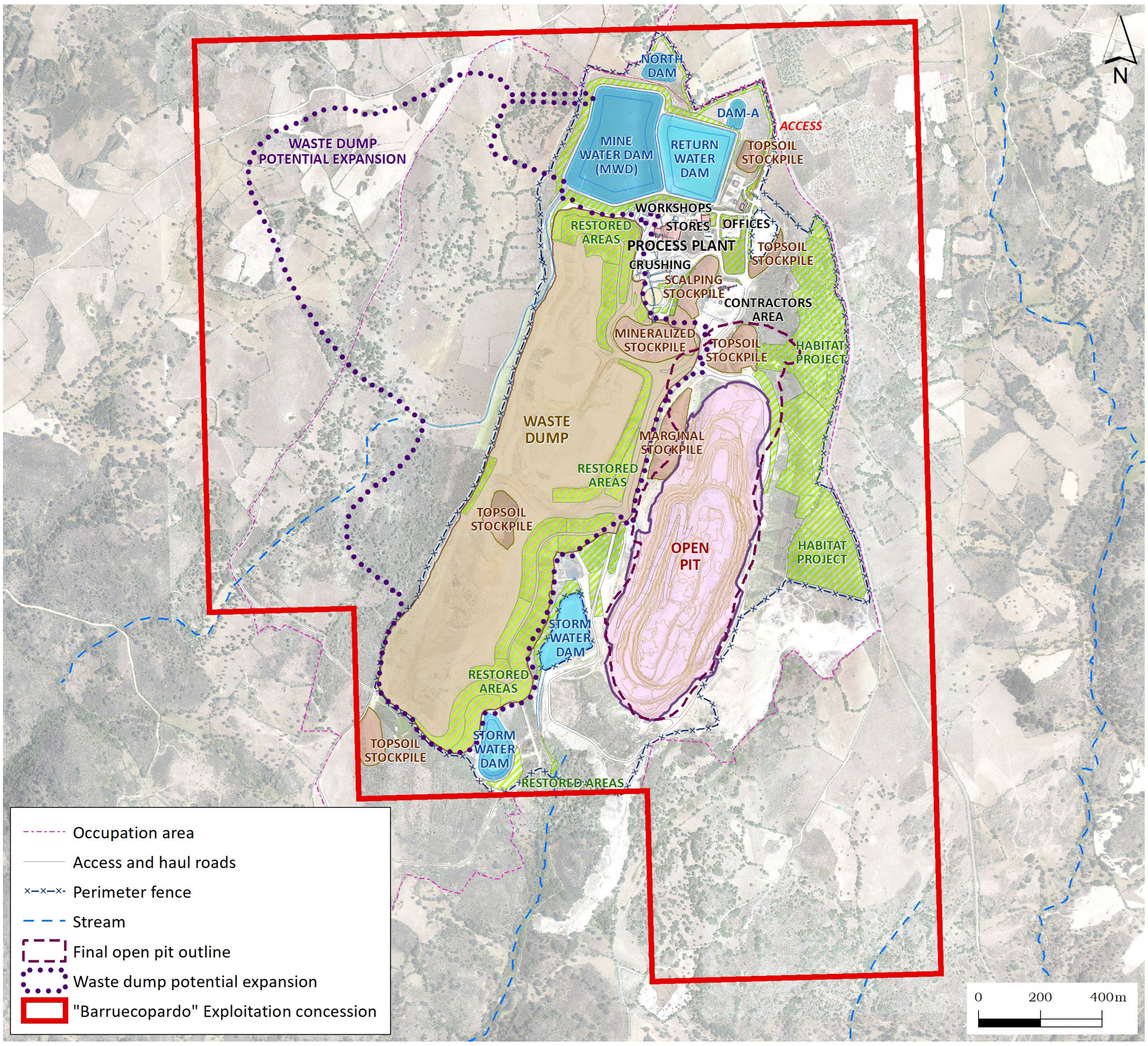


Figure 9-7 Potential extension WD Lay-out

The extension of the waste storage facility is needed before end of 2025, in order to be able to accommodate the waste produced as per the mine plan considered in this ORE report. If the extension is not granted in time, Saloro has other potential contingency plans to using currently authorised areas for mining activities as temporary waste storage sites until the expanded, permanent facility is fully permitted. This would imply an extra cost for rehandling the material placed in temporary waste facilities, to final destination if required.

10 Update for 2024 Mining

Mine production has been on-going 1st of January 2024 until 31st of August 2024. The base MRE model being dated 31 December 2023, therefore models and stockpile estimates have been depleted for the interim activity in 2024, so as to correctly estimate the correct Ore Reserve remaining as of 31 August 2024.

The phase position has been updated with the surface EXC_Agosto2024_TOTAL_3D.dtm , corresponds to the August end of month topographic survey as shown in the Figure 10-1

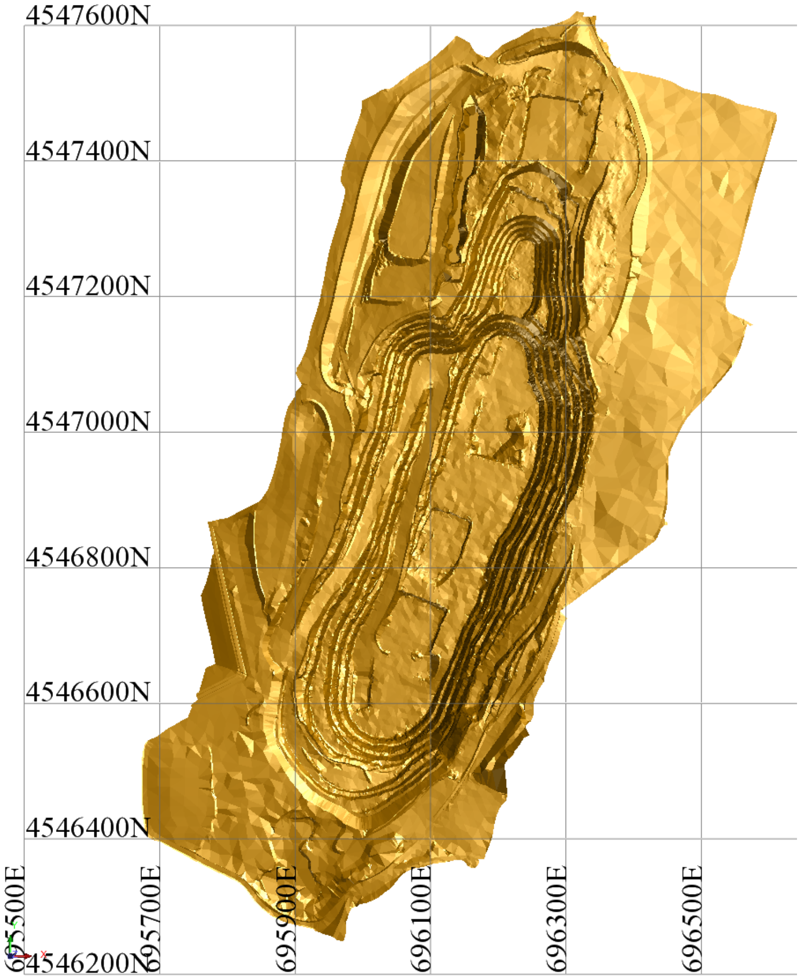


Figure 10-1 End of month surface, August 2024

During this eight month of operations a total of 4.4Mt of material has been excavated according to the reserves block model (*saloro_202310_res_rot_6x6x5.mdl*) to produce 503kt of high-grade ore and 414kt of low-grade ore. A total of 0.9Mt of ore at an average grade of 0.18% that contains 162,752 mtu. The material moved during this period is summarized in In Table 10-1.

The mine is slightly initiating the ramp-up to achieve the 1.45Mt of ore during 2024. As can be seen the mine is slightly down on the annual physical plan on a year-to-date basis by the end of May. However, this under achievement of plan is not considered material in terms of the LOM plan supporting this ORE. The monthly targets for the remainder of 2024 (corresponding to the months from the month 9 to the month 12 of the year 1 of the LOM Plan) have been slightly increased to regain this deficient, such that the end of year position is achieved.

Table 10-1 Actuals Jan-Aug 2024

	Actuals			
	Ore (t)	**Grade (%WO_3)**	**mtu (t)**	**Waste (t)**
Jan 24	56,757	0.22	12,314	421,337
Feb 24	74,948	0.15	11,444	428,847
Mar 24	101,969	0.18	18,367	521,937
Apr 24	121,318	0.17	20,312	378,214
May 24	151,419	0.20	29,833	326,319
Jun 24	100,440	0.14	14,352	427,762
Jul 24	172,284	0.17	29,250	571,906
Aug 24	137,631	0.20	26,880	439,567
Total	**916,766**	**0.18**	**162,752**	**3,515,889**

Together with the pit actuals, the stockpile status has been updated at the end of August 2024, as shown in Table 10-2.

Table 10-2 Stockpile update EOM August 24

Stockpile status	Tonnage EOM May 2024	Grade	Concentrate	Concentrate grade	mtu
A	144,883	0.194			28,058
B	157,290	0.102			16,009
OP					
MAR (not included)	337,399	0.064			21,593.54
scalping (concentrate included)	139,450		12,550	0.058	20,076
To plan/reserves					
HG (A stockpile + scalping)	157,433	0.183			48,134
LG (B stockpile + OP stockpile)	157,290	0.102			16,009
	335,375	0.061			20,572
Total	**650,098**	**0.10**			**84,715**

In next figure it is shown the stockpile inventory with the different stockpile disposition.

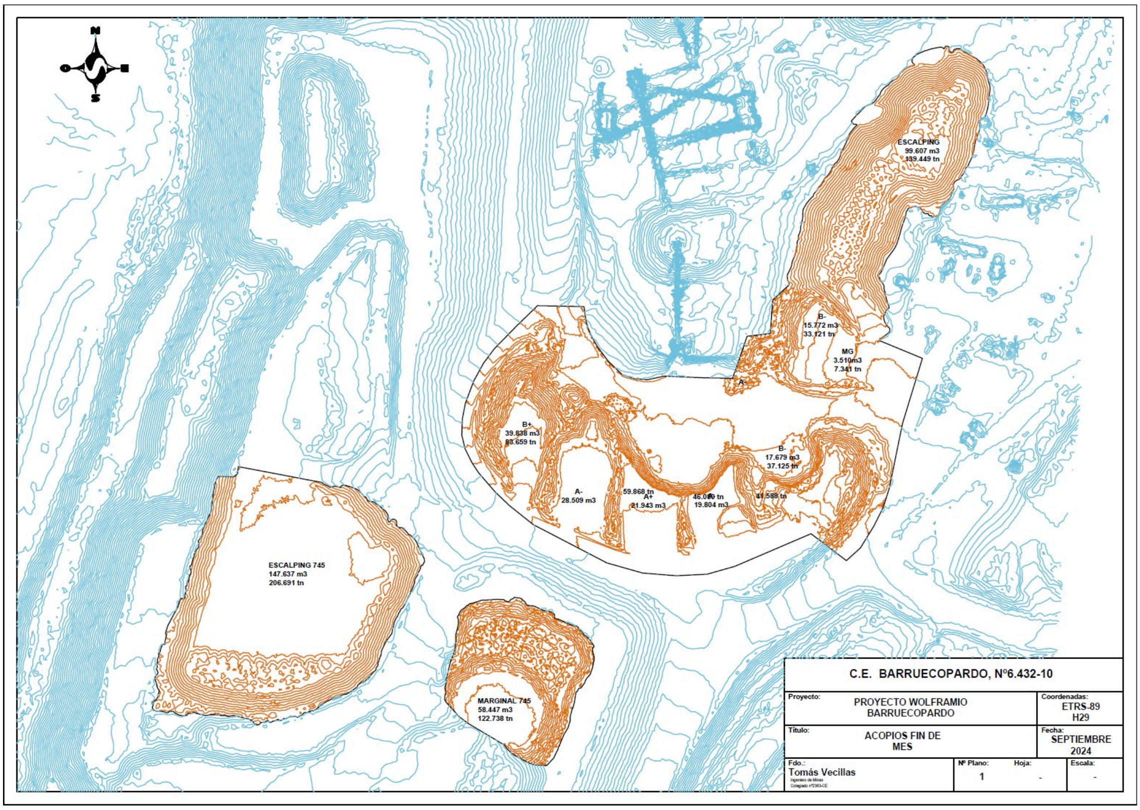


Figure 10-2 Stockpile location and inventory August 2024

11 Mineral processing

The mineral processing at Barruecopardo follows a typical comminution and gravimetric block flow diagram with a later refinement of the gravimetric concentrates by removing the sulphides using flotation and a further magnetic separation to remove paramagnetic elements (such as U and Th).

The plant was constructed from 2017 to 2019 and the initial design was done by Jacobs although it has not been possible to review the original plant design. This chapter describes the existing plant, its' performance and the implementation of the plans to increase the recovery of the plant.

This chapter has effectively contributed by Saloro. MiningSense has edited that so as it conforms to this report, added some figures and graphs to assist understanding and explanation. Therefore, MinignSense has not independently verified this contribution.

11.1 Metallurgical testwork

The 2012 Exploitation Project (EP) for the Mining License Application (MLA), list four stages of metallurgical tests that had been carried out on samples collected from the Barruecopardo mineralization:

- June 2007, SGS Lakefield.
- May-July 2008, Wardell Armstrong International (WAI).
- September 2008 - May 2009, Wardell Armstrong International (WAI).
- October 2011, Wardell Armstrong International (WAI).

The tests were performed on samples of over 0.75 tonnes with a grade similar to that expected to be treated in the designed process plant According to the EP submission these test results were the basis for the correct design of the process plant that was completed by Jacobs.

The testwork to develop the plant design was done during the Feasibility Study stage of the project, however there are no references to these testwork in the FS documents. MiningSense has not seen the evidence of this testwork.

The following equations show the recoveries as estimated in the FS, and are supposedly based on the testwork done:

$$IF\ (WO_3\ (Head\ grade) > 0.42\%,\ Met.\ Recovery = 80.5\%,$$

$$Else\ Met.\ Recovery = 10141719.75 * (WO_3(Head\ grade))^3 - 116721.57 * (WO_3(Head\ grade))^2 +$$

$$454.47 * WO_3(Head\ grade) + 0.2(Fixed\ Tail))$$

The recoveries expected in the DFS were substantially different from those achieved during the production phase. Planned/ design recoveries of ~80% compared to actual recovery of ~45%.

Thereby indicating the room for improvement that exists in the processing plant. The reasons for the below design performance are not a subject for this ORE report.

For the purposes of this ORE report metallurgical information will be based on existing operations, and the improvement plans developed by the current Saloro team assisted by specialised consultants.

11.2 Flowsheet

The existing plant has the block flow diagram shown in Figure 11-1.

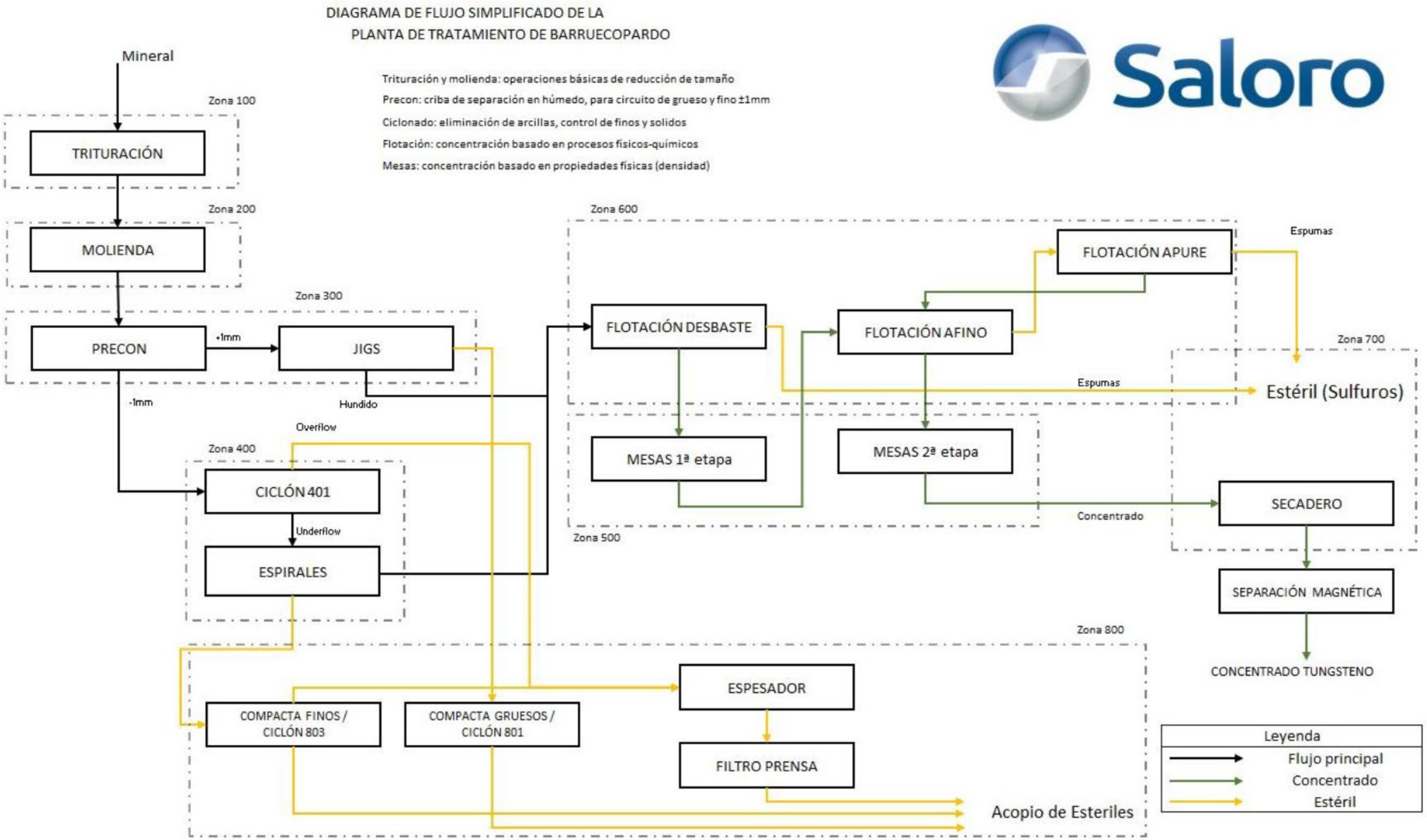


Figure 11-1 Flow diagram for Barruecopardo plant

11.3 Existing process description

The ore mined is stockpiled on the RoM pad, according to its WO_3 and arsenic grades. The appropriate portion of each stock feeds the primary crusher to obtain a blended ore feed to achieve an average grade of 0.17-0.20% WO_3.

The material fed passes through a primary jaw crusher. The ore is reduced from 800 mm to 110 mm. After crushing, the ore passes to secondary cone crushers to achieve the 5 mm that is supposed to be the liberation size.

Once the ore passes once through the secondary and tertiary crushing, material in the range of 8/20mm is rejected. Some tests are being currently done to review those limits to 8/40mm by adjusting the setting of the cone crushers. The reason is because the ore is liberated quickly, and the bigger size material typically corresponds to the granite minerals of quartz and feldspars. This stage is called as Scalping.

The material rejected from the mainstream, some 27%, is then fed to a X-Ray process to recover part of the ore that could be lost within the scalping stage. The ore recovered in the ore sorting is sent to the quaternary crushing, together with the material passing the scalping screen, then all the recombined material enters in the gravimetric plant.

The combined ore: the material non-rejected during scalping as well as the recovered in the ore sorting, then enters in the gravimetric concentration plant at a rate of 120 t/h, where is differentiated by screening to generate two circuits, fine and coarse. The water is added at the beginning of the gravimetric stages.

The coarse circuit (screen reject, +1mm) is fed at a rate of approximately 72 t/h and consists of two stages of concentrate using differential acceleration equipment, jigs, hydraulic pulse equipment dedicated to the concentration of high-density minerals, generating tailings composed of low-density minerals. The concentrate from the second jig stage continues to a rod mill to match the particle size of the fines/spiral circuit.

In parallel the fines circuit, which consists of the slurry (-1 mm) from the main screen, which receives a feed of approximately 40 t/h, passes through a battery of cyclones to eliminate clays. The screenings from the main screen are fed to a triple staged spirals. The spirals, like the jigs, concentrate the high-density minerals, obtaining a concentrate with a high sulphide and scheelite content, and eliminating the lower density minerals through the tailings.

After the previous stages the material passes through the first roughing flotation where the concentrates from both circuits are combined to eliminate sulphides from this high concentrated sulphide and scheelite pre-concentrate. Approximately 2.7% of the material fed to the plant, i.e. 4 t/h, feeds this flotation stage.

In the flotation stage, the sulphide minerals, arsenopyrite and pyrite, are concentrated in the froth and separated from the rest of the heavy materials. sulphides concentrate is treated as AF waste and delivered by an authorised company to an external controlled deposit, as described in the preceding chapter on waste storage.

The sink material from the flotation cells goes to a first stage of Wilfley tables. This is then fed through a hydro-classifier to make a two-stage separation, fines/coarse.

The last stage of the wet process is the refining flotation, where, as in the roughing stage, the aim is to remove the sulphide minerals that were not concentrated in the roughing flotation. It is a batch process where the particle size is controlled in order to achieve good reaction kinetics and flotation of all particle sizes. The concentrate sulphides stream then joins the previous sulphides stream.

The sink material from the second flotation stage passes through a second stage of shaking tables where it is controlled the final concentration of scheelite in the final product.

Finally, the concentrate is dried and passes through a cascade magnetic separator with induced rollers to remove magnetic and paramagnetic materials. This process removes the possible U in the ore and increases slightly the concentrate grade by removing other deleterious paramagnetic and magnetic minerals.

The crushing circuit currently processes an average of 1.4 MTPA (Million Tons Per Annum). However, based on design parameters, the circuit is capable of handling up to 275 tph without the sorters. The reality is that the plant capacity nowadays is 120tpa in the gravimetric area, which is the bottleneck of the process plant. To de-bottleneck the plant, the scalping and ore sorting processes were introduced in the plant, which also enables a reduction in the head grade and increase the potential ore to be processed.

11.3.1 Improvement plan

By incorporating the original recirculating load, the circuit's throughput can increase to as much as 525 tph. Presently, the XRT sorters process material in the -40+8 mm range at rates of up to 120 tph, which is 40 tph higher than the previous configuration that handled material in the -20+8 mm range. The throughput of the XRT sorters is largely determined by the top size of the feed material.

The supplier of the XRT sorters has experience with sorting material up to 85 mm, which presents an opportunity for Saloro to optimize the crushing process. By sorting larger material, Saloro could reduce the amount of material sent to the wet plant, increase metal content, lower wear on equipment, and improve overall recovery. To further increase the material reporting to the sorters, a new screening cut at 6 mm is proposed, involving the introduction of a wet screen.

The key opportunities for this optimization are listed below. As a result, considering 365 days a year, 24h per day, applying 75% availability (6,570 operating hours) and 275tph processed the total plant throughput will reach 1,806,750 tonnes per year.

11.3.1.1 Improvement 1: Decrease Feed to the Wet Plant

By pre-sorting non-metal bearing material, Saloro can reduce the load on the wet plant, enhancing processing efficiency.

11.3.1.2 Improvement 2: Increase Metal Content

Increase Metal Content: Reducing the amount of impurity (non-metal material) will lead to a higher concentration of metal in the feed.

11.3.1.3 Improvement3: Decrease equipment wear

Reducing the amount of recirculating material in both the dry and wet plants will minimize wear and tear on the equipment.

11.3.1.4 Improvement4: Improve recovery

By reducing fines generation and maximizing the use of existing wet plant equipment, Saloro can improve recovery rates.

11.3.2 Implementation program and expected outcomes

The feed reporting to the first screen will be screened in two size fractions: 80 mm and 30 mm. Further modifications will be made to the secondary screening stage, replacing the panels on the second deck with 6 mm panels. Introducing the existing wet screen from the stock yard and implementing a new XRT sorter.

- +80 mm fraction will report to the primary cone crusher.
- -80+30 mm fraction will be processed by the coarse XRT sorter. A maximum of 10% of this material will be accepted as pre-concentrate, which will then be crushed to 6 mm.
- -30+6 mm fraction will continue to be processed by the existing two sorters, with up to 10% being accepted as pre-concentrate. The sorter feed will first be dry screened at 6 mm, and a wet screen will be installed to enhance the cleanliness of the feed material.

Based on historical plant data, equipment specifications, and tests conducted so far, it is estimated that the system can run at a capacity of 1.8 MTPA, with an average feed grade of 0.16% WO_3. The pre-concentrate is expected to yield 85 tph at a grade of 0.51% WO_3, representing a 30% improvement in MTUs compared to the current plant feed.

This optimized approach will enhance efficiency across the circuit, improving throughput, metal recovery, and equipment longevity.

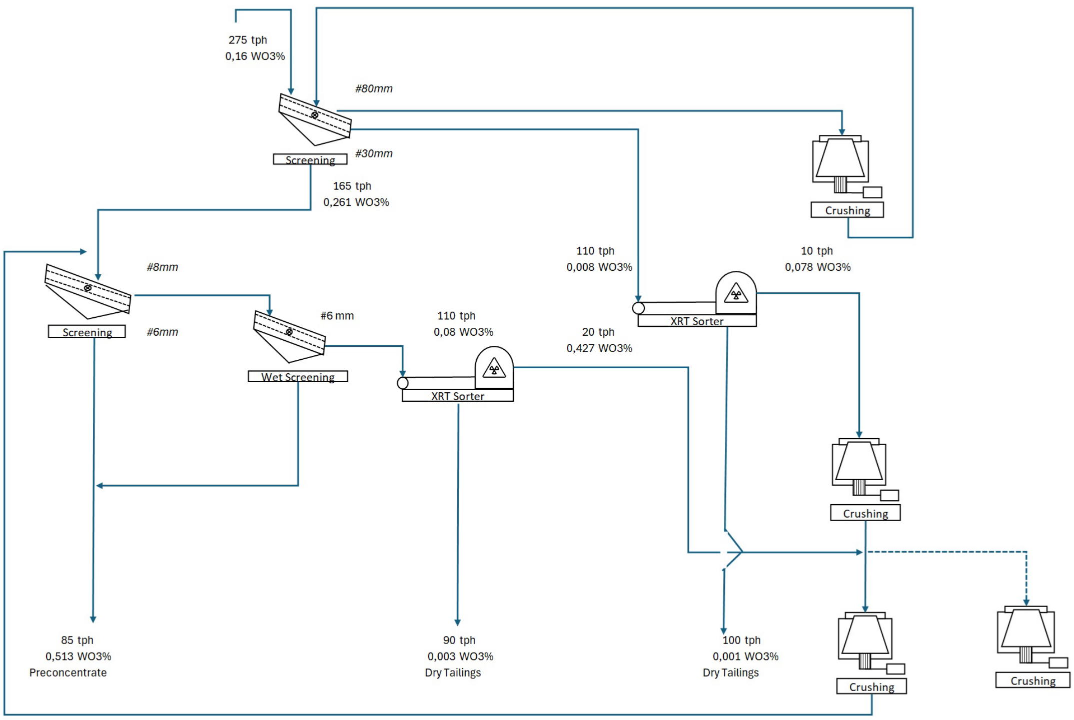


Figure 11-2 Circuit Flowsheet : August 2024

11.4 Metallurgical performance

11.4.1 Historic recoveries

The metallurgical performance over the last two years, until November 2023 is shown in Figure 11-3. Prior years data is not reliably available.

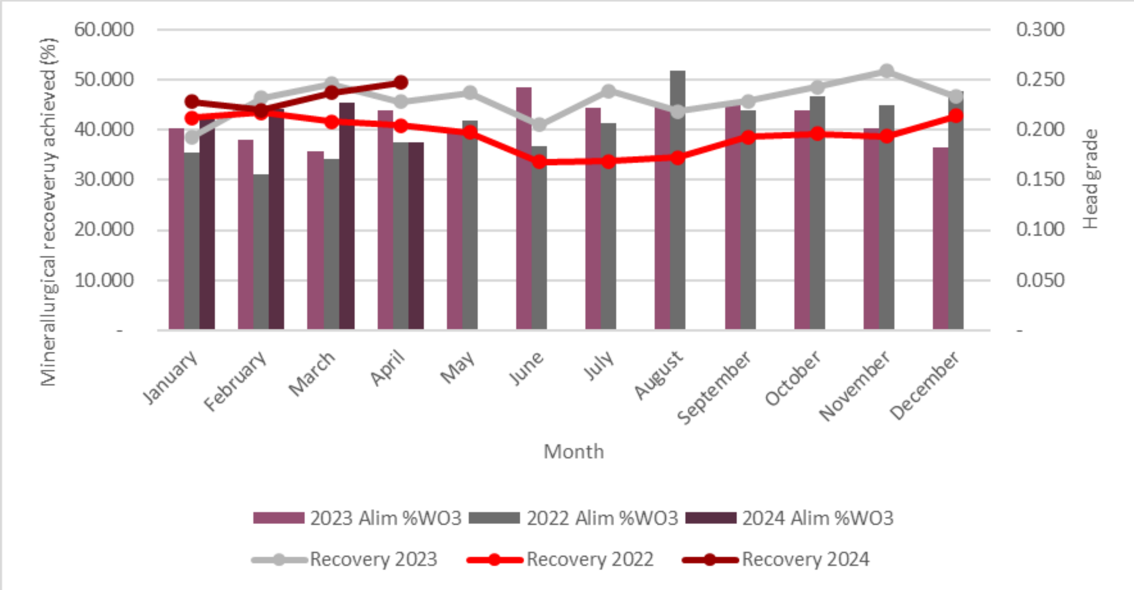


Figure 11-3 Plant Recoveries: 2022-2023

The average recovery in 2023 was 7% higher than in 2022, with just simple operational changes. The improvement plan, as described below was conceived and planned in the second half of 2023, for implementation from 2024 onwards. The initial results are encouraging.

11.4.2 Improvement plan

The improvement plan to increase metallurgical recovery and process plant throughput has been defined by Saloro, under the direction of the Plant Manager Mr Pedro Jiménez, and their specialist consultants, who also provided the recovery figures expected from the program. In this section MiningSense summarises the improvement activities that Saloro is putting in place.

These are listed in the order in which they are planned to be implemented.

11.4.2.1 Improvement 1: Alumina specific gravity control in the jigs

The change aims to recover the mixed coarse ore particles that Saloro are currently losing in the jigs section. The change consists of including a layer of alumina in the jigs with a close control on its thickness. This should then create a surface that better controls the differential density between the heavy and light minerals, and so to better separate them.

A photogrammetric analysis was carried out that identified that particles, although of large size, had a low density. Therefore they would be difficult to recover with a bed in the jig of 3.2 S.G. At the beginning of the project the manufacturer identified 2.6 S.G. alumina as the best media to line the bed. The historical maintenance on this alumina layer has not been good. It was also reported by the operators to be not used or not properly used. The aim is to recover and maintain the alumina layer in good condition so as to improve its performance.

To maintain the jigs and the alumina layer in good condition, and thereby obtain 100% performance, it will be also required to correct the operation of the hydraulic system, the start-up distributor and the clean water maintenance in the jig chamber.

This action was put in place in January 2024 with the expected outcomes after implementation

Based on the initial results it is considered a positive change that will produce measurable impact in the recovery. The challenge will be the on-going maintenance of both the alumina layer and the jigs operation.

11.4.2.2 Improvement 2: Change in cyclones

Tests have been carried out by Advanced Mineral Processing SL (AMP) for the optimization of the cyclones. The analysis concluded that to recover a greater quantity of ore in the cyclones, a double cyclone stage is needed. The second stage would receive the overflow of the first stage, recovering the 38µm fraction where the particle limit is located for a high yield in the spirals.

There are several options that can be executed in different steps in this area to minimize the investment.

A testwork report (CY401 report) developed by AMP has been provided showing the evidence of the expected results.

It is also noted by Saloro that increasing the recovery of fines in the current configuration of the circuit would result in a reduction in the performance of the spirals due to the results obtained in the plant. Although the yields in the plant tests vary, they all reflect the same: in a wide range of particle size from the lower fractions to <106µm, the performance of the spirals with material ranging from 0 to 1mm feed drops drastically. For this reason, this improvement must be done as a complete redistribution of the spirals system, as continuing with the current situation would result in rejection of fine ore in the spirals instead of in the cyclones.

Consistently increasing the efficiency of these cyclones will also require greater control of the feed conditions. For this Saloro is currently working with both the electrical department and the plant work program company (PROCISA), to put in place on-line automatic controls for density, flow and working pressure of the cyclones.

This improvement is due to be finished in June 2024 so the effects will be seen then. Due to the good reputation of AMP for gravity plants in Spain this is considered a credible improvement measure that should produce the expected increase in the recovery of the fines, thereby improving the overall process plant recovery.

11.4.2.3 Improvement 3: Flexible screens

With the decision to change from rigid to flexible screens, the aim is to eliminate the blinding of the current screens, where once they are clogged, the fine mineral can not pass to the appropriate circuit. Saloro has been monitoring how the "Precon" is behaving. The improvements have been mainly seen in the reduced amount of fines in the tailings of the coarse circuit

The flexible cloths require more frequent maintenance, with poor condition flexible cloths or worn mesh size will resulting in poor separation control. The effects of the use of flexible cloths will be monitored to adapt the exact cloth mesh to the observed conditions.

The improvement is expected to be in place by mid-2024.

11.4.2.4 Improvement 4: Screening of feed material for the shaking tables

The working and performance parameters of the shaking tables have been evaluated, confirming that the feed specifications by the supplier are not reached. Throughout the shift and for days a great variation in the granulometry of the feed to each type of table has been observed. Therefore, the performance of the head hydrosizer that feeds the shaking tables is not optimal. It is considered very important to properly feed the tables with a homogeneous size distribution material, thereby allowing correct separation, as the shaking tables will perform.

It is considered better option to achieve the better control in the tables feed by improving the use of a screen instead of adjusting the current hydrosizer. This is due to the reduction in the maintenance required and an operational improvement.

This improvement is expected to be completed by the end of 2024. The opinion of MiningSense is that the proposed change is reasonable, and that this change would produce a direct effect on recovery as it will increase the performance of the tables.

11.4.2.5 Improvement 5: Change in Spirals

As with the cyclone test, AMP is doing testwork to assess which of the currently available spirals on the market from Mineral Technologies are best suited for this operation. As at June 2024 the first test of three test is being finalized. A report similar to the CY401 test for the cyclones will be delivered at the end of the first test, with a plan for future testing and final recommendations.

It is considered that this change can produce an increase in the recovery although it needs to be proven with testing. The adjustment of the spirals in any case will be a simple test and its improvement is both possible and feasible, considering the poor historic performance of spirals area in particular. It is expected that the testwork discussed will be completed during 2024 so that the change in the spirals is expected to be done on the first quarter of 2025.

11.4.2.6 Improvement 6: Readjustment of the whole system based on previous changes

Between the results of the first and second test of the spirals, Saloro will know exactly how important the proposed screen changes are in order to obtain a high yield in the spirals.

The placement of the screen at this time is based on the data obtained in the plant, where the first AMP tests show similar data to actual results obtained by Saloro. The reduction in performance of the FLSmith and MT screens is thought to be due to the wide grain size range of the feed to the screens, where the fractions >200 microns behave very well, while the fines are lost. Separating these fines and giving them more favourable conditions for recovery as well as the use of a specific type of spiral for them, will generate a real change in plant and spiral recovery. The preceding changes are aimed at individual, isolated areas of the process pant. Whereas this improvement is considering the total process impact, of related stages in the process. Effectively the results of a change in one area, will allow another area to be improved.

This improvement is considered to be possible, but it implies that all the changes produce synergies to increase the recovery and/or consolidate changes in the plant. Saloro shows this improvement as cumulative with the improvement 2 although in the final presentation the apportion to the incremental recovery is not shown specifically.

11.4.2.7 Improvement 7: Changes in the feed fines production

Analysing the closed-circuit trials at the beginning of the project on the ore liberation size, together with the idea of a change in the size of the fractions in the crushing circuit to seek a lower fragmentation of the ore, generating a lower amount of ultra-fines, would mean increasing the mass of ore in the coarse circuit, where Saloro is finding a higher yield than in the spirals.

Knowing the good recovery that Saloro is having in the plant in the coarse circuits, may imply that making a displacement of the feed grain size curve on the >1mm fraction, by optimizing the density of the jig bed would generate an increase in recovery. It is important to emphasize the above because with this change what is really being proposed is to generate a lower amount of mineral liberation, having more mixtures of larger size than the liberated scheelite.

This change should also take into account the additional costs that it would cause in the mine, since part of the fine is generated from there. It would require a smaller bench blast, which would increase the amount of blasting to be done, increasing drilling and explosive consumption.

MiningSense believes that this change is not considered appropriate for to the current estimation of reserves as it is still pending to be properly assessed. In any case it is interesting to study for potential future use.

11.4.2.8 Other metallurgical improvements

Saloro is putting significant effort in trying to align the plant to increase recovery. Some of those changes whose effect is not yet clarified include:

- Reduction of the crushing size to limit the fines production to understand its effect on the Scalping stage and the following ore sorting circuit. For this opening the secondary and tertiary crushing equipment to enable the production of bigger fractions with a reduction in fines production and power consumption. The goal is to get a good separation in the Scalping stage with the basis that the ore particles would be liberated, and only the quartz or feldspar grains would remain in the coarse fractions: changing the final product of the secondary crusher from 8/20 to 8/40 mm.

- Ore sorting is a key factor that increases the recovery by rejecting the majority of the waste separated in the scalping circuit. Currently 2 ore sorters are working in parallel, and there are plans to include a third one.
- Incorporation of a Falcon circuit.

11.4.2.9 Summary of the 7 measures to improve recovery

The Figure 11-4 shows those initial improvements for increasing the recovery.

Improvement	Current	Alumina 3.2 SG	Cyclon	Felxible cloths	Crushing optimization	Optimization tables feed	Spirals change	Change in tables head screen
Max. recov. increase	=	2-3%	1-2%	1-2%	5%	2-3%	2-5%	5-10%
January	50%	53%	53%	55%	55%	55%	55%	55%
February	50%	53%	53%	55%	56%	56%	56%	56%
March	50%	53%	55%	57%	58%	58%	58%	58%
April	50%	53%	55%	57%	58%	60%	60%	60%
May	52%	55%	55%	57%	58%	60%	60%	60%
June	52%	55%	57%	59%	60%	62%	62%	62%
July	52%	55%	57%	59%	60%	62%	64%	64%
August	52%	55%	57%	59%	62%	64%	66%	68%
September	55%	58%	57%	59%	62%	64%	66%	70%
October	55%	58%	59%	61%	64%	67%	69%	72%
November	55%	58%	59%	61%	64%	67%	72%	76%
December	55%	58%	59%	61%	66%	69%	74%	79%

Figure 11-4 Incremental impact of recovery improvement plan stages

The following graph summarises the incremental increase in the recovery and the contribution of each of the seven measures exposed in this chapter as per Saloro's plan. The presentation with the contribution of each improvement is shown in the appendix 4 as a Saloro presentation, where it appears as part of the spirals circuit change the incorporation of a Falcon to improve ultrafines recovery. As can be seen in Figure 11-5 the improvements 6 and 7 are not considered material, for this reserves estimation. They are not certain to deliver any increase in the recovery as they need to be tested properly. This is the reason why MinignSense are using 71% as a long term recovery for ORE, whereas Saloro are discussing a 78% recovery after all of the improvement plan is implemented.

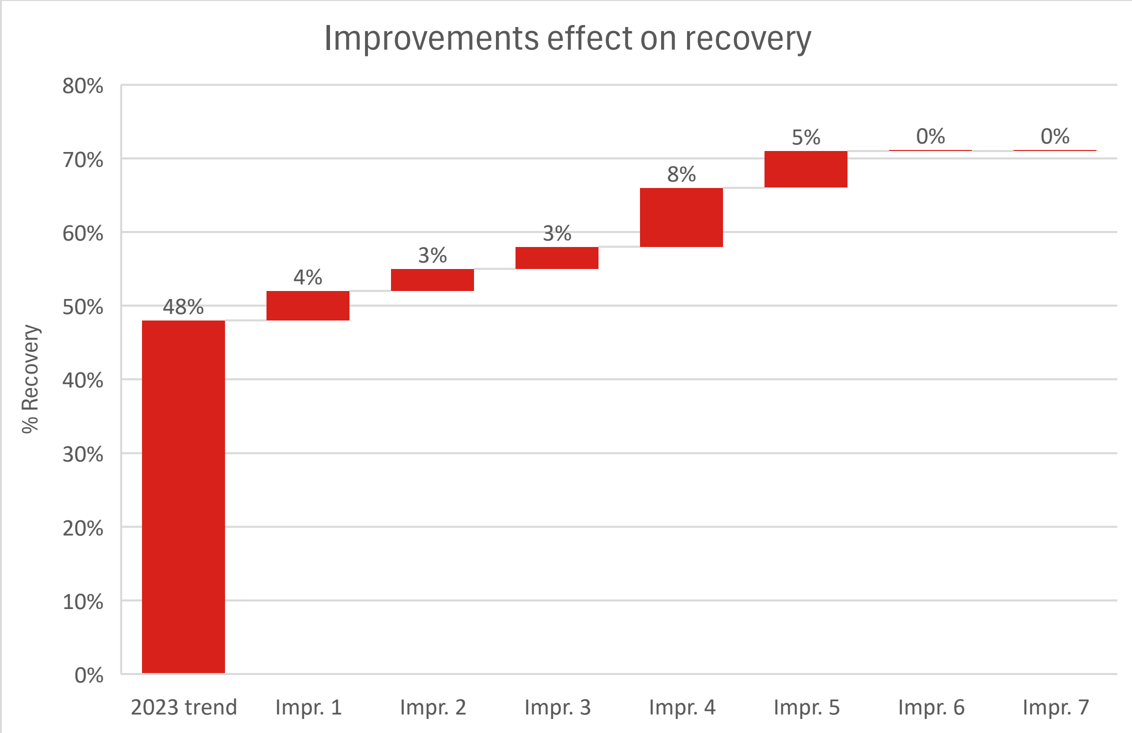


Figure 11-5 Apportion of improvements to the global metallurgical recovery

11.4.2.10 Process Plant throughput improvements

11.4.3 Implementation program and expected recovery curve

In January 2024 the first improvement was put in place. of the impact on recovery is shown in Figure 11-6.

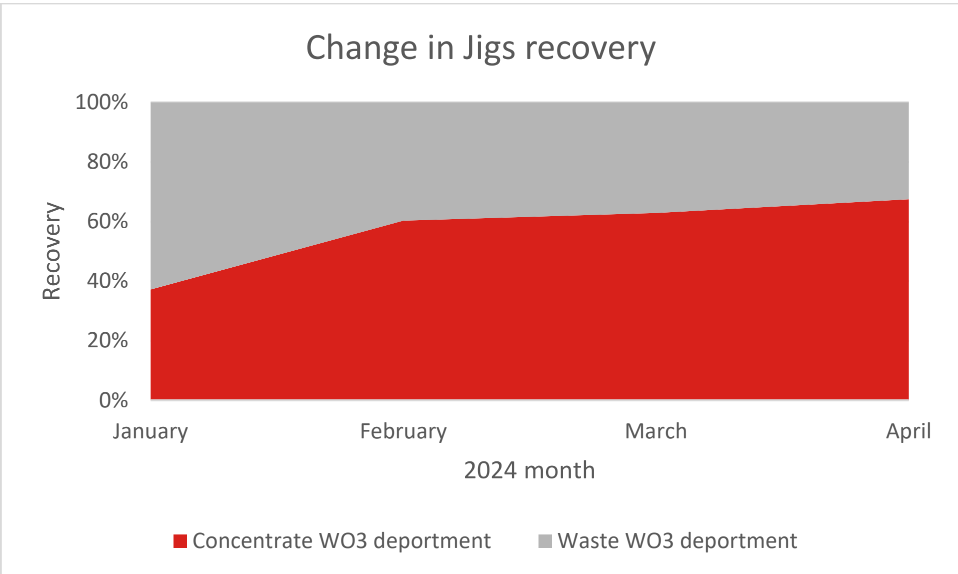


Figure 11-6 Recovery Improvement #1 Change Jigs configuration

During the writing of the current ORE report, Saloro is completing the changes in the plant to incorporate the following 3 improvements, after the change in the jigs in January. The results will be seen in coming periods but the expected recovery curve is shown in the Figure 11-7 for the first two years after the changes are done. Another 3 improvements will be developed to complete the 7 described above to get the 71% recovery.

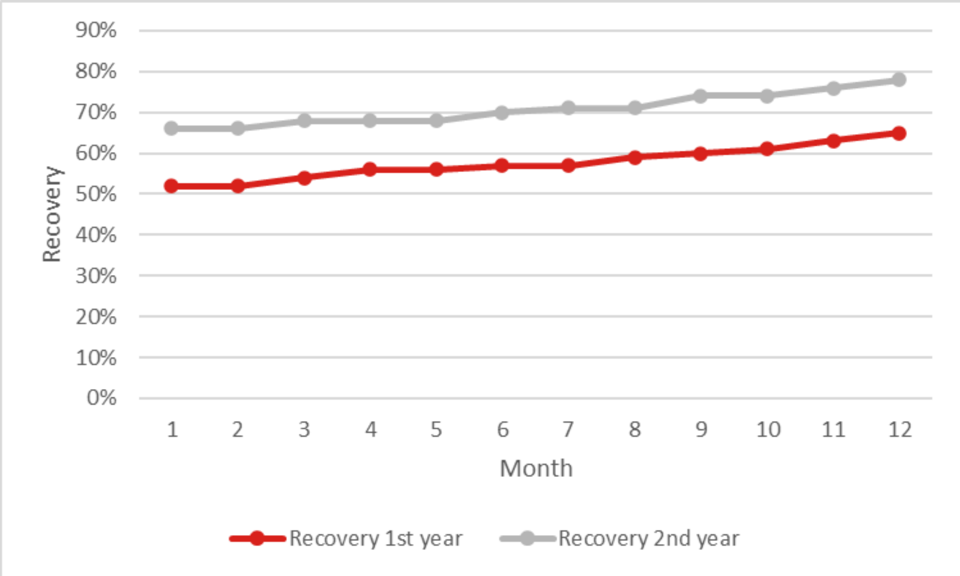


Figure 11-7 Expected recovery curve with processing plant improvements (Client plan)

The opinion of MiningSense is that the recovery curve can be up to 71% based on the combination of the improvements shown in the Figure 11-4 and Figure 11-5, and without considering the potential effect of the improvement numbers 6 and 7.

The recovery shown in the Figure 11-7 is then, for the purposes of this Ore Reserves Estimates reduced to a maximum of 71% recovery by the end of the second year after the improvements in the plant are implemented. See figure below.

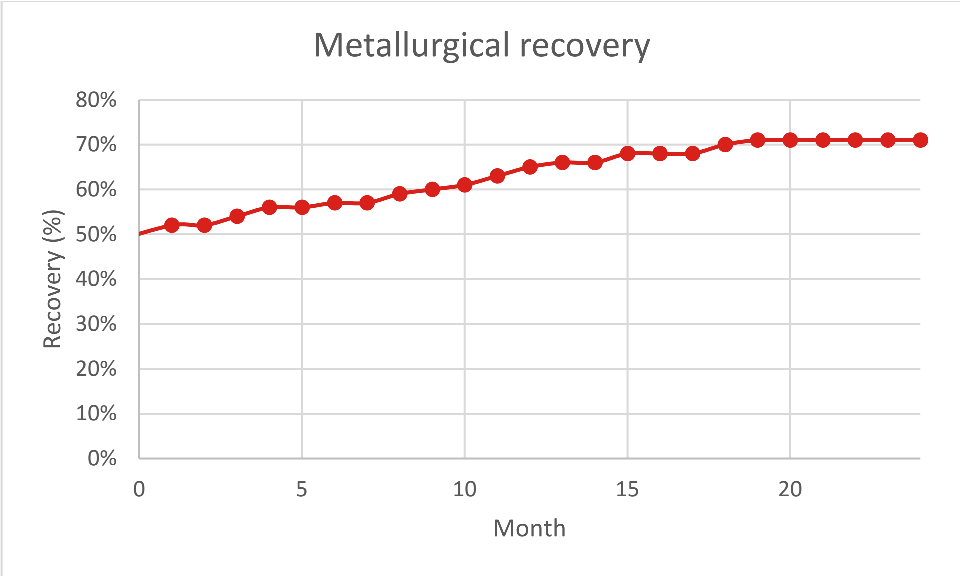


Figure 11-8 Metallurgical recovery profile used for the ORE

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11.5 Costs

The changes that will drive the recovery improvement implies an expenditure on new equipment, training and operational aspects. The following figure shows the plan to put in place those improvements in the plant.

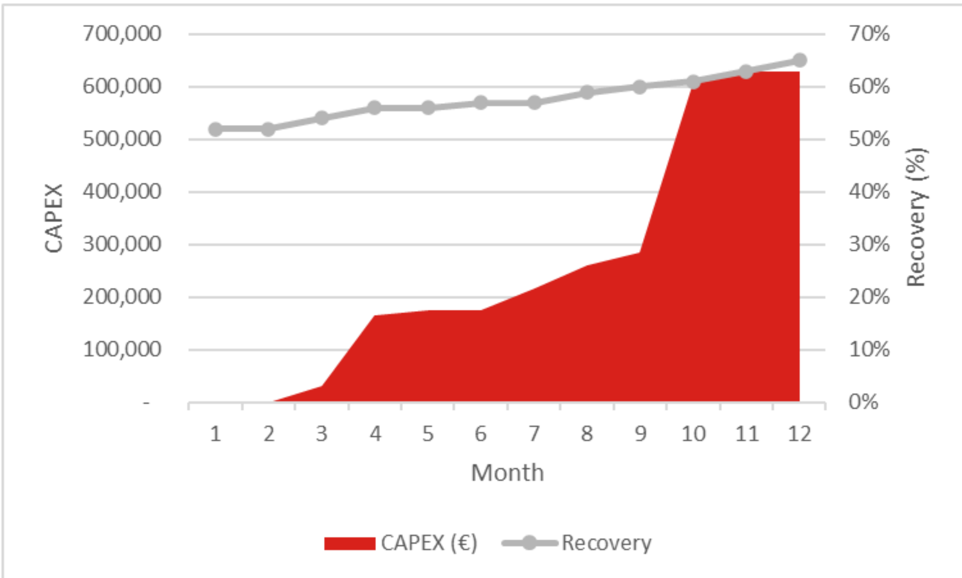

Figure 11-9 CAPEX in plant VS expected recovery during the first year

12 Environmental, social and permitting

The Environmental License (Declaración de Impacto Ambiental) for the project was granted in 2014. This environmental license relies on the Mining License. This license was applied for in 2012 capturing the project as described in the 2012 Exploitation Project and Rehabilitation Plan that includes the direction on mine closure. The costs included in the economic analysis are done to achieve the requirements stated in the Rehabilitation Plan approved by the Mining and Environmental Licenses.

The Mining License (ML) was granted in December 2014 for a period of 30 years, the license is then active and still has more than 20 years validity.

In 2015 the City Council of Barruecopardo granted the urban development license and the authorization of exceptional use in common rural land for the reopening of the wolfram mining operation promoted by Saloro. These three constitute the significant operating licences required.

The mining activities in any case should follow those as described in 2012 application for which the mining license was granted in 2014. Any material change would need a specific approval. This approval would have to follow the same permitting route as a original mining license, including a public consultation and environmental impact assessment.

The precise meaning of “material change” is unclear but can be summarised as:

- Increase in the production (process plant)
- Increase in the footprint
- Increase in the waste produced
- Material changes in the mining method
- Material changes in the waste management
- Important changes in the water discharge
- Important changes in the emissions

Material changes do not include change to the production rate, mining method, waste management method, water discharge or project emissions. Therefore, a completely new mining licence is not required for those changes. However, the increase in mining reserves implies a change in the footprint of the pit and the waste dump. These will require extra extensions to permits, as discussed previously.

Due to the highly favourable perception of the mine in the area it is not expected that the Social License would be declined and hence, based on the very good performance on environmental aspects of the project, the Environmental License for a new project is likely to be granted.

The existing Mining License could last until the end of the phase 3, according to the existing pit footprint approved of 34Ha, recorded in the existing mining license. The final pit contained up to the phase 3 considered 36Ha that is considered similar to the already approved 34Ha. It is after the phase 3 when an extension of the current mining project is needed. With the current phase development it is expected to open phase 4 before phase 3, which means that the permit extension needs to be granted by 2026.

During the period in which Saloro has operated the Barruecopardo mine no environmental incidents/accidents have been reported. The company has tried to minimize the possible environmental effects, in compliance with the regulations and the Environmental License.

The monitoring program for the protected animals in the project area has gained wide recognition by the local society and the environmental professionals.

The company put in place a system of visits for the public, so as to be transparent and open to the society.

The Barruecopardo mine is in a highly sensible environmental area, forming part of the Natura 2000 European Network. The mine is in the border of the Las Arribes del Duero Natural Park and very close to the Portuguese border where there is the Douro International Natural Park on the other side of the Duero River.

13 Costs

13.1 Introduction

Saloro has provided the planned capital expenditure to maintain production and to implement the outlined changes in the processing plant to increase recovery, and the operating costs. These have had minor adjustments by MiningSense on the sustaining capital. MiningSense has developed the calculations for haulage distances to adjust the associated contract costs to the proposed mine plan. This has been done with reference to the clauses in the current mining contract. The rehabilitation cost has been used from the original rehabilitation plan of 2012, updating to actual costs by reference to the CPI basis and using the final surface for the mine plan.

13.2 Capital Expenditure

Sustaining capital has been estimated based on an annual expenditure of 100k€, typical for a plant of 10M€ initial cost, as the maintenance and care and control costs are included as OPEX.

On top of the sustaining capital expenditure cost, Saloro has provided the costs associated costs with the recovery improvement plan. Table 13-1 shows the expected expenditure.

Table 13-1 Recovery improvement plan Capex

Item	U.	Total	Yr1-Q1	Yr1-Q2	Yr1-Q3	Yr1-Q4
Improvement 1: Alumina beds in Jigs (already done)	€	**-**	-	-	-	-
Improvement 2: Change in CY401	€	**90,000**	21,000	-	69,000	-
Improvement 3: Flexible screens	€	**80,000**		45,000	-	35,000
Improvement 4: Screening table feeding	€	**200,000**	-	50,000	-	150,000
Improvement 5: Spirals	€	**200,000**	-	40,000	-	160,000
Improvement 6: Circuit adjustment	€	**60,000**	10,000	10,000	40,000	-
Improvement 7: Changes to reduce fines	€	**-**	-	-	-	-
Total	€	**630,000**	31,000	145,000	109,000	345,000

The following figure shows the CAPEX expenditure over the life of mine, including a sustaining capital figure of 100,000€ per year.

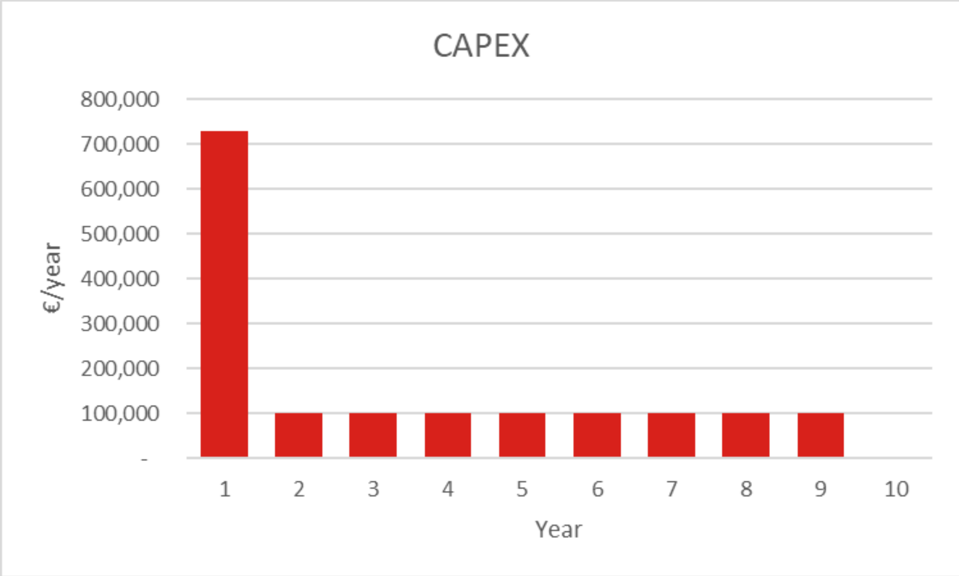

Figure 13-1 Yearly CAPEX

The total CAPEX over the life of mine accumulates to 1.53M€. This cost does not include the rehabilitation costs that are a separate cost as discussed in section 13.4.

13.3 Operating costs

Unit operating costs have been derived from the Saloro' own cost reports the existing contracts in place as follows:

- Ore and waste movement is subcontracted to PEAL company since 2020.
- Waste management is subcontracted to PEAL, including the tailings management.
- Crusher feed is subcontracted to PEAL.
- Plant is operated by Saloro.
- Mine management is done by Saloro
- General management is done by Saloro

The PEAL contract that drives the mine costs has been read and used by MiningSense. The 2020 contract was made for 3 years plus another two, the automatic extension has been exercised, and the contract is now in its' fourth year. In one year, the contract will expire, and a new contract will need to be agreed. The good contract performance until now and the potential increase in the total ore and waste movement per year are good basis to think that is probable that pricing and performance should be maintained in similar conditions. The contact includes a rise and fall formula to update the prices based on current salaries, explosives, fuel and spare parts variation No escalation of prices has been considered in the assessment of operating cost

13.3.1 Mining costs

As indicated previously, the mining cost are primarily driven by the PEAL contract. The contract as such is not included in this ORE report but the summary of the main cost results is shown in Table 13-2.

Table 13-2 Mining OPEX breakdown

Item	Unit cost	Units	Total cost (LoM)
Mine			**122,235,182€**
Waste			82,021,775€
Mining	3.75	€/bcm	78,225,314€
Extra-distance	0.04	€/bcm/Hm	3,796,461€
Ore			**17,541,910€**
Mining	4.03	€/bcm	17,043,969€
Extra-distance	0.04	€/bcm/Hm	497,941€
Others			**22,671,497€**
Contour blast	199.33	€/month	16,743€
Grade control	1.02	€/oret	4,333,208€
Primary crusher feed	0.36	€/t to plant	4,176,088€
Mine dewatering cost	17,806.75	€/month	1,495,767€
Mine technical department	150,591.56	€/month	12,649,691€

The total cost over the life of mine for mining activities sums 122.2M€, divided in:

- Waste mining: 82.0M€
- Ore mining: 17.5M€
- Others (including owners mining supervision costs): 22.7M€

13.3.2 Processing costs

The plant is fully operated by Saloro team. The costs have been divided into:

- Processing fixed costs: includes all the costs not dependent on the ore tonnes processed, working in normal conditions. Specifically, it includes labour costs, amortization costs for the equipment and maintenance services.
- Processing variable costs: includes the rest of the costs to process the ore and varies with the tonnes and quality of the ore processed. Specifically, it includes: power, spare parts, water management, reagents, consumables and spare parts. Updated to June 2024.
- Tailings management costs: the tailings transport to the final installation facility is subcontracted to the mining contractor (PEAL at present moment). It is conceptualised as a cost per tonne moved to the TSF.

Table 13-3 shows the breakdown of the processing costs.

Table 13-3 Processing OPEX costs

Item	Unit cost	Units	Total cost (LoM)
Process			**83,644,115€**
Fixed costs	485,562	€/month	40,787,221€
Variable costs	2.92	€/t	34,215,112€
Tailings management	0.74	€/t	8,641,782€

13.3.3 General and Administration costs

The general and administration costs have been provided by Saloro as unit cost per year. It includes the general administration and services costs: admin office costs, communications, insurances, labour…

The summary of those costs is shown in Table 13-4.

Table 13-4 General and administrative OPEX costs

Item	Unit cost	Units	Total cost (LoM)
G&A			**16,577,793€**
Technical office	35,646.87	€/month	2,994,337€
General and administration	161,707.81	€/month	13,583,456€

13.3.4 Selling costs

Apart from the payability of the ore, it is also considered a transport cost to port so that the assumed selling price is a FOB price. Table 13-5 summarises the selling cost.

Table 13-5 Selling costs summary

Item	Unit cost	Units	Total cost (LoM)
Selling			**3,587,013 €**
Transport cost	2.85	€/mtu WO_3	3,587,013 €

The selling cost is considered per WO_3 mtu sold. Assuming an average grade of 65% WO_3 in the concentrates, the equivalent unit cost per tonne of concentrate is €182.6/t of concentrate.

13.3.5 OPEX summary

The Figure 13-2 shows the components of the OPEX over the life of mine.

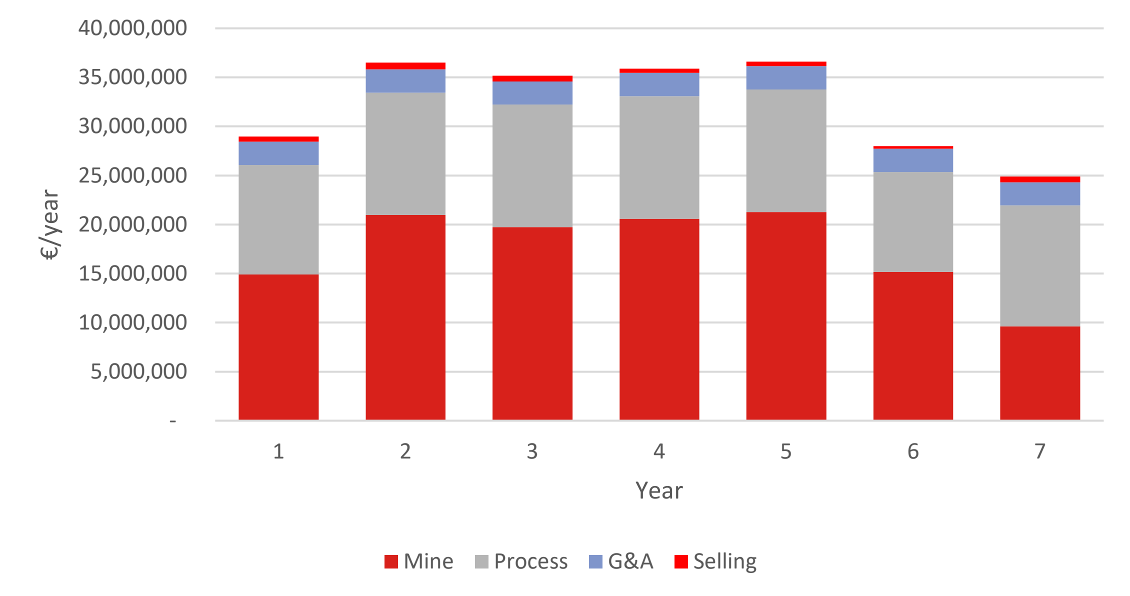

Figure 13-2 OPEX over the life of mine

Table 13-6 shows the total OPEX cost distribution.

Table 13-6 OPEX total and unit cost estimate

Item	Unit	Yearly	TotalLoM	€/t(o+w)	€/tore	€/mtuWO3
Mine	k€	13,582	122,235	1.90	11.05	97.24
Process	k€	9,294	83,644	1.30	7.56	66.54
G&A	k€	1,842	16,578	0.26	1.50	13.19
Selling	k€	399	3,587	0.06	0.32	2.85
Total OPEX	k€	**25,116**	**226,044**	**3.51**	**20.43**	**179.82**

13.4 Rehabilitation costs

Those costs are based on the cost estimation done in 2012, updated to 2024 as per CPI when no actual costs are available. For the waste dump slopes rehabilitation it has been used the 2024 unit costs provided by Saloro. Up to 31 May 2024 a total of 10Ha has been rehabilitated. An initial bond of 1.5M€ was put as a warrantee of the future rehabilitation works to be done. This bond is recoverable if the final rehabilitation fulfils the requirement of the mining and environmental licences as assessed by the authorities. The recovery of this bond is not considered for the model

The most important activities related to the rehabilitation are:

1. Topographical restoration and revegetation.
2. Processing plant & facilities decommissioning.

The rehabilitation for the pit is limited to adapting some areas of the pit to a 20m height to make them more suited for future birds' habitat. Most of the pit slopes are already with this configuration so it is expected limited work in this area will be required.

The topographical restoration includes: landform, topsoil placement, revegetation and maintenance a total cost per square meter have been calculated from the Rehabilitation Plan (Sadim, 2012) approved, that indicates a 25cm topsoil thickness and a combination of seeds for the revegetation. The total cost to rehabilitate the slopes of the waste dump is €1.68/m^2, provided by Saloro.

Regarding the decommissioning, the Rehabilitation Plan indicates a total of 3,142,626€, including the rehabilitation of:

- Final waste dump
- North pond
- Plant area
- Sulphide area
- North dam slope
- Main haul roads
- In pit waste dump
- General
- Post-closure

The previous decommissioning cost has been factorized to update the 2012 to 2024 costs by used CPI again. So, the decommissioning cost used is 3,928,283 €.

The following table shows the rehabilitation costs breakdown.

Table 13-7 Rehabilitation costs

Item	Unit cost	Units	Total cost (LoM)
Rehabilitation			**5,112,832 €**
Waste Dump Slope Rehab	1.68	€/sqm	1,223,549 €
Decommissioning and post-closure	3,928,283	€/year	3,928,283 €

Over the life of mine it has been assumed that the waste dump rehabilitation is done on continuous basis. At the end of the mine life the decommissioning cost will be incurred.

14 Technical Economic Model

MiningSense has prepared a high-level technical economic model to test the economic viability of the Ore Reserves under the given set of assumptions for the Saloro open pit operation. MiningSense notes that the net present value ("NPV") as presented herein does not constitute a valuation of the asset and is solely to comply with the JORC Code to demonstrate Reasonable Prospects of Economic Extraction (RPEE).

14.1 Production Plan

The section 8 of this report describes the mine plan proposed to mine the reserves, it includes the consumption of the current stockpiles and their change along the life of mine to accommodate the available material in the pit and the plant capacity.

A total plant feed (primary crushing feed) of 108,700 t of ore per month during first year and 141,820 t of ore the rest of the LoM have been considered. The primary crusher feed is shown in the Figure 14-1. The figures in that table include mining losses and dilution.

The metallurgical recovery is shown in Figure 14-1

, where year -1 corresponds to year 2023 and year +1 corresponds to year 2024 in which the majority of the changes in the plant has been made although the final recoveries are expected to increase in the following year (2025 or year +2). The mine plan has been developed with objective of maintain a minimum WO_3 production of 7 deliveries of 20t concentrate per month equivalent to 1,680t concentrate per year.

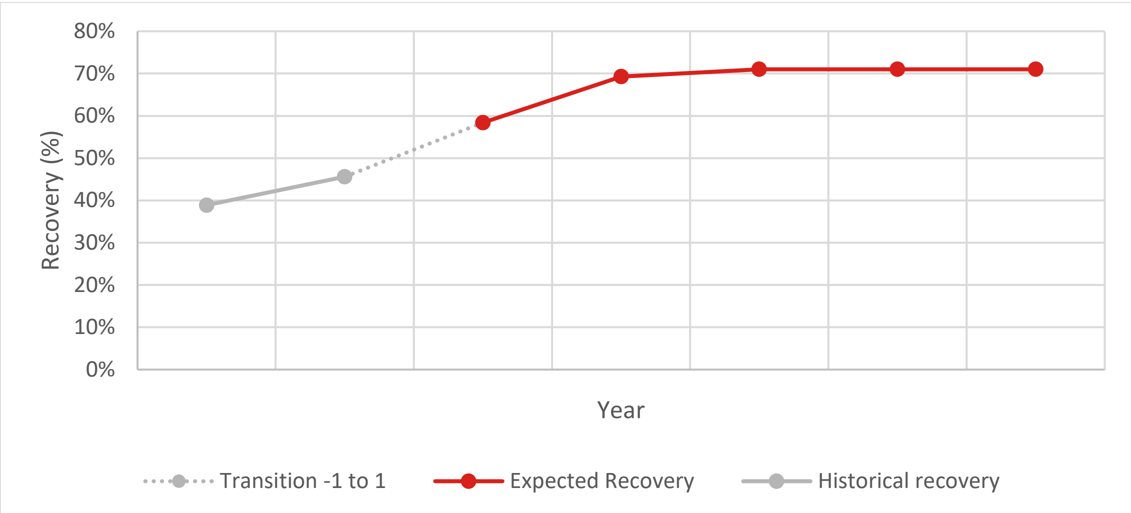

Figure 14-1 Recoveries: historical and assumed for the LoM

The concentrate produced is shown in Figure 14-2 . It has been assumed a flat 64% WO_3 in the concentrate.

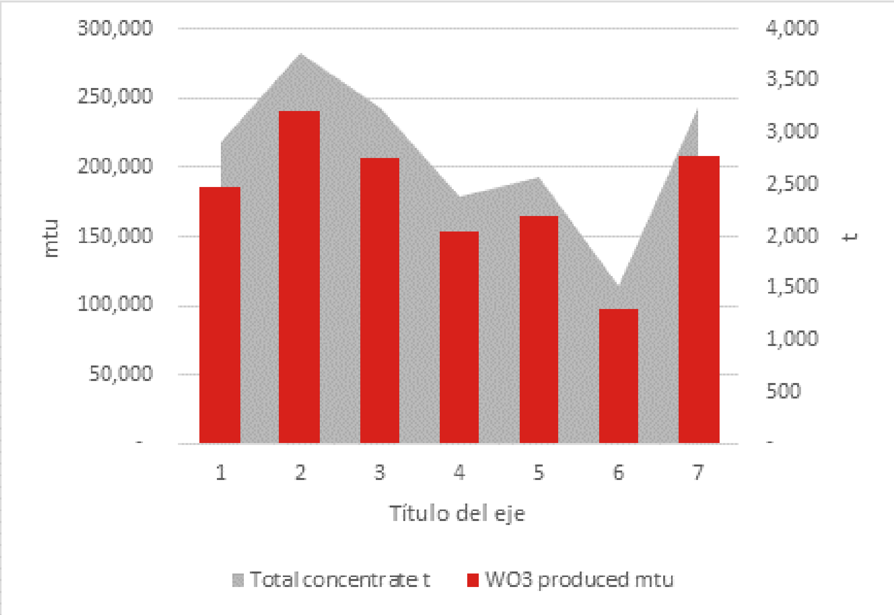

Figure 14-2 Concentrate production

14.2 Sales

The sales of concentrate have been considered with an APT price based on the Wood Mackenzie forecast as outlined in the discussion regards cut-off grade as a base case.

The following table summarizes the WM base case forecast from 2021 to 2030, after year 2030, as no forecast is available, a flat price of US330$/mtu has been considered for the base case.

Table 14-1 WM forecast APT price scenarios for the period 2021 to 2030

	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030
WM APT base	**280.0**	**330.0**	**320.0**	**310.0**	**315.0**	**330.0**	**330.0**	**330.0**	**330.0**	**330.0**
WM APT low	265.0	275.0	280.0	280.0	280.0	275.0	270.0	265.0	260.0	260.0
WM APT high	340.0	370.0	385.0	390.0	395.0	400.0	405.0	410.0	415.0	415.0

A flat exchange rate of US1.10$:1.00€ has been considered. All cost and revenue are in 2024 Euros, No inflation or scaling has been considered for the model.

Payability used is 78% according to the average payability considered between the 3 contracts on place. A fixed rate of taxes of 25% on the revenues has been considered.

14.3 Results

Financial assessment was completed to check reasonable prospects of positive economic outcome using these factors and assumptions.

This resulted in the Competent Person being of the opinion that there indeed are reasonable prospects of economic extraction.Economic KPIs

The summary of the physicals derived from the mine plan are shown in Table 14-2.

Table 14-2 Mine plan physicals

Parameter	Unit	Value
Waste mined	t	53,408,158
Ore	t	11,065,695
Av grade	WO_3%	0.16
WO_3 contained	mtu	1,735,537
WO_3 recovered	mtu	1,257,064
Concentrate produced	t	19,642

The material considered ore, including ore loss and dilution, in the mine plan contains 7,976,305t coming from measured resource, 3,391,246t coming from indicated resource and 153,683t inferred resource material. In this production plan the inferred material but is not considered as ore it is considered as waste. In this production plan the inferred material is not considered at all.

The all-in unit cost is shown in Table 14-3 in US$.

Table 14-3 All in Unit cost summary

	US$/t(o+w)	US$/tore	US$/mtu$WO_3$
Mine	2.09	12.15	106.96
Process	1.43	8.31	73.19
G&A	0.28	1.65	14.51
Selling	0.06	0.36	3.14
Total OPEX	3.86	22.47	197.80
Total CAPEX	0.02	0.13	1.16
Total Rehabilitation	0.09	0.51	4.51
Total OPEX+CAPEX+Rehab	3.97	23.11	203.47

14.4 Sensitivity analysis

A sensitivity analysis on various economic drivers of the operation has been completed. The influence of changes in percentage of price, recovery, exchange rate and grade have the same effect on the project economics, so it is more interesting to understand which of these can cause that the project to become non-economic.

The following graphs, Figure 14-3 to Figure 14-8 shows this situation for the four main drivers of the project.

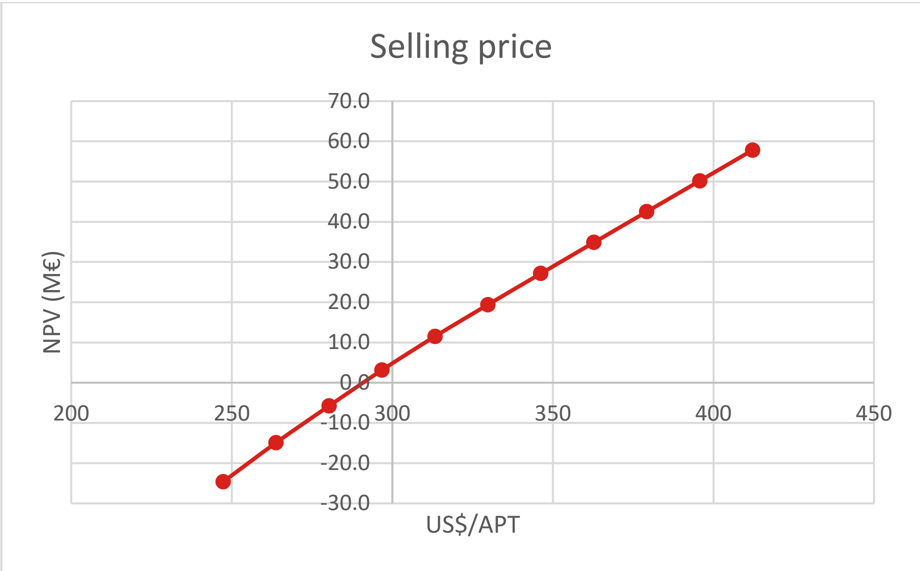

Figure 14-3 Sensitivity analysis on the selling price (US$/APT)

The project becomes un-economic with a selling price of US$300/mtu(APT).

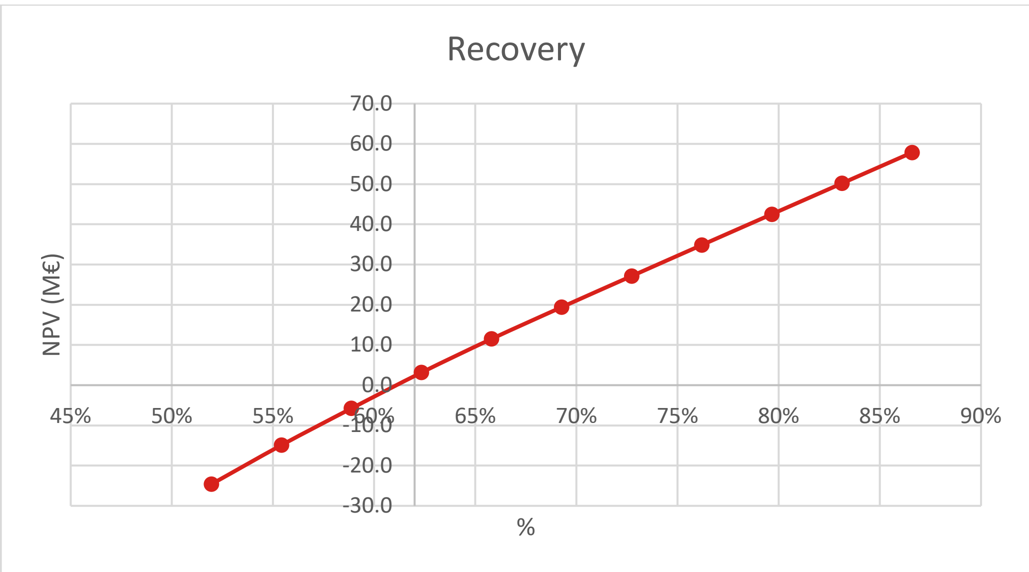

Figure 14-4 Sensitivity to metallurgical recovery

The sustained recoveries below 60% makes the project un-economic.

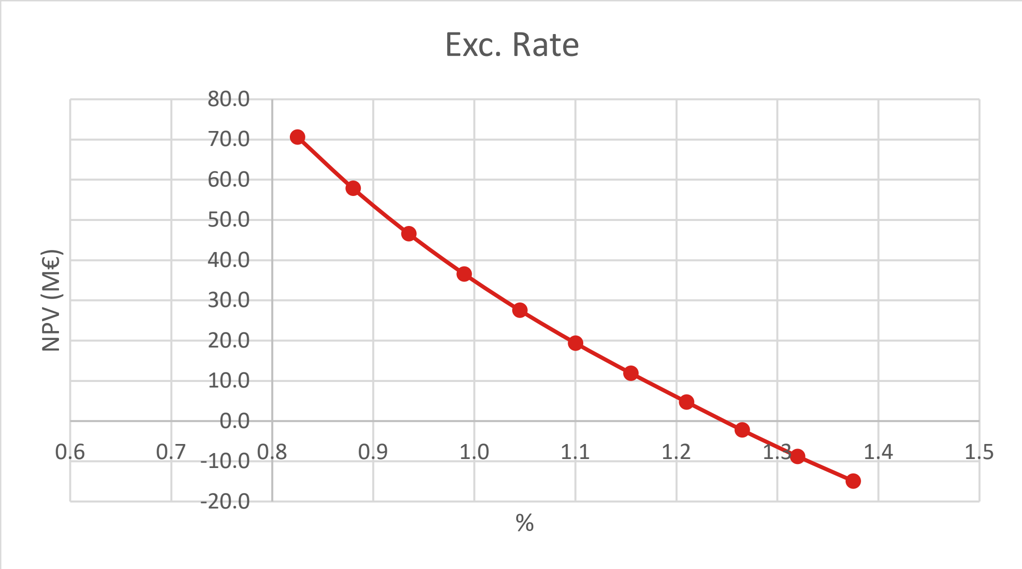

Figure 14-5 Sensitivity to exchange rate

The exchange rate US$/EUR above 1.2 makes the project un-economic.

Regarding opex and capex the influence of those is shown with percentage of variation in the following graph.

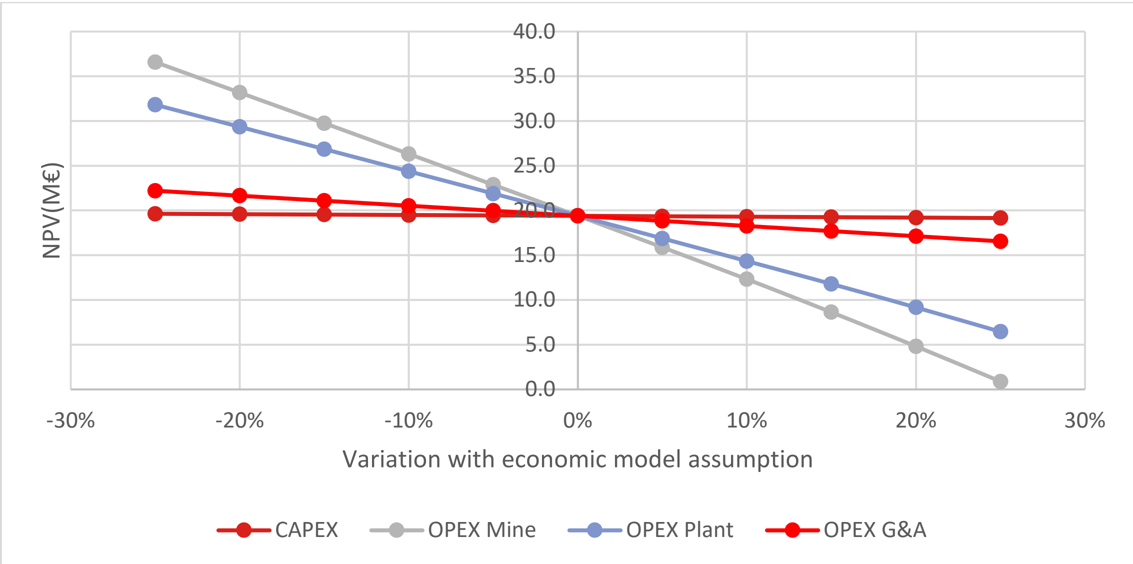

Figure 14-6 Sensitivity to variation in costs

The cost that has more influence in the project value is the mine cost, but this needs an increase of more than 20% to make the project un-economic.

It is interesting to understand how the break-even cut-off grade moves with changes in metallurgical recoveries, as shown in Figure 14-7.

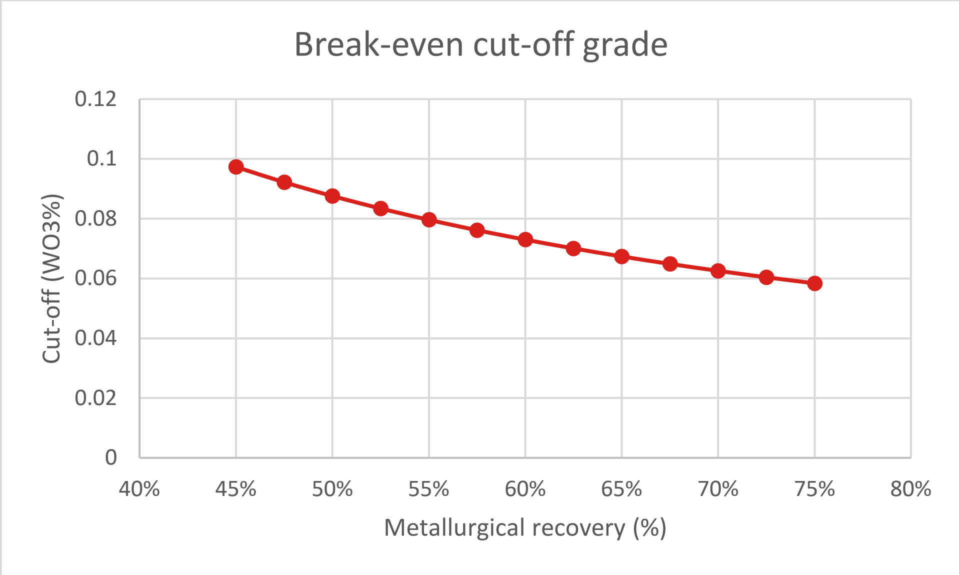

Figure 14-7 Cut-off grade sensitivity to metallurgical recovery

Another important factor that can produce an improvement in the project value is the control of the dilution. The assumed dilution after block model reblocking is 15%, this produces a total dilution of 29%, combining the planned and the operational dilution. An ideal 0% dilution is not technically achievable but with better technologies and operational control it is considered achievable to reduce the operational dilution to 5% what means an overall dilution of 18%.

The following graph shows the influence of the overall dilution in the project economics.

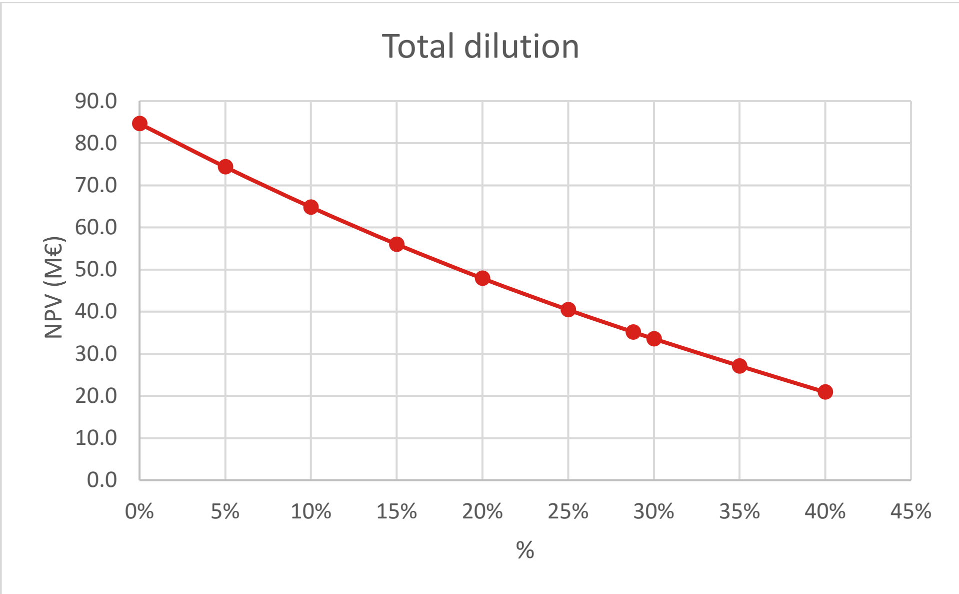

Figure 14-8 Sensitivity to variation in overall dilution

A reduction of the overall dilution to 20% (from the current 29%) almost increase the project value a 37%. Therefore, investment required to support the reduction in dilution would likely be supported.

14.5 Conclusions on the economic analysis

- The economic model considers 7 years of sustained production.
- No negative cash-flow is produced in any year from the year 1 to the year 7.
- The mine plan considered within reserves produce a positive project NPV.
- The mine plan is hence considered feasible from the technical and economical point of view.
- The project is very sensible to external factors like the price and the exchange rate.
- The project is relatively not sensible to the costs.
- The project is highly dependent on the recoveries, with recoveries maintained below 60% makes the project un-economic.
- The recovery, a Saloro controllable risk, is the main driver of the project that can be modified with better technology or controls as Saloro is trying to implement. However, this is also the riskiest factor and with existing recoveries the project is hardly economically feasible.
- Other Saloro controllable risk with an important influence on the project economics is the dilution. A reduction in the operational dilution to 5% from current 15% (global dilution of 18-20%) could improve the project economics by increasing its NPV a 37%.

15 Ore Reserves Estimate

The Table 15-1 shows the Resource conversion into Reserves.

Table 15-1 Resource to reserve and design conversion

	Mineral Resource Estimation Cut-Off 0.05			Ore Reserve Cut-Off 0.06*			Pit Design Cut-off 0.06*			
Category	**Tonnes (Mt)**	**Grade (WO_3 %)**	**Contained Metal (t of WO_3)**	**Tonnes (Mt)**	**Grade (WO_3 %)**	**Contained Metal (t of WO_3)**	**Tonnes (Mt)**	**Grade (WO_3 %)**	**Contained Metal (t of WO_3)**	**Category**
Measured	10.05	0.191	19,196	7.13	0.155	11,021	7.68	0.164	12,581	**Proven**
Indicated	10.46	0.174	18,200	3. 33	0.141	4,704	3.40	0.141	4,770	**Probable**
Inferred	3.86	0.259	9,997							
Grand Total	**24.37**	**0.195**	**47,522**	**10.46**	**0.156**	**16,367**	**11.07**	**0.157**	**17,351**	

*Includes loss and dilution

The Ore Reserve Estimation in accordance with the JORC Code (2012 Edition) guidelines are reported in the Table 15-2.

"An Ore Reserve is the economically mineable part of a Measured and/or Indicated Mineral Resource. It includes diluting materials and allowances for loses, which may occur when the material is mined or extracted and is defined by studies at Pre-Feasibility or Feasibility level as appropriate that include application of Modifying Factors. Such studies demonstrate that, at the time of reporting, extraction could reasonably be justified." JORC Code (2012 Edition)

This Ore Reserves have demonstrated economic viability as shown in 14 Technical Economic Model and it can be declared with sufficient confidence extending the Life of Mine.

Table 15-2 Ore Reserves Statement September 2024

Classification Category	Mining Type	Tonnes (t)	Grade (WO_3%)	Metal contained (mtu)
Proven	Open-Pit	6,816,530	0.16	1,102,148
	Stockpile	314,723	0.14	
Total Proven		7,131,253	0.155	1,102,148
Probable	Open-Pit	3,332,177	0.14	470,387
	Stockpile			
Total Probable		3,332,177	0.141	470,387
Total	Open-Pit	10,148,707	0.16	1,572,535
	Stockpile	314,723	0.14	64,143
Total Ore Reserve		**10,463,430**	**0.156**	**1,636,678**

A summary of the assumptions and inputs are listed below:

- Reported from the reserves block model saloro_202310_res_rot_6x6x5.mdl regularized block model from the resources block model saloro_202310_res_rot.mdl.
- Cut-off grade 0.06 % WO_3 for the long-term used for all the stages of the project.
- Modifying factors operational loss 6% and 15% operational dilution over a regularised model that includes 2% loss and 12% dilution against the resource model.
- Metallurgical recovery of 58% during first year of production and the rest of LoM metallurgical recovery of 71%.
- Stockpiles A, B, OP and scalping have been considered. No marginal stockpile is included in this Ore Reserve Statement. Although it has been included in the LOM mine plan developed to test reasonable economic extraction. This is minor in quantity, and described in section 8.
- The reporting standard adopted for the reporting of the ORE uses the terminology, definitions and guidelines given in the Joint Ore Reserves Committee (JORC) Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (2012).
- It is considered that last report completed in 2012 scheduled 9 years of production starting in 2019 and this ORE reports additional 7 years of production plan which means the LoMP has been extended a total of 3 years of production since last ore reserves declaration. Below, in Table 15-3, 2012 MRE and reserves included in the production plan in the exploitation project for reference.

Table 15-3 2012 MRE and Reserves

	MRE 2012			Reserves 2012 (not under standard code reported)			
Category	**Tonnes (Mt)**	**Grade (WO_3 %)**	**Contained Metal (t of WO_3)**	**Tonnes (Mt)**	**Grade (WO_3 %)**	**Contained Metal (t of WO_3)**	**Category**
Measured	5.47	0.34	18,000	5.20	0.37	19,209	**Proven**
Indicated	12.33	0.26	32,000	2.87	0.32	9,169	**Probable**
Inferred	9.59	0.23	22,000	0.81	0.24	1,975	
Grand Total	**27.39**	**0.27**	**72,000**	**8.07**	**0.35**	**28,378**	**Proven + Probable**

16 Risk assessment

The ability in achieving and/or delivering the ore reserve estimate included in this report has been assessed and likelihood evaluation in a matrix in Appendix 2, highlights have been summarized in Table 16-2. Although a risk assessment is not required in the JORC 2012 edition, it is a likely required inclusion of future revisions to JORC, and hence is provided here for forward compatibility.

The risk score is built in dependence of the severity of the consequence and the likelihood of the event. Consequence goes from insignificant to catastrophic, the likelihood of the event occurs goes from rare to almost certain and the risk score from low to high as shown in the risk assessment Table 16-1.

Table 16-1 Risk assessment factors

Consequence	Likelihood	RISK SCORE
Insignificant	Almost Certain	High
Minor	Likely	
Moderate	Possible	Medium
Major	Unlikely	Low
Catastrophic	Rare	

The combination of the two factors, delivers the risk score which gives the level of the risk and will guide to prioritize the mitigation actions to decrease the severity of the consequence if implemented.

Table 16-2 summarizes the risk assessment of the project per area and suggestions on how to mitigate or decrease the risk with possible action plan. As the result of this risk evaluation in has been acknowledged that improvement opportunities in some areas do exist. These are described in section 17.1. Corresponding action plan is covered in section 17.2 .

Table 16-2 Risk & Mitigation assessment

Area	Unwanted Event	Unwanted result	Inherent Risk Level	Existing Control	Mitigation
Metallurgical Recovery	Plant improvement plan does not deliver forecast recovery improvement	Lower recovery means lower metal produced.	H	Project Plan	Define KPI to follow-up and action plan B
Metallurgical Recovery	Plant improvement plan is much slower to deliver recovery improvement, than planned	As above.	H	Project Plan	Project Management and reporting
Metallurgical Recovery	Concentrate quality lower than limits	Reprocessed will be needed, increase in costs.	M		
Mineral Processing	Decrease of availability, less operating hours per year	Lower process throughput	M		
Geological Risk	unforested elevated deleterious elements	Revenue penalty deductions.	L	Product sampling	Geological modelling
Geological Risk	Resource model consistently underperforming	Actual grades lower than forecast; thus less metal	M	Grade control	Monthly reconciliation process
Geological Risk	Indicated resources don't become Measured resources	Lower proved reserves	H	Geology control	Exploration campaign in defined area
Geological Risk	North area veins not as homogeneous as expected	Higher dilution	M	Geology control	Different composites definition for North and South. More drilling and sampling needed
Revenue	Actual APT price received consistently below the WoodMac 2021 forecast	Wrong revenue assumption used in reserve estimate	M	Nil	Use contracted prices
Revenue	Chain supply break	Reduction in the concentrate production.	L		Secure stock with long-term contracts
Mining Operations	Not "clean" Mining of ore zones. Thus more loss, and more dilution	Lower metal	M	Pit Supervision	Training of excavator operators

Area	Unwanted Event	Unwanted result	Inherent Risk Level	Existing Control	Mitigation
Mining Operations	Lower actual productivity. Can not achieve the nominal mine plan	Either lower tonnes, or higher costs; or both	M		
Cost Base	Unexpected rise in costs, due to change in cost inputs	Less economic ore	H	Accounts	Secure cost base via long term contracts
Cost Base	Extra trucking required to place waste	Extra mining costs	H	Nil	Destination planning
Mine Plan	Mining equipment has not been calculated, fleet equipment and drill capacity has not been considered as bottleneck	Either lower tonnes, or higher costs; or both	M		Include fleet equipment calculation
Mine Plan	Planning resolution at % bench level	Inaccurate production plan vs timing	M		Include blast masters at weekly resolution, bench developing plan, spatial reconciliation
Mine Closure	Mine closure requirement becomes more expensive and more extensive due to changes in regulation and expectations since permits granted in 2012	Extra Costs	L	Engage with regulator to reconfirm closure requirements	
Geotechnical	Unpredicted rock fall	Delay operation	M	Geotechnical control	Improve Existing Controls and defined geotechnical domains
Water Management	Reach water storage limit	Use the pit as inpit pond	M	Environmental management	Build the osmosis water treatment plant
Permits	Extension permits for WD and TSF not delivered in time	Stop Operation	M		
Reserve Estimate	Actual varies from planned	Time to compile a credible reserve	M		

17 Forward work plan

This section presents the opportunities detected during the provision of this service and the forward plan to improve the Barruecopardo project.

17.1 Opportunities

Below are listed key opportunities for improving the different areas of work.

- A close control on dilution and losses could imply a reduction of them and an increase in the project value.
- Saloro is reviewing their contracts with a view to varying the conditions applicable to their concentrate sales, this could imply a better recovery or better selling conditions.
- With better knowledge of the deposit phase 5 may become economical. Particularly as potential inferred material can be upgraded to Indicated resource category.
- Include the current marginal stockpile with more detailed cost calculation or even try to locate the old tailings that potentially could contain tungsten in proportions above the COG. That is, in prior periods of poor recovery, significant amounts of WO_3 would have been disposed of as tailings. There is no liability with those old tailings for Saloro if those are not removed or occupied by the mine plan so if the material becomes suitable for processing, the resultant tailings would need to be treated accordingly.

17.2 Future work plan

- Closely monitor the effectiveness of the implementation of the plan to improve recovery in the plant.
- The increase in the pit to the north and in depth should be preceded by a conversion of indicated resources into measured and to try to incorporate more inferred material into the mine plan as indicated. For this reason, the drilling program that is due to be approved is very important for future reserves estimation.
- Develop the change management processes to operationally move to the designs completed in this service, and plans developed in this work.
- The efforts in the control of dilution and losses require improved monitoring with a potential review of those figures to take place in the future reserves estimate.
- A concerted plan is required to accurately measure loss and dilution, and then to reduce it. Other narrow vein mines operate at significantly lower values for loss and dilution. Potential avenues to explore include:
    1. Modelling these as a “skin” on the resource, rather than applying a %’s to block models. This is likely to align practice with planning, particularly in grade control.

2. Orientating the mining faces, so that excavators retreat along strike, could be beneficial. This may include assessing the geometry of the excavator buckets.
3. Training of operators and supervisory geological staff.
4. Assessing blast initiation sequences to minimise Dilution and loss is a common practise at Saloro, the control on how the new explosives can modify this needs to be monitored.
5. Fleet equipment study to optimize operation in narrow areas of the pit, what could reduce the SMU.

- Perform volume reconciliation against actuals and plan on blast and polygon scale.
- Working on the submission of various permits is required. These include waste storage, Environmental Impact, and overall mining licence. Delays in obtaining these required extensions to permits will incur costs and may lead to reduction in concentrate production.
- A full Mine closure plan should be developed, recognising the obligations in this may have changed since the mine closure portion of the current operating permit was approved in 2012. In particular the costing of the mine closure program should be done from a first principals basis.
- Measure, and sample, stockpiles.
- Grade and metal reconciliation between the process and the mining can help substantially to close gaps between their calculations. This should also include reconciliation with the stockpiles.
- Consider adding the missing deleterious elements to resource model
- Undertake waste dump (destination) planning, so that actual haulage costs are forecasted accurately. Mining is the most significant cost for the operation, and in that waste haulage the largest controllable cost.
- Assess in-pit waste dumping, particularly in upper benches of early phases where the pit does not require deepening. This will reduce costs, and reduce surface disturbance for waste storage, that needs future rehabilitation.
- Assess a move to an electronic Fleet Management System so as to aid grade control and production recording. Options are available for mines of Barrauecopardo size.
- Early works to prepare for the next contract mining negotiation should be considered. Is an opportunity to increase certainty at a LoM scale over the greatest cost element.
- Asses, with the resource geologist, where the next resource drilling campaign should be targeted.
- Define geotechnical areas or sectors to improve design with specific parameters for each pit slope.
- Trade off study of UG mining operations vs OP in specific deposit areas.
- Move to annual updates on Ore Reserves, noting ASX requirements of the parent company EQ Resources who is listed on the Australian stock exchange, as well a the likely upcoming changes to JORC.

- As life of mine is extended, fixed assets in material handling need to be reviewed to ensure they can continue to provide reliable service. These may require increases to sustaining capex.

  Environmental bond estimate to be revised to include the extension of the LoM, including the extension of rehabilitation areas in pit and waste dump.

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19 Acronyms and terms

AF	Acid Forming
AMP	Advanced mineral processing
APP	Aproved
APT	Ammonium Paratungstate
ASX	Australian Securities Exchange
BM	Block Model
BOCYL	Boletín Oficial de Castilla y León.
CAPEX	Capital expenditures
CBS	Conditional bias slope
CEG	Complejo Esquisto-Grauváquico / Shist-Grauwacke Complex
CF	Cash Flow
CFM	Cash Flow Model
CHK	Checked
CIZ	Central Iberian Zone
COG	Cut-off grade
CP	As defined by JORC
cm3	Cubic centimeter
CPI	Consumer Price Index
CSA	Mining Consultancy Company; authored resources and reserves reports in DFS
DCF	Discounted Cash Flow
DD	Diamond Drill
DDH	Diamond Drill Holes
DFS	Definitive Feasibility Study
DIA	Declaración de Impacto Ambiental, environmental permit
EBI	Earnings Before Interest
EBITD	Earnings Before Interest, Taxes and Depreciation
EBITDA	Earnings Before Interest, Taxes, Depreciation and Amortisation
ENE	East-northeast
EOM	End of Month
EOY	End of Year
EP	Exploitation Project
EQ Resources Limited	100% owner of Saloro S.L.U.
ESE	East-Southeast
ETRS	European Terrestrial Reference System
ETRS89	European Terrestrial Reference System 1989
EUR	Euros
EurGeol	Professional title awarded by the European Federation of Geologists
FEM	Finite element methods
FOB	Free on board
FoS	Factor of safety
FS	Feasibility study
G&A (costs)	General and Administration costs
GSI	Geological strength index

HB	Hoek and Bray
HG	High grade
ID2	Inverse distance squared
IGME	Instituto Geológico y Minero de España / Spanish geological and mining institute
IMEB	Iberian Mining Engineers Board
INE	Spanish statistics agency
IP	Investigation Permit
ITC	Instrucción Técnica Complementaria, Complementary Technical Instruction
JCS	Joint compressive strength
JORC	Joint Ore Reserves Committee
JRC	Joint roughness coefficient
KE	Kriging efficiency
km2	square kilometer
KNA	Kriging Neighborhood Analysis
KPI	Key performance indicators
LG	Low grade
LOM	Life Of Mine
LoMP	Life of Mine Plan
MAGNA	Mapa Geológico Nacional / Spanish national geological map
MAGNA50	Mapa Geológico Nacional / Spanish national geological map scale 1:50000
MAR	Marginal
ML	Mining License
MLA	Mining License Application
Mpa	Megapascal
MP	Mine Plan
MRE	Mineral resource estimation
MT	Million Tonne
MTU	Metric tonne unit
MWD	Main water dam
NAF	Non-Acid Forming
NNE	North-northeast
NPV	Net present value
NW	Northwest
Oaktree	Previous owner of Saloro S.L.U. current shareholder of EQ Resources
OK	Ordinary kriging
OP	Open Pit, out of Polygon ore
OPEX	Operation Expeditures
ORE	Ore Reserve Estimate
PEAD	HDPE, High Density Polyethylene
PEAL	Contract miners currently operating the Barruecopardo pit for Saloro SLU
QAQC	Quality assurance and quality control
RC	Reverse circulation holes
RD	Real Decreto

RGNB	Reglamento General de Normas Básicas
RL	Reduced level
RMR	Rock mass rating
ROM	Run of mine
RPEE	Prospects of Economic Extraction
SE	Southeast
SGS	Conslulting Company responsible of 2007 metallugical testing
SL	Sociedad Limitada, Limited company
SLO	Saloro
SLU	Sociedad Limitada Unipersonal, Single Person Limited
SMU	Selective Mining Unit
SR	Stripping Ratio
SRF	Stress Reduction Factor
SSE	South-southeast
SSW	South-southwest
SW	Southwest
TSF	Tailings storage facilities
UG	Underground
UK	United Kingdom
US	United States
UTM	Universal Transverse Mercator
UV	Ultraviolet
WAI	Wardell Amstrong International. Consulting services company, particulary involved with the DFS
WD	Waste Dump
WM	Wood Mackenzie
WNW	West-northwest
WSW	West-southwest
WO3	Tungsten Oxide grade
XRF	X-Ray Fluorescence lamp