

29 July 2024

HIGH-GRADE DRILLING RESULTS CONFIRM MAIN MINERALISED LEVEL AT MT CARBINE

EQ Resources Ltd is a global tungsten producer with mining activities in Australia and Spain.

Highlights:

- Completed a further 37 holes of Infill RC Drilling at 10m spacing into the Main Vein Packages at Mt Carbine, totaling 1,437m of drilling
- High-grade drilling results confirm the main mineralised level of the deposit is being intersected starting at 295-305m RL
- Drilling of the main ore zone revealed several high-grade intersections*, including:
 - 8m @ 1.33% WO₃ MCM 241 from 14m
 - 4m @ 2.33% WO3 MCM 241 from 27m
 - 13m @ 0.88% WO3 MCM 256 from 38m
 - 7m @ 1.23% WO₃ MCM 259 from 20m
 - 5m @ 1.44% WO3 MCM 261 from 6m
 - 7m @ 0.81% WO₃ MCM 263 from 28m
 - 9m @ 1.73% WO3 MCM 269 from 25m
 - 9m @ 0.61% WO3 MCM 272 from 8m
 - 7m @ 0.71% WO3 MCM 272 from 44m
- Individual veins with true widths ranging from 0.3m to 3.0m were intersected, with grades ranging from 0.5% to 7.67% WO₃

*Intervals are down hole intercepts sampled at 1m intervals and then composited.

EQ Resources Limited ("EQR" or "the Company") is pleased to announce the results of a further 37 Infill Reverse Circulation Drill holes ("RC" holes), totaling 1,437m of drilling and targeting the main benches of the Andy White Open Pit.

Drilling from the current pit floor at the 295-305m level reveals four main zones of mineralization, covering a 100m strike and 80m width (see Figure 1 and 2). This section is part of the main vein system, known to extend for 1.2km along strike with substantial width. Parallel and to the north lies the Iron Duke Vein system, similar in scale but currently defined only at the inferred resource level. Both vein systems extend an additional 80m below the planned Pit II depth of 250m RL. Further evaluations will be conducted to assess deeper extensions.

EQR's CEO, Kevin MacNeill, commented: "The main ore body level at the Iolanthe-Bluff-Wayback-Johnson vein system shows outstanding results. Although mining will commence next year on most of these benches, it is pleasing to see that the excellent infill results align well with our Pit II design. The consistency of these veins confirmed in this round of drilling provide us very promising targets for underground vein mining, and the extensions of these zones to the west will constitute a substantial part of our underground ore body."



RC	CORILL HOLE SU	JMMARY (S	IGNIFICAN	T RESULTS)
Hole	Vein	From (m)	To (m)	Interval (m)	Grade (WO ₃ %)
MCM 238	South Johnson	20	21	1	0.67
MCM 239	South Johnson	24	28	4	0.51
MCM 240	South Johnson	4	5	1	0.88
MCM 241	South Johnson	14	22	8	1.31
	South Johnson	27	31	4	2.32
MCM 242	South Johnson	7	10	3	1.26
MCM 242	South Johnson	18	21	3	0.83
MCM 245	Wayback	21	23	2	0.55
MCM 247	Wayback	0	4	4	1.14
	Wayback	13	15	2	1.88
MCM 248	Wayback	5	8	3	1.32
MCM 248	Wayback	15	16	1	0.97
MCM 249	Wayback	14	15	1	0.80
MCM 251	South Johnson	0	10	10	0.54
MCM 252	South Johnson	32	33	1	0.62
MCM 255	Wayback	20	26	6	0.87
MCM 255	Wayback	42	44	2	0.85
	Bluff	16	23	7	0.83
MCM 250	Bluff	38	51	13	0.88
	Bluff	20	22	2	1.51
	Bluff	27	29	2	0.73
MCM 256	Bluff	36	38	2	0.61
	Bluff	43	45	2	1.36
MCM 259	Bluff	20	27	7	1.23
MCM 260	Wayback	23	27	4	1.41
MCM 261	Wayback	6	11	5	1.44
MCM 262	Wayback	22	25	3	1.64
MCM 262	Wayback	33	40	7	0.64
MCM 263	Bluff	15	17	2	0.51
MCM 263	Bluff	28	35	7	0.81
MCM 264	Bluff	45	46	1	1.15
MCM 266	Wayback	19	20	1	0.56
MCM 268	Bluff	13	15	2	1.04
MCM 269	Iolanthe	10	13	3	0.87
MCM 269	Iolanthe	25	34	9	1.73
MCM 270	Iolanthe	34	37	3	0.59
MCM 271	Bluff	10	12	2	0.79
MCM 272	Bluff	8	17	9	0.61
MCM 272	Iolanthe	44	51	7	0.71

Table 1 - Significant Zones of Mineralisation (see individual hole details in Appendix 1)





Figure 1 - Orthomosaic Image of Pit I Floor showing Drill Locations for 37 Holes reported in this announcement



Figure 2 - Insert of the recent drill holes on the 295m bench showing the pit floor and significant intercepts



This drilling aimed to target the zone below the current mine level of 295m RL in the main pit area. The detailed examination of this primary ore body has provided the Company with increased confidence in future mining plans. Remarkably, in this program with 10m spacing, only one out of 37 holes failed to yield significant results.



Figure 3 - Shows Isometric View of Current Pit 1 in grey, relative to the recent drilling below with high-grade (>0.5% WO₃) shown in red

This drilling program builds on the good results so far from the Company's 2024 Drilling Campaign (see ASX announcement <u>'Mt Carbine Infill Drilling Reveals Additional High-Grade Ore In Stage II Waste Cutback Area</u>' dated 3 June 2024, and ASX announcement <u>'Mt Carbine Infill Drilling Reveals High-Grade Zones In Stage II Pit</u>' dated 30 April 2024).



Figure 4 - Block Model showing main high-grade vein packages relative to Pit I (in blue, currently mined) & II (in grey, next stage mine plan)

Released on authority of the Board by:

Kevin MacNeill Chief Executive Officer

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About the Company

EQ Resources Limited is a leading tungsten mining company dedicated to sustainable mining and processing practices. The Company is listed on the Australian Securities Exchange, with a focus on expanding its world-class tungsten assets at Mt Carbine in North Queensland (Australia) and at Barruecopardo in the Salamanca Province (Spain). The Company leverages advanced minerals processing technology and unexploited resources across multiple jurisdictions, with the aim of being a globally leading supplier of the critical mineral, tungsten. While the Company also holds gold exploration licences in New South Wales (Australia), it aims to create shareholder value through the exploration and development of its current project portfolio whilst continuing to evaluate corporate and exploration opportunities within the new economy and critical minerals sector globally.

Competent Person's Statements

EQ Resources' exploration and resource work is being managed by Mr. Tony Bainbridge, AusIMM. Mr. Bainbridge is engaged as a contractor by the Company and is not "independent" within the meaning of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (the JORC Code). Mr. Bainbridge has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in JORC Code 2012. The technical information contained in this announcement relating exploration results are based on, and fairly represents, information compiled by Mr. Bainbridge.

Forward-looking Statements

This announcement may contain forward-looking statements. Forward-looking statements address future events and conditions and therefore involve inherent risks and uncertainties. Actual results may differ materially from those currently anticipated in such statements. Particular risks applicable to this announcement include risks associated with planned production, including the ability of the Company to achieve its targeted production outline due to regulatory, technical or economic factors. In addition, there are risks associated with estimates of resources, and there is no guarantee that a resource will have demonstrated economic viability as necessary to be classified as a reserve. There is no guarantee that additional exploration work will result in significant increases to resource estimates. Neither the Australian Securities Exchange nor its Regulation Services Provider (as that term is defined in policies of the Australian Securities Exchange) accepts responsibility for the adequacy or accuracy of this announcement.





Appendix 1 – Individual Assay Results

Note for grade control RC sampling the Company is using its own calibrated internal laboratory set up with a Thermo Scientific ARL Quant'X X-Ray Fluorescence Spectrometer that has been calibrated with official standards and has a 10% external QAQC program being applied to all assays. This machine however is not from a NATA accredited lab. See attached Table 1 from the JORC Code for full information on processing and QAQC details.
 Intervals in table represent downhole depth, not true thickness with no applied upper cut. The highlight (bold) intervals represent where King-Veins have intersected above 1% WO₃ grade. It should be noted drilling was completed at 70 degree dip and a high angle to the vein systems.

Hole #	East	North	RL	EOH	Dip	Azm	From	То	WO3%	Interval	WO3 %
							2	3	0.16	1	0.16
MCM 237	22,890	26.340	296.5	33.0	65	180	8	9	0.58		
	,000	_0,0.0		0010		_	9	10	0.14	2	0.36
							28	29	0.13	1	0.13
MCM 238	22,880	26,340	296.4	33.0	65	180	20	21	0.67	1	0.67
							24	25	0.89		
MCM 239	22,870	26,339	296.7	33.0	65	180	25	26	0.80		
							20	21	0.13	Λ	0.51
							<u>21</u>	5	0.20	4	0.01
							28	20	0.00	I	0.00
MCM 240	22,860	26,340	296.5	33.0	65	180	20	30	0.13		
							30	31	0.07	3	0.23
							14	15	0.13		0.20
							15	16	2.97		
							16	17	1.53		
							17	18	0.86		
							18	19	3.76	4	2.28
MCM 244	22.960	26.244	206.4	22.0	C.F.	0	19	20	0.73		
	22,860	26,341	296.4	33.0	60	0	20	21	0.12		
							21	22	0.38	8	1.31
							27	28	6.27		
							28	29	0.46		
							29	30	2.40		
							30	31	0.15	4	2.32
							0	1	0.35	1	0.35
							7	8	3.31		
	00.070	00.040	000.0	00.0	05	0	8	9	0.18	•	4.00
	22,870	26,340	296.8	33.0	65	0	9	10	0.30	3	1.26
							18	19	1.52		
							19	20 21	0.73	2	0.83
MCM 243	22 880	26 3/1	206 5	33.0	65	0	20	Z I	0.20 Significant	Results	0.03
	22,000	20,041	200.0	00.0	00	0	0	1	0.60	Results	
							1	2	0.11		
							2	3	0.37	3	0.36
							15	16	0.41	-	
	~~~~~	00.044	000 F		05	•	16	17	0.19		
MCM 244	22,890	26,341	296.5	33.0	65	0	17	18	0.06		
							18	19	0.02		
							19	20	0.72		
							20	21	0.17	6	0.26
							31	32	0.11	1	0.11
							8	9	0.46		
MCM 245	22,880	26,330	296.4	33.0	65	180	9	10	0.90		
							10	11	0.23		



							11	12	0.16	4	0.43
							21	22	0.91		
							22	23	0.18	2	0.55
							10	11	0.33	1	0.33
							24	25	1.39		
MCM 246	22,888	26,329	296.7	33.0	65	180	25	26	0.24		
							26	27	0.24	3	
							0	1	0.30	-	
							1	2	3.52		
							2	3	0.62		
MCM 247	22,870	26,330	296.1	33.0	65	180	3	4	0.13	4	1.14
							13	14	2.85	-	
							14	15	0.90	2	1.88
							1	2	0.10	1	0.10
							5	6	2.13		
MCM 248	22,860	26,330	296.0	33.0	65	180	6	7	1.61		
							7	8	0.22	3	1.32
							15	16	0.97	1	0.97
MCM 249	22,850	26,330	295.6	33.0	65	180	14	15	0.80	1	0.80
							0	1	0.11	1	0.11
MCM 250	22,841	26,329	295.5	33.0	65	180	24	25	0.18	1	0.18
							32	33	0.33	1	0.33
							0	1	0.60		
							1	2	3.40		
							2	3	0.72		
							3	4	0.09		
							4	5	0.01		
MCM 251	22,840	26,340	295.2	33.0	65	0	5	6	0.01		
							6	7	0.01		
							7	8	0.21		
							8	9	0.15		
							9	10	0.17	10.00	0.54
							29	30	0.43	1.00	0.43
MCM 252	22,850	26,341	295.3	33.0	65	0	32	33	0.62	1.00	0.62
							3	4	0.31		
							4	5	0.22	2.00	0.26
MCM 252	22.850	26.240	205 /	22.0	65	190	9	10	0.22		
	22,000	20,340	295.4	55.0	05	100	10	11	0.76	2.00	0.49
							29	30	0.83		
							30	31	0.10	2.00	0.46
							2	3	0.65		
MCM 254	22 840	26 339	295.3	33.0	65	180	3	4	0.15	2.00	0.40
	22,010	20,000	200.0	00.0	00	100	14	15	0.18	1.00	0.18
							21	22	0.15	1.00	0.15
							0	1	0.36		
							1	2	0.14	2.00	0.25
							20	21	1.18		
							21	22	2.15		
							22	23	0.63		
MCM 255	22,899	26,341	296.9	51.0	65	180	23	24	0.24		
							24	25	0.71		
							25	26	0.31	6.00	0.87
							34	35	0.37	1.00	0.37
							42	43	1.50		
							43	44	0.20	2.00	0.85



							0	1	0.13	1.00	0.13
							5	6	0.19	1.00	0.19
							9	10	0.52		
							10	11	0.10		
							11	12	0.10	3.00	0.24
							16	17	0.59		
							17	18	1.85		
							18	19	0.14		
							19	20	0.06		
							20	21	2.46		
							21	22	0.51		
							22	23	0.23	7.00	0.83
MCM 256	22,870	26,320	295.9	51.0	65	180	38	39	2.55		
							39	40	3.05		
							40	41	1.25	3.00	2.28
							41	42	0.93		
							42	43	0.67		
							43	44	0.49		
							44	45	0.47		
							45	46	0.70		
							46	47	0.34		
							47	48	0.18		
							48	49	0.11		
							49	50	0.56		
							50	51	0.15	13.00	0.88
							3	4	0.21	1.00	0.21
							/	8	0.15		
							8	9	0.08	0.00	0.44
							9	14	0.11	3.00	0.11
							13	14	0.40		
							14	16	0.24		
							16	17	0.15		
MCM 257	22 861	26.319	296.3	51.0	65	180	17	18	0.00		
	22,001	20,010	200.0	0110	00	100	18	19	0.30	6.00	0 34
							24	25	0.00	1.00	0.23
							44	45	0.14	1.00	0.20
							45	46	0.66		
							46	47	0.23		
							47	48	0.09		
							48	49	1.07		
							49	50	0.51	6.00	0.45
							0	1	0.13	1.00	0.13
							17	18	0.12	1.00	0.12
							20	21	0.11		
							21	22	2.91	2.00	1.51
							27	28	1.24		
MCM 258	22,850	26,319	295.8	51.0	65	180	28	29	0.23	2.00	0.73
							36	37	1.02		
							37	38	0.21	2.00	0.61
							39	40	0.07	1.00	0.13
							43	44	2.59		
							44	45	0.13	2.00	1.36
MCM 259	22,841	26,321	295.5	51.0	65	180	4	5	0.42	1.00	0.42
		•	-	-		-	20	21	1.99		



							21	22	1 31		
							22	23	0.23		
							23	24	0.12		
							24	25	3.93		
							25	26	0.82		
							26	27	0.20	7.00	1.23
							0	1	0.31		
							1	2	0.10		
							2	3	0.11	3.00	0.17
MCM 260	22.831	26.339	295.3	51.0	65	180	23	24	2.20	0.00	0
	,	,					24	25	2.20		
							25	26	0.76		
							26	27	0.47	4	1.41
							0	1	0.17	-	
							1	2	0.66		
							2	3	0.18	3	0.34
							6	7	1.72		
MCM 261	22,831	26,340	295.3	33.0	65	0	7	8	3.82		
							8	9	0.73		
							9	10	0.71		
							10	11	0.20	5	1.44
							22	23	3.72	•	
							23	24	1.07		
							24	25	0.13	3.00	1.64
							33	34	2.67		
							34	35	0.74		
MCM 262	22,896	26,341	296.8	51.0	65	180	35	36	0.19		
							36	37	0.49		
							37	38	0.17		
							38	39	0.10		
							39	40	0.15	7.00	0.64
							15	16	0.78		
							16	17	0.24	2	0.51
							28	29	3.38		
							29	30	1.34		
							30	31	0.25	3.00	1.66
MCM 263	22,889	26,322	296.4	51.0	65	180	31	32	0.13		
							32	33	0.10		
							33	34	0.29		
							34	35	0.19	5.00	0.81
							37	38	0.19	1.00	0.19
							50	51	0.21	1.00	0.21
							21	22	0.98		
							22	23	0.16		
							23	24	0.05		
							24	25	0.01		
							25	26	0.04		
MCM 264	22,881	26,321	296.4	51.0	65	180	26	27	0.85		
							27	28	0.25		
							28	29	0.07	7.00	0.35
							45	46	1.15	1.00	1.15
							49	50	0.13		
							50	51	0.05		
MCM 265	22 830	26 330	205 5	33 U	65	180	0	1	0.20	3.00	0.38
	22,030	20,330	290.0	33.0	00	100	18	19	0.12	1.00	0.12



MCM 268         22,821         26,312         305.0         33.0         65         180         2         0.07         2           MCM 266         22,821         26,332         295.5         33.0         65         180         1         0.11         6.00         0.34           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.14           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.14           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 268         22,828         26,312         305.0         33.0         65         180         9         10         0.48         1.00         0.41           1         2         0.31         -         -         7         8         0.11         7.00         0.41           1         1         1         1.00         0.28         -         6         7         0.12								25	26	0.13		
MCM 268         22,821         26,312         305.0         33.0         65         180         9         1.0         0.48         1.00         0.34           MCM 266         22,821         26,331         295.5         33.0         65         180         12         13         0.14         1.00         0.34           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.34           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           12         13         0.14         1.00         0.48         1.00         0.48         1.00         0.48           13         14         0.83         1.00         0.24         3         1.66         3         4         0.31         1.00         0.24           13         14         0.83         1.00         0.28         26         <								26	27	0.10		
MCM 266         22,821         26,331         295.5         33.0         65         180         12         13         0.11         6.00         0.34           MCM 266         22,821         26,331         295.5         33.0         65         180         12         13         0.14         1.00         0.14           19         20         0.56         1.00         0.56         1.00         0.56           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.14           19         20         0.56         1.00         0.56         1.00         0.56         1.00         0.56           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           1         22,828         26,312         305.0         33.0         65         180         7         8         0.11         7.00         0.41           13         14         0.83         -         -         2.00         1.04         18         19         0.28         1.00         0.2								27	28	1.37		
MCM 266         22,821         26,321         295.5         33.0         65         180         0         1         0.30         31         0.11         6.00         0.34           MCM 267         22,821         26,331         295.5         33.0         65         180         9         10         0.48         1.00         0.14           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 268         22,828         26,312         305.0         33.0         65         180         9         10         0.48         1.00         0.41           MCM 268         22,828         26,312         305.0         33.0         65         180         7         8         0.11         7.00         0.41           13         14         0.83         -         -         13         14         0.83         -         -           22,828         29         0.11								28	29	0.27		
MCM 266         22,821         26,331         295.5         33.0         65         180         0         1         0.34         1.00         0.34           MCM 267         22,821         26,331         295.5         33.0         65         180         12         13         0.14         1.00         0.34           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 268         22,828         26,312         305.0         33.0         65         180         9         10         0.48         1.00         0.48           MCM 268         22,828         26,312         305.0         33.0         65         180         7         8         0.11         7.00         0.41           13         14         0.83         1.00         0.28         26         27         0.12         2.00         1.04           18         19         0.22         3.00         0.87								20	30	0.10		
MCM 268         22,821         26,331         295.5         33.0         65         180         12         13         0.14         1.00         0.34           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.34           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 268         22,828         26,312         305.0         33.0         65         180         7         8         0.11         7.00         0.41           13         14         0.5         0.20         -         -         5         6         0.06         -         -         -         10         11         1.03         0.21         2.00         1.04           18         19         0.28         1.00         0.28         -         -         26         27         0.12         - <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>30</th><th>31</th><th>0.10</th><th>6.00</th><th>0.34</th></t<>								30	31	0.10	6.00	0.34
MCM 266         22,821         26,331         295.5         33.0         65         180         12         13         0.14         1.00         0.14           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.14           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 268         22,828         26,312         305.0         33.0         65         180         7         8         0.11         7.00         0.41           13         14         0.5         0.20         -         -         10         11         15         0.21         2.00         1.04           14         15         0.21         2.00         1.04         14         15         0.21         2.00         1.04           14         15         0.21         2.00         1.00         0.28<								0	1	0.11	1.00	0.34
MCM 260       22,811       26,332       295.1       33.0       65       180       9       10       0.14       1.00       0.156         MCM 267       22,811       26,332       295.1       33.0       65       180       9       10       0.48       1.00       0.48         MCM 267       22,811       26,332       295.1       33.0       65       180       9       10       0.48       1.00       0.48         MCM 268       22,828       26,312       305.0       33.0       65       180       7       8       0.11       7.00       0.41         13       14       0.83       14       15       0.21       2.00       1.04         13       14       0.83       1.00       0.28       26       27       0.12       27       28       0.56       28       29       0.11       3.00       0.26         10       11       1.53       11       12       0.87       12       13       0.21       2.00       1.04         18       19       0.228       1.00       0.28       26       27       28       0.62       28       29       0.11       3.00       0.87	MCM 266	22 821	26 331	295 5	33.0	65	180	12	13	0.04	1.00	0.34
MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 267         22,811         26,332         295.1         33.0         65         180         9         10         0.48         1.00         0.48           MCM 268         22,828         26,312         305.0         33.0         65         180         7         8         0.11         7.00         0.41           13         14         0.83         14         15         0.21         2.00         1.04           18         19         0.28         1.00         0.28         26         27         0.12         27         28         0.56         28         29         0.11         3.00         0.26           MCM 269         22,831         26,300         304.8         51.0         65         180         29         0.03         -         -           26         27         0.12         27         28	110111 200	22,021	20,001	200.0	00.0	00	100	10	20	0.14	1.00	0.14
MCM 268         22,828         26,312         305.0         33.0         65         180         3         1         2         0.30         3           MCM 268         22,828         26,312         305.0         33.0         65         180         7         8         0.11         7.00         0.41           13         14         0.5         0.20         5         6         0.06         6         7         0.23         7         8         0.11         7.00         0.41           13         14         0.83         14         15         0.21         2.00         1.04           18         19         0.28         1.00         0.28         1.00         0.28           26         27         0.11         3.00         0.26         10         11         1.53           11         12         0.87         11         3.00         0.87         25         26         0.22         26         27         0.12           27         28         0.62         27         0.12         3.00         0.87         25         26         0.22         26         27         0.12         27         28         0.62	MCM 267	22 811	26 332	295.1	33.0	65	180	9	10	0.00	1.00	0.30
MCM 268       22,828       26,312       305.0       33.0       65       180       7       8       0.11       7.00       0.41         13       14       0.83       14       15       0.20       5       6       0.06       6       7       0.23       7       8       0.11       7.00       0.41         13       14       0.83       14       15       0.21       2.00       1.04         18       19       0.28       20       1.04       18       19       0.28       1.00       0.28         26       27       0.12       2.00       1.04       18       19       0.28       1.00       0.28         26       27       0.12       27       28       0.56       28       29       0.11       3.00       0.26         10       11       1.53       11       12       0.87       12       13.00       0.87         25       26       0.22       26       27       0.12       27       28       0.62         27       28       0.62       22       26       22       26       22       26       22       26       29       0.03		,•	_0,00_		00.0			1	2	0.30	1.00	0.10
MCM 268       22,828       26,312       305.0       33.0       65       180       3       4       5       0.20         5       6       0.06       6       7       0.23       7       8       0.11       7.00       0.41         13       14       0.83       14       0.83       14       15       0.21       2.00       1.04         18       19       0.28       1.00       0.28       1.00       0.28         26       27       0.12       2.00       1.04       18       19       0.28       1.00       0.28         26       27       0.12       200       1.04       11       1.53       11       12       0.87         12       13       0.21       3.00       0.87       12       13       0.21       3.00       0.87         25       26       0.22       26       27       0.12       27       28       0.62       28       29       0.03       11       1.53       11       12       13       0.21       3.00       0.87       26       27       28       29       0.03       28       29       0.03       28       29       0.03<								2	3	1.66		
MCM 268       22,828       26,312       305.0       33.0       65       180       7       8       0.01       7.00       0.41         13       14       0.83       14       15       0.20       1.04         13       14       0.83       1.00       0.41         14       15       0.21       2.00       1.04         18       19       0.28       1.00       0.28         26       27       0.12       2.00       1.04         18       19       0.28       1.00       0.28         26       27       0.12       200       1.04         18       19       0.28       0.56       1.00       0.28         26       27       0.12       200       1.04       1.00       1.01       1.53         10       11       1.53       1.00       0.26       1.00       0.21       3.00       0.87         25       26       0.22       26       0.22       26       27       0.12       20       1.00       1.01         12       13       0.21       3.00       0.87       26       27       0.12       20       28 <t< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>3</th><th>4</th><th>0.31</th><th></th><th></th></t<>								3	4	0.31		
MCM 268       22,828       26,312       305.0       33.0       65       180       7       8       0.11       7.00       0.41         13       14       0.83       14       15       0.23       1.04       13         14       15       0.21       2.00       1.04       13       14       0.83       1.04         18       19       0.28       1.00       0.28       2.00       1.04         18       19       0.28       1.00       0.28       2.00       1.04         18       19       0.28       1.00       0.28       2.00       1.04         18       19       0.28       1.00       0.28       2.00       1.04         18       19       0.28       1.00       0.28       2.00       1.00       0.28         26       27       0.12       2.00       1.01       1.53       11       12       0.87       2.00         25       26       0.22       2.03       3.00       0.87       2.00       2.00       1.00       0.87         26       27       0.12       2.00       2.00       2.00       1.00       1.00       1.00								4	5	0.01		
MCM 268       22,828       26,312       305.0       33.0       65       180       7       8       0.11       7.00       0.41         13       14       0.83       14       15       0.21       2.00       1.04         18       19       0.28       1.00       0.28         26       27       0.12       2.00       1.04         18       19       0.28       1.00       0.28         26       27       0.12       2.00       1.04         18       19       0.28       1.00       0.28         26       27       0.12       27       28       0.56       5         27       28       0.51       3.00       0.26       11       1.00       0.28         10       11       1.53       11       12       0.87       12       13       0.21       3.00       0.87         25       26       0.22       26       27       0.12       26       27       0.12       26       27       0.12       26       27       0.12       28       29       0.03       28       28       29       0.03       28       28       29 <td< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th>5</th><th>6</th><th>0.20</th><th></th><th></th></td<>								5	6	0.20		
MCM 268       22,828       26,312       305.0       33.0       65       180       7       8       0.11       7.00       0.41         13       14       0.83								6	7	0.00		
MCM 269         22,831         26,300         304.8         51.0         65         130         130         0.11         1.00         0.141           13         14         0.83         14         15         0.21         2.00         1.04           18         19         0.28         1.00         0.28         1.00         0.28           26         27         0.12         27         28         0.56         28         29         0.11         3.00         0.26           10         11         1.53         11         12         0.87         12         13         0.21         3.00         0.87           25         26         0.22         26         27         0.12         27         28         0.62         28         29         0.03         11         12         0.87         12         13         0.21         3.00         0.87           25         26         0.22         26         27         0.12         27         28         0.62         28         29         0.03         28         29         0.03         30         31         3.68         30         31         3.68         300         4.57	MCM 268	22 828	26.312	305.0	33.0	65	180	7	8	0.11	7.00	0.41
MCM 269       22,831       26,300       304.8       51.0       65       180       14       15       0.21       2.00       1.04         18       19       0.28       1.00       0.28         26       27       0.12       27       28       0.56         28       29       0.11       3.00       0.26         10       11       1.53       11       12       0.87         12       13       0.21       3.00       0.87         25       26       0.22       26       27       0.12         27       28       0.62       28       29       0.03       11         12       13       0.21       3.00       0.87       25       26       0.22         26       27       0.12       27       28       0.62       28       29       0.03         29       30       7.67       30       31       3.68       31       32       2.37       3.00       4.57	1110111 200	22,020	20,012	000.0	00.0	00	100	13	1/	0.11	7.00	0.41
MCM 269 22,831 26,300 304.8 51.0 65 180 MCM 269 30 7.67 30 31 3.68 31 32 2.37 3.00 4.57								14	15	0.00	2 00	1 04
MCM 269 22,831 26,300 304.8 51.0 65 180 105 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100 0.20 100								18	10	0.21	1.00	0.28
MCM 269 22,831 26,300 304.8 51.0 65 180 20 27 28 0.56 28 29 0.11 3.00 0.26 10 11 1.53 11 12 0.87 12 13 0.21 3.00 0.87 25 26 0.22 26 27 0.12 27 28 0.62 28 29 0.03 29 30 7.67 30 31 3.68 31 32 2.37 3.00 4.57								26	27	0.20	1.00	0.20
MCM 269 22,831 26,300 304.8 51.0 65 180 29 30 7.67 MCM 269 22,831 26,300 304.8 51.0 65 180 29 30 7.67 30 31 3.68 31 32 2.37 3.00 4.57								20	28	0.12		
MCM 269 22,831 26,300 304.8 51.0 65 180 29 22,831 26,300 304.8 51.0 65 180 29 22,831 26,300 304.8 51.0 65 180 20 20 20 20 20 20 20 20 20 20 20 20 20								28	20	0.00	3.00	0.26
MCM 269 22,831 26,300 304.8 51.0 65 180 MCM 269 22,831 26,300 304.8 51.0 65 180 MCM 269 22,831 26,300 304.8 51.0 65 180 MCM 269 22,831 26,300 304.8 51.0 65 180 11 12 0.87 12 13 0.21 3.00 0.87 25 26 0.22 26 27 0.12 27 28 0.62 28 29 0.03 29 30 7.67 30 31 3.68 31 32 2.37 3.00 4.57								10	11	1.53	5.00	0.20
MCM 269 22,831 26,300 304.8 51.0 65 180 MCM 269 22,831 26,300 304.8 51.0 65 180 MCM 269 22,831 26,300 304.8 51.0 65 180 MCM 269 22,831 26,300 304.8 51.0 65 180 12 13 0.21 3.00 0.87 25 26 0.22 26 27 0.12 27 28 0.62 28 29 0.03 29 30 7.67 30 31 3.68 31 32 2.37 3.00 4.57								11	12	0.87		
MCM 269 22,831 26,300 304.8 51.0 65 180 MCM 269 22,831 26,300 304.8 51.0 65 180 MCM 269 22,831 26,300 304.8 51.0 65 180 MCM 269 22,831 26,300 304.8 51.0 65 180 30 31 3.68 31 32 2.37 3.00 4.57								12	12	0.07	3.00	0.87
MCM 269       22,831       26,300       304.8       51.0       65       180       29       30       7.67         30       31       3.68       31       32       2.37 <b>3.00 4.57</b>								25	26	0.21	5.00	0.07
MCM 269       22,831       26,300       304.8       51.0       65       180       29       30       7.67         30       31       3.68       31       32       2.37       3.00       4.57								26	20	0.22		
MCM 269 22,831 26,300 304.8 51.0 65 180 30 31 3.68 31 32 2.37 3.00 4.57								20	28	0.12		
MCM 269 22,831 26,300 304.8 51.0 65 180 29 30 7.67 30 31 3.68 31 32 2.37 3.00 4.57								28	20	0.02		
MCM 269 22,831 26,300 304.8 51.0 65 180 30 31 3.68 31 32 2.37 3.00 4.57								29	30	7 67		
<u>31</u> <u>32</u> <u>2.37</u> <u><b>3.00</b> <u>4.57</u></u>	MCM 269	22,831	26,300	304.8	51.0	65	180	30	31	3.68		
								31	32	2.37	3.00	4.57
32 33 0.54								32	33	0.54	0.00	
33 34 0.35 <b>9.00 1.73</b>								33	34	0.35	9.00	1.73
43 44 0.19								43	44	0.19		
44 45 0.03								44	45	0.03		
45 46 0.11								45	46	0.11		
46 47 0.22 4.00 0.14								46	47	0.22	4.00	0.14
6 7 0.61								6	7	0.61		
7 8 0.13								7	8	0.13		
8 9 0.04								8	9	0.04		
9 10 0.16								9	10	0.16		
MCM 270 22,811 26,292 305.6 51.0 65 180 10 11 0.08	MCM 270	22,811	26,292	305.6	51.0	65	180	10	11	0.08		
11 12 0.11 6.00 0.19								11	12	0.11	6.00	0.19
34 35 1.29								34	35	1.29		
35 36 0.39								35	36	0.39		
36 37 0.10 3.00 0.59								36	37	0.10	3.00	0.59
MCM 271 22 811 26 211 204 7 22 0 65 400 10 11 0.47		22.044	26.244	2047	22.0	<u>e</u> e	400	10	11	0.47		
<b>INIGINE 27 1</b> 22,811 20,311 304.7 33.0 05 180 11 12 1.10 2.00 0.79		22,811	20,311	304.7	33.0	60	180	11	12	1.10	2.00	0.79
0 1 0.19 1.00 0.19								0	1	0.19	1.00	0.19
8 9 2.34								8	9	2.34		
MCM 272 22,821 26,310 305.1 51.0 65 180 9 10 0.36	MCM 272	22,821	26,310	305.1	51.0	65	180	9	10	0.36		
10 11 0.20								10	11	0.20		
11 12 0.04								11	12	0.04		



							12	13	0.01		
							13	14	1.23		
							14	15	0.12		
							15	16	0.96		
							16	17	0.24	9.00	0.61
							22	23	0.41	1.00	0.41
							29	30	0.10	1.00	0.10
							44	45	1.37		
							45	46	1.13		
							46	47	1.27		
							47	48	0.54		
							48	49	0.31		
							49	50	0.17		
							50	51	0.20	7.00	0.71
MCM 273	22 812	26 298	305.2	33.0	65	180	0	1	0.11	1.00	0.11
	22,012	20,290	505.2	55.0	00	100	20	21	0.14	1.00	0.14



# JORC Table 1 - Exploration Results

## Section 1 - Sampling Techniques and Data

Criteria	Explanation	Commentary
Sampling techniques	Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc.). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.	<ul> <li>Sampling was taken from a cyclone mounted on the side of the RC rig which provides a continuous split as the sample is taken.</li> <li>The sample locations were marked out using DGPS locator staff and sampling was taken as channel continuous sample of outcrop.</li> <li>The samples each represent 1m of drilling and generally weigh 5 kg of material that is P90 of -5mm. Between samples the hole is flushed with air between samples to avoid contamination between zones. A sieve is used to fill a sample tray with each trip tray box representing 1m. These chip trays are used to log the hole and are examined under blue light to see the presence of scheelite.</li> <li>The entire sample size is split down to 500gm charge which is then pulverized to 75 micron before 200gm is split into making up the representative sample.</li> </ul>
Drilling techniques	Drill type (e.g. core, reverse circulation, open- hole hammer, rotary air blast, auger, Bangka, sonic, etc.) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc.).	Reverse Circulation Drilling.
Drill sample recovery	<ul> <li>Method of recording and assessing core and chip sample recoveries and results assessed.</li> <li>Measures taken to maximise sample recovery and ensure representative nature of the samples.</li> <li>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</li> </ul>	<ul><li>The samples were recorded on the maps and also on the digital survey instrument (Texas DGPS).</li><li>There does not appear to be any link between sample recovery and grade.</li></ul>
Logging	<ul> <li>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</li> <li>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc.) photography.</li> <li>The total length and percentage of the relevant intersections logged.</li> </ul>	Mapping occurred on floor bench outcrop and was mapped for alteration, geology, mineralisation and structure. The veins shown were measured for strike and continuity.





Criteria	Explanation	Commentary
Sub-sampling techniques and sample preparation	<ul> <li>If core, whether cut or sawn and whether quarter, half or all core taken.</li> <li>If non-core, whether riffled, tube sampled, rotary split, etc. and whether sampled wet or dry.</li> <li>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</li> <li>Quality control procedures adopted for all sub- sampling stages to maximise representivity of samples.</li> <li>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</li> <li>Whether sample sizes are appropriate to the grain size of the material being sampled.</li> </ul>	The 5kg samples were crushed in Jaw initially and split at <5mm to get down to 1kg. Finer crushing then occurred until we could achieve a representative 500gm sample. This was pulverized in LM2 grinder and a subset of - 200mesh powder of 200gm was split off. Approximately 10grams of this fine powder was then taken for assay internally using our own XRF analysis machine using full QAQC protocols.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. For geophysical tools, spectrometers, handheld XRF instruments, etc., the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.	The sample assay was taken with 10% of the samples in the batch were standards with known tungsten / Arsenic values. A further 10% blanks was inserted to ensure there was no carryover of sample nor any variance in the drift curve for the Thermofisher XRF machine.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel. The use of twinned holes. Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. Discuss any adjustment to assay data	Sampling was undertaken by Site Geological Team under the supervision of Tony Bainbridge chief geologists who has 42 years of experience in mining and exploration. The samples and methodology for these samples was also supervised by Tony Bainbridge as QP for the Mt Carbine Project. It can be verified the custody of the sample and that all QAQC was checked before these results have been reported here.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. Specification of the grid system used. Quality and adequacy of topographic control.	The samples collected are representative and our QAQC sampling in comparison to ALS laboratories in Brisbane Australia resides with 2% of their results during checks. A calibration curve is regularly checked for consistency in our XRF machine.
Data spacing and distribution	<ul> <li>Data spacing for reporting of Exploration Results.</li> <li>Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.</li> <li>Whether sample compositing has been applied.</li> </ul>	RC hole locations are shown in Figure 3 and detailed in Appendix 1. Spacing is considered sufficient to establish geological and grade continuity. No composites were used.



Criteria	Explanation	Commentary
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	All RC Holes are taken at a 65-70 degree dip with both dip and direction surveyed accurately. The veining in the pit is dominantly vertical and the high angle to the veins needs to be calculated in the estimations of zones.
Sample security	The measures taken to ensure sample security.	The sample is taken to the Company's internal laboratory on the same day as taken. The lab has a perimeter fence and secured during the night.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	No audit of the sampling has as yet been undertaken and it is planned to drill shallow percussion holes to validate this trench result.

## Section 2 - Reporting of Exploration Results

(	Criteria	listed	in the	preceding	section als	o apply t	o this	section)	
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Criteria	Explanation	Commentary
Mineral tenement and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	The resource estimates reported herein are all within Mining Leases 4867 (358.5ha, expiry 31-07-2048) and 4919 (7.891ha, expiry 31-08-2049), held by Mt Carbine Quarries Pty Ltd. The Mining Leases lie within Brooklyn Grazing Homestead Perpetual Lease. Native Title has been extinguished in the Mining Leases by Deed of Grant.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	<ul> <li>No previous examination of these results have been reported.</li> <li>Historical (1974-1987) mine records: A nearly complete record of mine production, including amounts of mined rock consigned to the LGS has been compiled using published and unpublished archives, including reporting for State Royalty returns.</li> </ul>
Geology	Deposit type, geological setting and style of mineralisation.	<ul> <li><u>The Deposit</u></li> <li><u>The Mt Carbine tungsten deposit is a sheeted quartz</u> vein deposit. Many sub-parallel, sub-vertical quartz veins have been deposited in fractures developed in the host rocks metasediments in a zone that drilling and mapping of historical surface workings have shown to be approximately 300m wide and at least 1.4km long, trending at about 315 degrees.</li> <li><u>Grade Variation</u></li> <li>Sampling, drill core logging, geostatistical analysis of drill core assay data and mapping of the open pit have determined that all the material mined during the previous operation was mineralised to some</li> </ul>



Criteria	Explanation	Commentary
		extent and that the mineralogy of the deposit was uniform. There is little doubt that the mineralogy of the stockpile material is identical to that mined and processed. The material in the stockpile comprises a single formation, the result of the alteration of Siluro-Devonian meta-sedimentary host rocks (Forsythe and Higgins, 1990). The amount of quartz veining varies within the mineralised zone and previous mining and exploration have been concentrated at the south- eastern end of the mineralised zone. It is well understood that there are high-grade zones within the mineralisation in this part of the deposit and that the higher-grade zones are surrounded by lower grade mineralisation. Interpretation of recent drilling suggests that the main high-grade zone may plunge to the north of the present open pit. The previous mine assumption that quartz vein abundance is directly correlated with grade is not supported by an independent review of quartz vein abundance and grade.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: easting and northing of the drill hole collar elevation or RL (Reduced Level - elevation above sea level in metres) of the drill hole collar dip and azimuth of the hole down hole length and interception depth hole length. If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case	See Appendix 1.
Data aggregation methods	In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated. Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. The assumptions used for any reporting of metal equivalent values should be clearly stated	The samples have been composited on a weighted average for the distance of each sample. No cut off grades were used.



Criteria	Explanation	Commentary
Relationship between mineralisation widths and intercept length	<ul> <li>These relationships are particularly important in the reporting of Exploration Results.</li> <li>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</li> <li>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').</li> </ul>	As the drilling is mainly at 65 degrees and the veins intersected are dominantly vertical it is necessary that the reader of such results understand they are not true widths reported but rather downhole intercepts which are taken into account in the modelling and resource reporting information provided.
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Sample locations are shown in Figure 3.
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	<ul><li>The results of all the drilling at Mt Carbine had at one point or another been reported in the public forum and readers are asked to review these press releases for context. The immediately adjacent hole to this drilling is shown on the sections etc.</li><li>All sample results collected have been reported including high and low intervals.</li></ul>
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	N/A
Further work	The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling). Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	The company plans to continue to drill using an RC rig on a 10 x 10m pattern for grade control. All holes are at 65 degree dips.